API Well Number: 43013518530000

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 3
AMENDED REPORT ☐

APPLICATION FOR PERMIT TO DRILL

1. WELL NAME and NUMBER Lejeune 1-17-3-2WH	
2. TYPE OF WORK DRILL NEW WELL ● REENTER P&A WELL ○ DEEPEN WELL ○	**3. FIELD OR WILDCAT** WILDCAT
4. TYPE OF WELL Oil Well Coalbed Methane Well: NO	**5. UNIT or COMMUNITIZATION AGREEMENT NAME**
6. NAME OF OPERATOR NEWFIELD PRODUCTION COMPANY	**7. OPERATOR PHONE** 435 646-4825
8. ADDRESS OF OPERATOR Rt 3 Box 3630 , Myton, UT, 84052	**9. OPERATOR E-MAIL** mcrozier@newfield.com
10. MINERAL LEASE NUMBER (FEDERAL, INDIAN, OR STATE) Patented	**11. MINERAL OWNERSHIP** FEDERAL ○ INDIAN ○ STATE ○ FEE ●
12. SURFACE OWNERSHIP FEDERAL ○ INDIAN ○ STATE ○ FEE ●	
13. NAME OF SURFACE OWNER (if box 12 = 'fee') Murray Sheep Ranch, LLC	**14. SURFACE OWNER PHONE (if box 12 = 'fee')** 435-823-1114
15. ADDRESS OF SURFACE OWNER (if box 12 = 'fee') P.O. Box 96, ,	**16. SURFACE OWNER E-MAIL (if box 12 = 'fee')**
17. INDIAN ALLOTTEE OR TRIBE NAME (if box 12 = 'INDIAN')	**18. INTEND TO COMMINGLE PRODUCTION FROM MULTIPLE FORMATIONS** YES ○ (Submit Commingling Application) NO ●
19. SLANT VERTICAL ○ DIRECTIONAL ○ HORIZONTAL ●	

20. LOCATION OF WELL	FOOTAGES	QTR-QTR	SECTION	TOWNSHIP	RANGE	MERIDIAN
LOCATION AT SURFACE	227 FNL 1115 FEL	NENE	17	3.0 S	2.0 W	U
Top of Uppermost Producing Zone	660 FNL 660 FEL	NENE	17	3.0 S	2.0 W	U
At Total Depth	660 FSL 660 FEL	SESE	17	3.0 S	2.0 W	U

21. COUNTY DUCHESNE	**22. DISTANCE TO NEAREST LEASE LINE (Feet)** 227	**23. NUMBER OF ACRES IN DRILLING UNIT** 40
	25. DISTANCE TO NEAREST WELL IN SAME POOL (Applied For Drilling or Completed) 1270	**26. PROPOSED DEPTH** MD: 13117 TVD: 8615
27. ELEVATION - GROUND LEVEL 5214	**28. BOND NUMBER** B001834	**29. SOURCE OF DRILLING WATER / WATER RIGHTS APPROVAL NUMBER IF APPLICABLE** 437478

Hole, Casing, and Cement Information

String	Hole Size	Casing Size	Length	Weight	Grade & Thread	Max Mud Wt.	Cement	Sacks	Yield	Weight
Cond	17.5	14	0 - 60	37.0	H-40 ST&C	0.0	Class G	35	1.17	15.8
Surf	12.25	9.625	0 - 2500	36.0	J-55 LT&C	8.3	Type III	216	3.33	11.0
							Type III	95	1.9	13.0
I1	8.75	7	0 - 9143	26.0	P-110 Other	11.5	35/65 Poz	263	2.59	11.5
							50/50 Poz	289	1.62	13.0
Prod	6.125	4.5	8217 - 13117	13.5	P-110 Other	11.5	No Used	0	0.0	0.0

ATTACHMENTS

VERIFY THE FOLLOWING ARE ATTACHED IN ACCORDANCE WITH THE UTAH OIL AND GAS CONSERVATION GENERAL RULES

☑ WELL PLAT OR MAP PREPARED BY LICENSED SURVEYOR OR ENGINEER	☑ COMPLETE DRILLING PLAN
☑ AFFIDAVIT OF STATUS OF SURFACE OWNER AGREEMENT (IF FEE SURFACE)	☐ FORM 5. IF OPERATOR IS OTHER THAN THE LEASE OWNER
☑ DIRECTIONAL SURVEY PLAN (IF DIRECTIONALLY OR HORIZONTALLY DRILLED)	☑ TOPOGRAPHICAL MAP

NAME Don Hamilton	**TITLE** Permitting Agent	**PHONE** 435 719-2018
SIGNATURE	**DATE** 11/07/2012	**EMAIL** starpoint@etv.net

API NUMBER ASSIGNED
43013518530000

APPROVAL

Permit Manager

RECEIVED: January 09, 2013

Newfield Production Company
1-17-3-2WH
Surface Hole Location: 227' FNL, 1115' FEL, Section 17, T3S, R2W
Bottom Hole Location: 660' FSL, 660' FEL, Section 17, T3S, R2W
Duchesne County, UT

Drilling Program

1. Formation Tops

Uinta	Surface
Green River	3,532'
Garden Gulch member	6,433'
Uteland Butte	8,729'
Lateral TD	8,615' TVD / 13,117' MD

2. Depth to Oil, Gas, Water, or Minerals

Base of moderately saline	4,420'	(water)
Green River	6,433' - 8,615'	(oil)

3. Pressure Control

Section	BOP Description
Surface	12-1/4" diverter
Interm/Prod	The BOP and related equipment shall meet the minimum requirements of Onshore Oil and Gas Order No. 2 for equipment and testing requirements, procedures, etc for a 5M system. A 5M BOP system will consist of 2 ram preventers (double or two singles) and an annular preventer (see attached diagram). A choke manifold rated to at least 5,000 psi will be used.

4. Casing

Description	Interval		Weight (ppf)	Grade	Coup	Pore Press @ Shoe	MW @ Shoe	Frac Grad @ Shoe	Safety Factors		
	Top	Bottom (TVD/MD)							Burst	Collapse	Tension
Conductor 14	0'	60'	37	H-40	Weld	--	--	--	--	--	--
									--	--	--
Surface 9 5/8	0'	2,500'	36	J-55	LTC	8.33	8.33	12	3,520	2,020	453,000
									2.51	2.54	5.03
Intermediate 7	0'	8,766' 9,143'	26	P-110	BTC	11	11.5	15	9,960	6,210	830,000
									2.41	1.42	3.49
Production 4 1/2	8,217'	8,615' 13,117'	13.5	P-110	BTC	11	11.5	--	12,410	10,670	422,000
									3.05	2.49	6.38

Assumptions:

Surface casing MASP = (frac gradient + 1.0 ppg) - (gas gradient)
Intermediate casing MASP = (reservoir pressure) - (gas gradient)

RECEIVED: November 07, 2012

Production casing MASP = (reservoir pressure) - (gas gradient)
All collapse calculations assume fully evacuated casing with a gas gradient
All tension calculations assume air weight of casing
Gas gradient = 0.1 psi/ft

All casing shall be new.
All casing strings shall have a minimum of 1 centralizer on each of the bottom 3 joints.

5. Cement

Job	Hole Size	Fill	Slurry Description	ft^3 / sacks	OH excess	Weight (ppg)	Yield (ft^3/sk)
Conductor	17 1/2	60'	Class G w/ 2% KCl + 0.25 lbs/sk Cello Flake	41 / 35	15%	15.8	1.17
Surface Lead	12 1/4	2,000'	Type III + .125 lbs/sk Cello Flakes	720 / 216	15%	11.0	3.33
Surface Tail	12 1/4	500'	Type III + .125 lbs/sk Cello Flakes	180 / 95	15%	13.0	1.9
Intermediate Lead	8 3/4	3,933'	Premium - 65% Class G / 35% Poz + 10% Bentonite	680 / 263	15%	11.5	2.59
Intermediate Tail	8 3/4	2,710'	50/50 Poz/Class G + 1% bentonite	469 / 289	15%	13.0	1.62
Production	6 1/8	--	Liner will not be cemented. It will be isolated with a liner top packer.	-- / --	--	--	--

The surface casing will be cemented to surface. In the event that cement does not reach surface during the primary cement job, a remedial job will be performed.

Actual cement volumes for the intermediate casing string will be calculated from an open hole caliper log, plus 15% excess.

The cement slurries will be adjusted for hole conditions and blend test results.

The production liner will be left uncemented. Individual frac stages will be isolated with open hole packers. A liner top hanger and packer will be installed 50' above KOP.

6. Type and Characteristics of Proposed Circulating Medium

Interval	Description
Surface - 2,500'	An air and/or fresh water system will be utilized. If an air rig is used, the blooie line discharge may be less than 100' from the wellbore in order to minimize location size. The blooie line is not equipped with an automatic igniter. The air compressor may be located less than 100' from the well bore due to the low possibility of combustion with the air/dust mixture. Water will be on location to be used as kill fluid, if necessary.
2,500' - TD	A water based mud system will be utilized. Hole stability may be improved with additions of KCl or a similar inhibitive substance. In order to control formation pressure the system will be weighted with additions of bentonite, and

RECEIVED: November 07, 2012

if conditions warrant, with barite.
Anticipated maximum mud weight is 11.5 ppg.

7. Logging, Coring, and Testing

Logging: A dual induction, gamma ray, and caliper log will be run in the intermediate section from the top of the curve to the base of the surface casing. A compensated neutron/formation density log will be run in the intermediate section from the top of the curve to the top of the Garden Gulch formation. A cement bond log will be run from the top of the curve to the cement top behind the intermediate casing.

Cores: As deemed necessary.

DST: There are no DST's planned for this well.

8. Anticipated Abnormal Pressure or Temperature

Maximum anticipated bottomhole pressure will be approximately equal to total depth (feet) multiplied by a 0.57 psi/ft gradient.

8,615' x 0.57 psi/ft = 4928 psi

No abnormal temperature is expected. No H_2S is expected.

9. Other Aspects

An 8-3/4" vertical hole will be drilled to a kick off point of 8,267' .
Directional tools will then be used to build to 92.30 degrees inclination.
The 7" intermediate casing string will be set once the well is landed horizontally in the target zone.

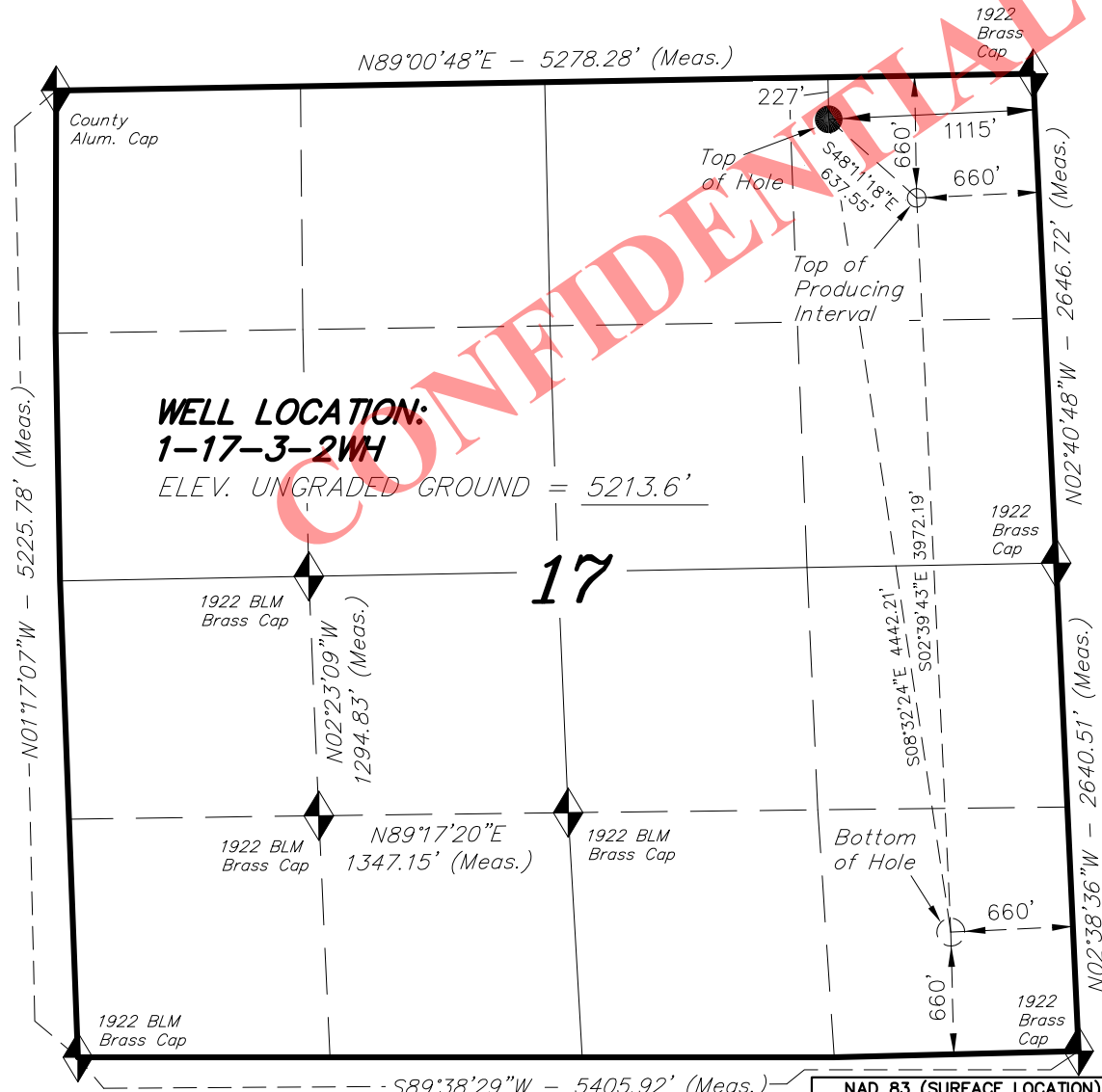
The lateral will be drilled to the bottomhole location shown on the plat.
A liner with a system of open hole packers will be used to provide multi-stage frac isolation in the lateral. The top of the liner will be place 50' above KOP and will be isolated with a liner top packer.

Newfield requests the following variances from Onshore Order #2:
- Variance from Onshoer Order #2, III.E.1
  Refer to Newfield Production Company Standard Operating Practices "Ute Tribal Green River Development Program" paragraph 9.0

RECEIVED: November 07, 2012

API Well Number: 43013518530000

T3S, R2W, U.S.B.&M.



◆ = SECTION CORNERS LOCATED

BASIS OF ELEV; Elevations are based on an N.G.S. OPUS Correction. LOCATION: LAT. 40°04'09.56" LONG. 110°00'43.28" (Tristate Aluminum Cap) Elev. 5281.57'

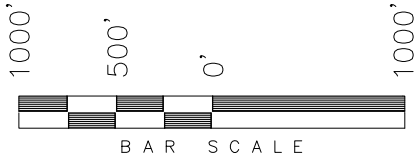
NAD 83 (SURFACE LOCATION)
LATITUDE = 40°13'42.81" LONGITUDE = 110°07'41.40"
NAD 27 (SURFACE LOCATION)
LATITUDE = 40°13'42.96" LONGITUDE = 110°07'38.86"

NAD 83 (TOP OF PROD. INTERVAL)	NAD 83 (BOTTOM HOLE LOCATION)
LATITUDE = 40°13'38.54" LONGITUDE = 110°07'35.36"	LATITUDE = 40°12'59.32" LONGITUDE = 110°07'33.77"
NAD 27 (TOP OF PROD. INTERVAL)	**NAD 27 (BOTTOM HOLE LOCATION)**
LATITUDE = 40°13'38.69" LONGITUDE = 110°07'32.81"	LATITUDE = 40°12'59.47" LONGITUDE = 110°07'31.22"

NEWFIELD EXPLORATION COMPANY

WELL LOCATION, 1-17-3-2WH, LOCATED AS SHOWN IN THE NE 1/4 NE 1/4 OF SECTION 17, T3S, R2W, U.S.B.&M. DUCHESNE COUNTY, UTAH.

TARGET BOTTOM HOLE, 1-17-3-2WH, LOCATED AS SHOWN IN THE SE 1/4 SE 1/4 OF SECTION 17, T3S, R2W, U.S.B.&M. DUCHESNE COUNTY, UTAH.



NOTES:

1. Well footages are measured at right angles to the Section Lines.
2. Bearings are based on Global Positioning Satellite observations.

THIS IS TO CERTIFY THAT THE ABOVE PLAT WAS PREPARED FROM FIELD NOTES OF ACTUAL SURVEYS MADE BY ME OR UNDER MY SUPERVISION AND THAT THE SAME ARE TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.

REGISTERED LAND SURVEYOR
No. 189377
08-01-12
STACY W. STEWART
STATE OF UTAH

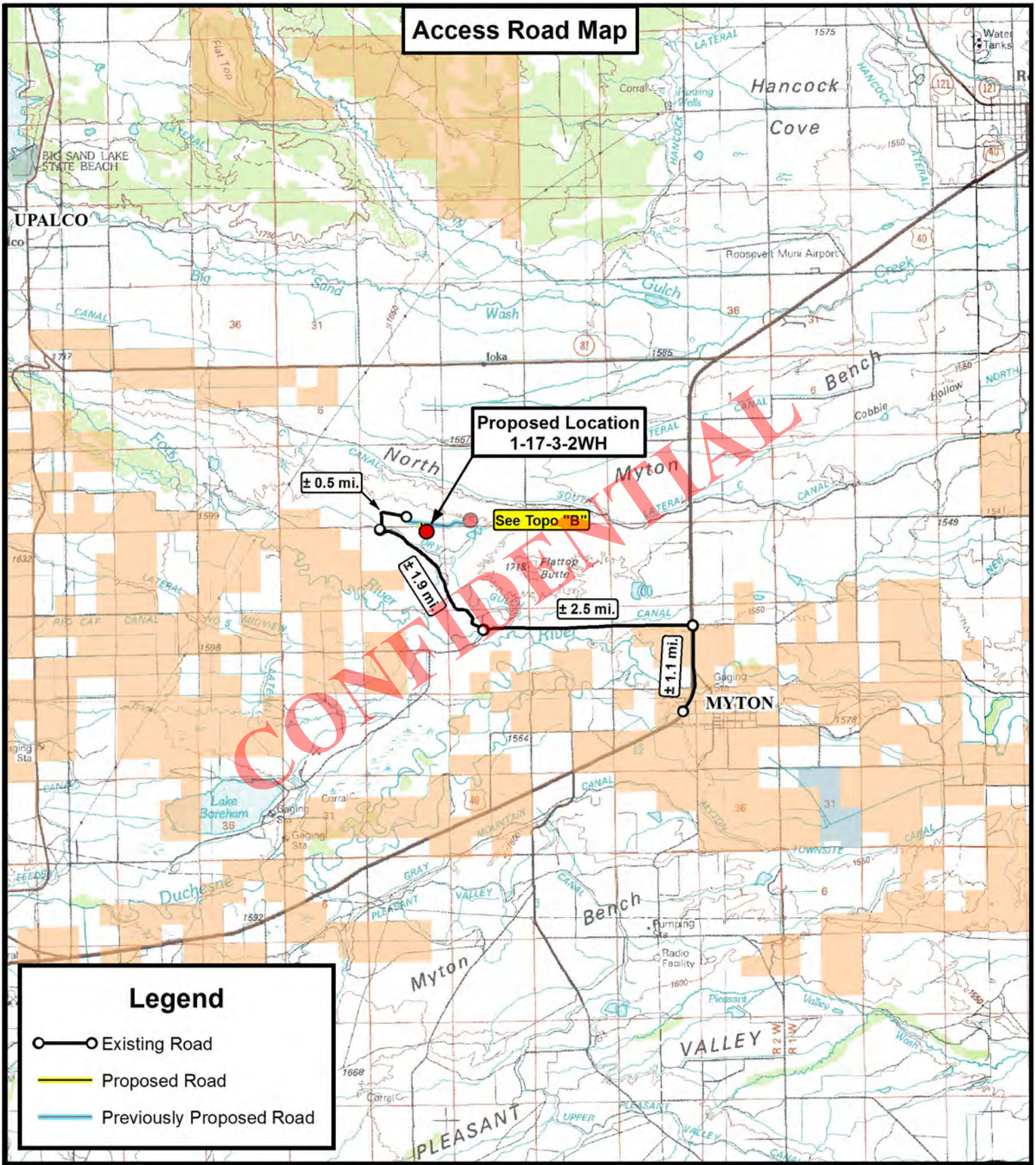
REGISTERED LAND SURVEYOR
REGISTRATION No. 189377
STATE OF UTAH

TRI STATE LAND SURVEYING & CONSULTING
180 NORTH VERNAL AVE. – VERNAL, UTAH 84078
(435) 781-2501

DATE SURVEYED: 07-27-12	SURVEYED BY: Q.M.	VERSION:
DATE DRAWN: 08-01-12	DRAWN BY: M.W.	V1
REVISED:	SCALE: 1" = 1000'	

RECEIVED: November 07, 2012

API Well Number: 43013518530000



Tri State Land Surveying, Inc.
180 NORTH VERNAL AVE. VERNAL, UTAH 84078
P: (435) 781-2501
F: (435) 781-2518

N

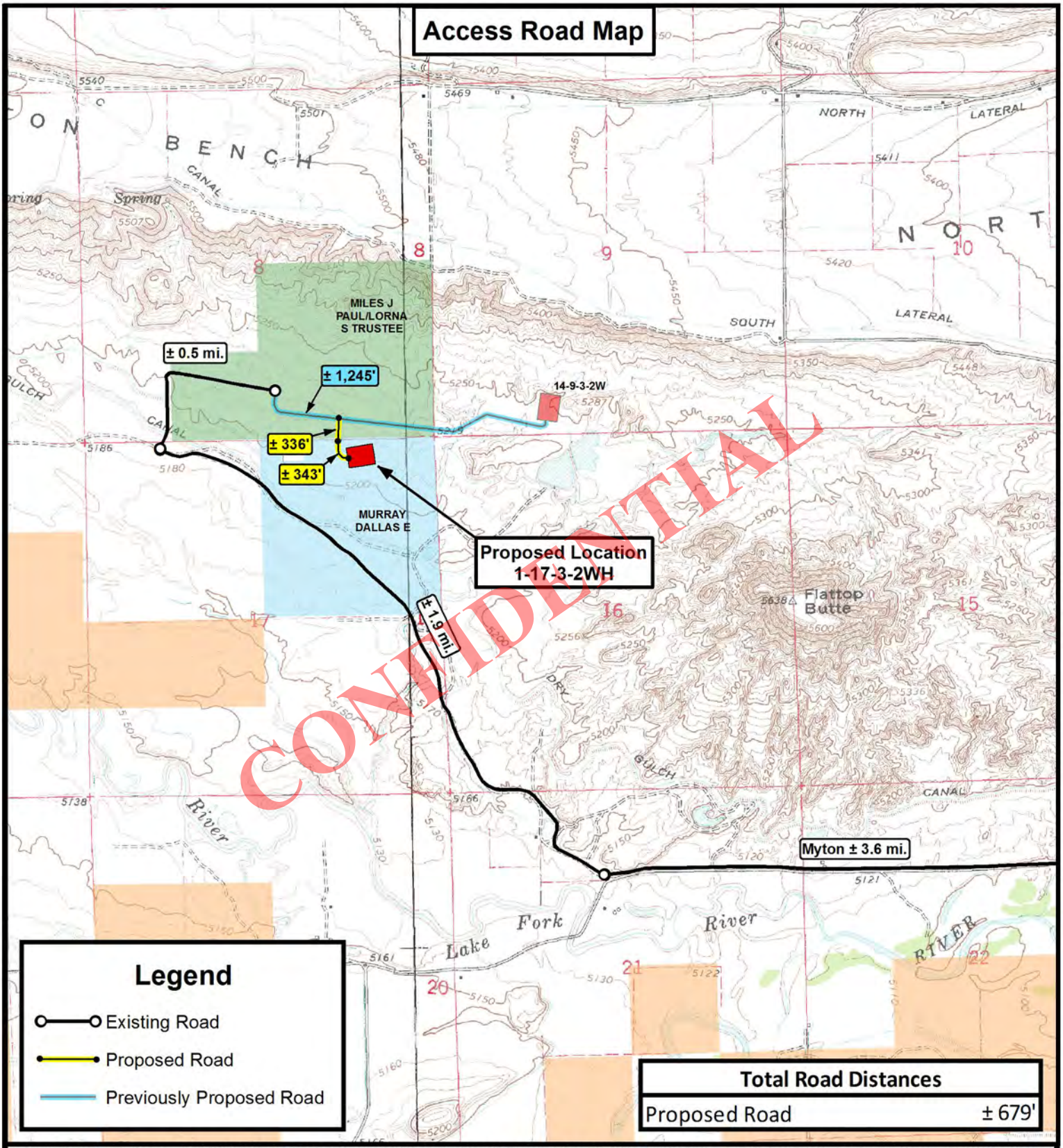
NEWFIELD EXPLORATION COMPANY
1-17-3-2WH
SEC. 17, T3S, R2W, U.S.B.&M.
Duchesne County, UT.

DRAWN BY:	A.P.C.	REVISED:	VERSION:
DATE:	08-01-2012		V1
SCALE:	1:100,000		

TOPOGRAPHIC MAP

SHEET A

API Well Number: 43013518530000



THE PARCEL INFORMATION SHOWN HAS NOT BEEN SURVEYED BY TRI-STATE LAND SURVEYING, INC. - TRI-STATE DOES NOT WARRANTY PROPERTY PARCEL DATA OR ANY ASSOCIATED INFORMATION. A PROPERTY SURVEY IS REQUIRED TO DETERMINE THE ACTUAL LOCATION OF PROPERTY LINES AND SHOW ACCURATE DISTANCES ACROSS PARCELS.

Tri State Land Surveying, Inc.
180 NORTH VERNAL AVE. VERNAL, UTAH 84078
P: (435) 781-2501
F: (435) 781-2518

N

NEWFIELD EXPLORATION COMPANY
1-17-3-2WH
SEC. 17, T3S, R2W, U.S.B.&M.
Duchesne County, UT.

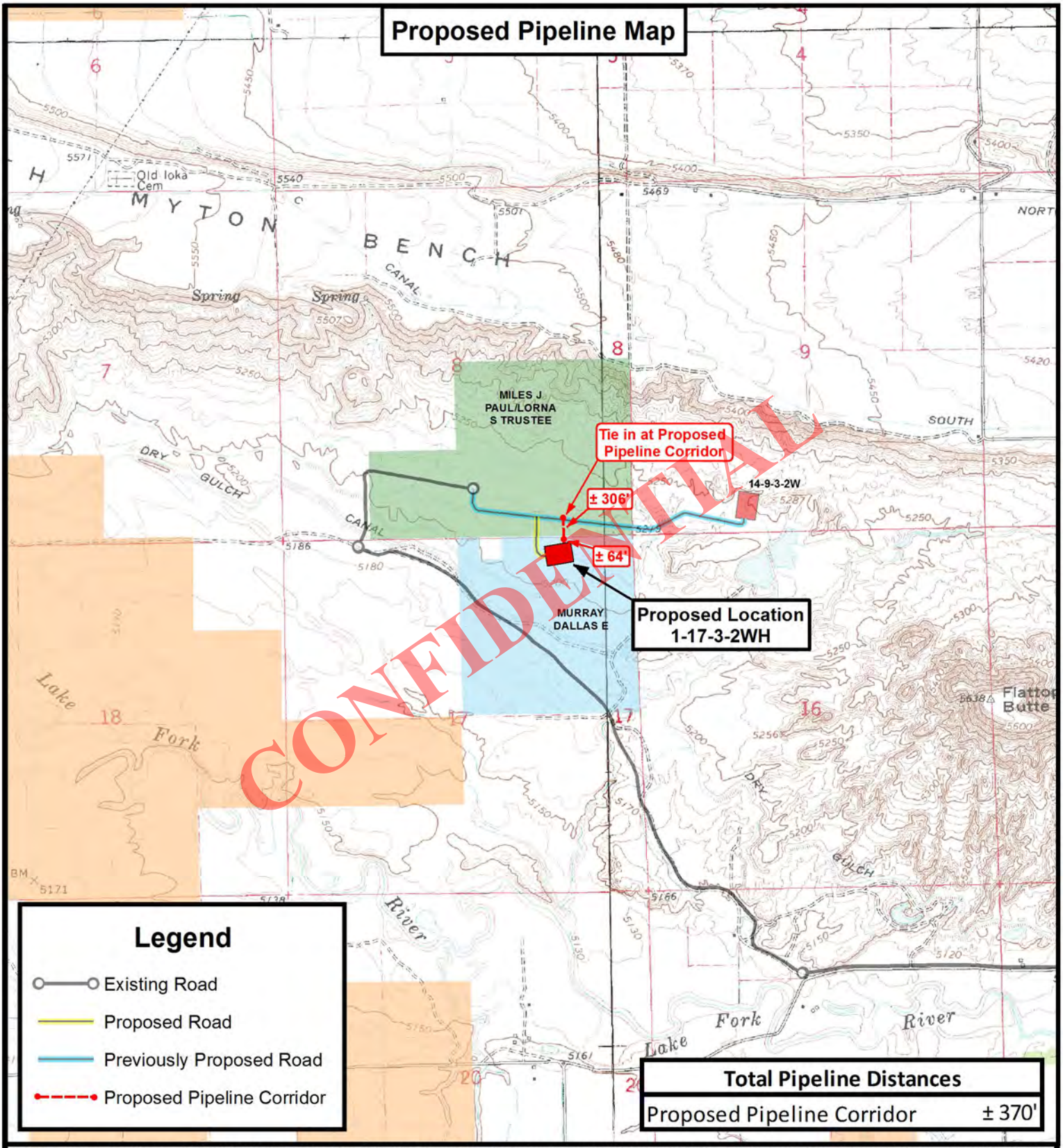
DRAWN BY:	A.P.C.	REVISED:	VERSION:
DATE:	08-01-2012		V1
SCALE:	1 " = 2,000 '		

TOPOGRAPHIC MAP

SHEET B

API Well Number: 43013518530000

Proposed Pipeline Map



Legend

- Existing Road
- Proposed Road
- Previously Proposed Road
- Proposed Pipeline Corridor

Total Pipeline Distances	
Proposed Pipeline Corridor	± 370'

THE PARCEL INFORMATION SHOWN HAS NOT BEEN SURVEYED BY TRI-STATE LAND SURVEYING, INC. - TRI-STATE DOES NOT WARRANTY PROPERTY PARCEL DATA OR ANY ASSOCIATED INFORMATION. A PROPERTY SURVEY IS REQUIRED TO DETERMINE THE ACTUAL LOCATION OF PROPERTY LINES AND SHOW ACCURATE DISTANCES ACROSS PARCELS.

Tri State Land Surveying, Inc.
180 NORTH VERNAL AVE. VERNAL, UTAH 84078
P: (435) 781-2501
F: (435) 781-2518

N

NEWFIELD EXPLORATION COMPANY

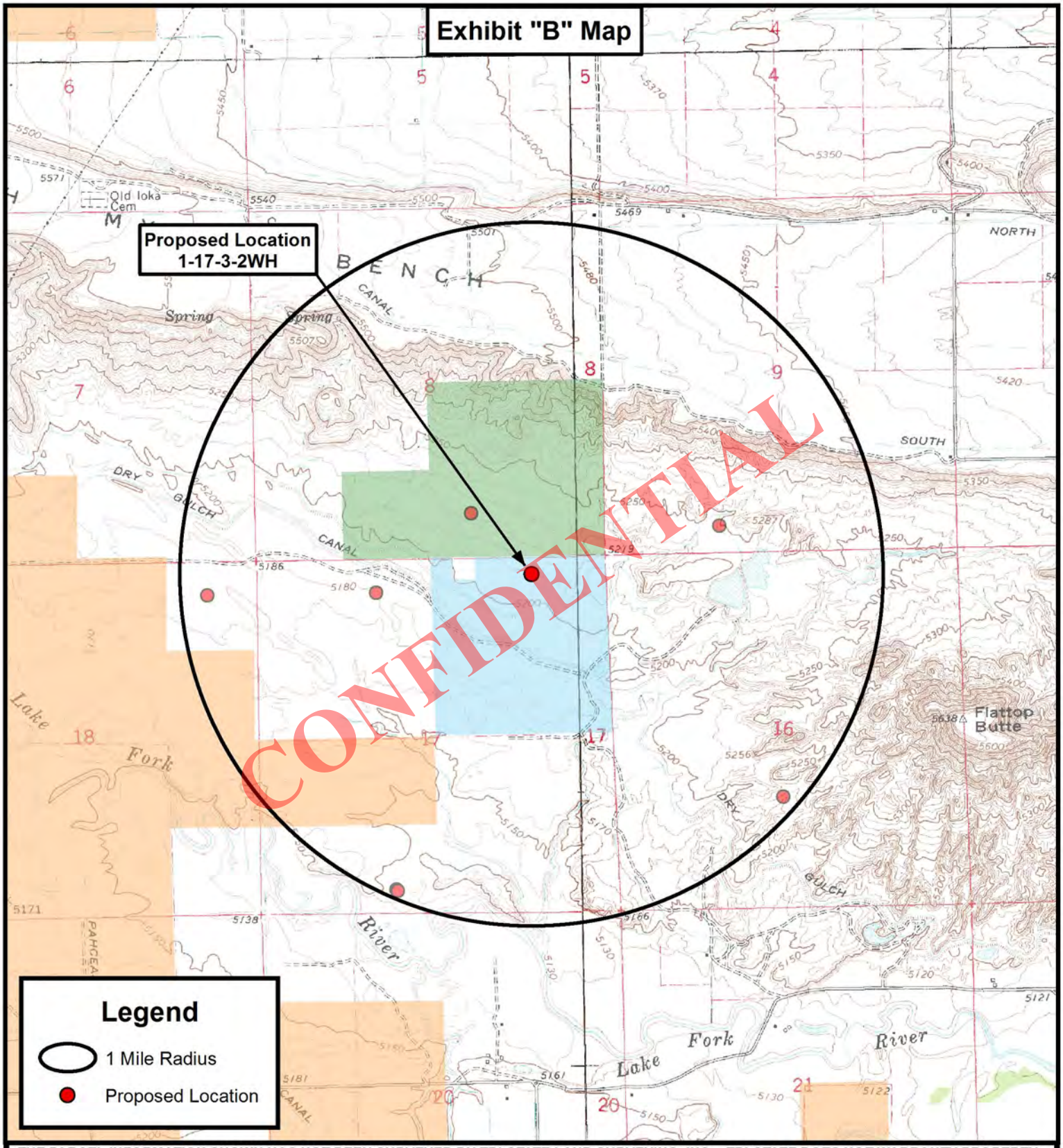
1-17-3-2WH
SEC. 17, T3S, R2W, U.S.B.&M.
Duchesne County, UT.

DRAWN BY:	A.P.C.	REVISED:	VERSION:
DATE:	08-01-2012		V1
SCALE:	1 " = 2,000 '		

TOPOGRAPHIC MAP

SHEET C

API Well Number: 43013518530000



THE PARCEL INFORMATION SHOWN HAS NOT BEEN SURVEYED BY TRI-STATE LAND SURVEYING, INC. - TRI-STATE DOES NOT WARRANTY PROPERTY PARCEL DATA OR ANY ASSOCIATED INFORMATION. A PROPERTY SURVEY IS REQUIRED TO DETERMINE THE ACTUAL LOCATION OF PROPERTY LINES AND SHOW ACCURATE DISTANCES ACROSS PARCELS.

Tri State Land Surveying, Inc.
180 NORTH VERNAL AVE. VERNAL, UTAH 84078
P: (435) 781-2501
F: (435) 781-2518

N

NEWFIELD EXPLORATION COMPANY

1-17-3-2WH
SEC. 17, T3S, R2W, U.S.B.&M.
Duchesne County, UT.

DRAWN BY:	A.P.C.	REVISED:	VERSION:
DATE:	08-01-2012		V1
SCALE:	1 " = 2,000 '		

TOPOGRAPHIC MAP

SHEET D

Newfield Exploration Company

Duchesne County, UT
Sec. 17-T3S-R2W
1-17-3-2WH

Plan A Rev 0

Plan: Proposal Plan A Rev 0

Sperry Drilling Services

Proposal Report

26 October, 2012

Well Coordinates: 7,254,915.78 N, 2,023,424.40 E (40° 13' 42.81" N, 110° 07' 41.40" W)
Ground Level: 5,213.59 ft

Local Coordinate Origin:	Centered on Well 1-17-3-2WH
Viewing Datum:	WELL-RKB @ 5231.59ft (Original Well Elev)
TVDs to System:	N
North Reference:	True
Unit System:	API - US Survey Feet - Custom

Geodetic Scale Factor Applied
Version: 2003.16 Build: 43I

HALLIBURTON

API Well Number: 43013518530000

Project: Duchesne County, UT
Site: Sec. 17-T3S-R2W
Well: 1-17-3-2WH
Wellbore: Plan A Rev 0
Design: Proposal Plan A Rev 0

Newfield Exploration Company

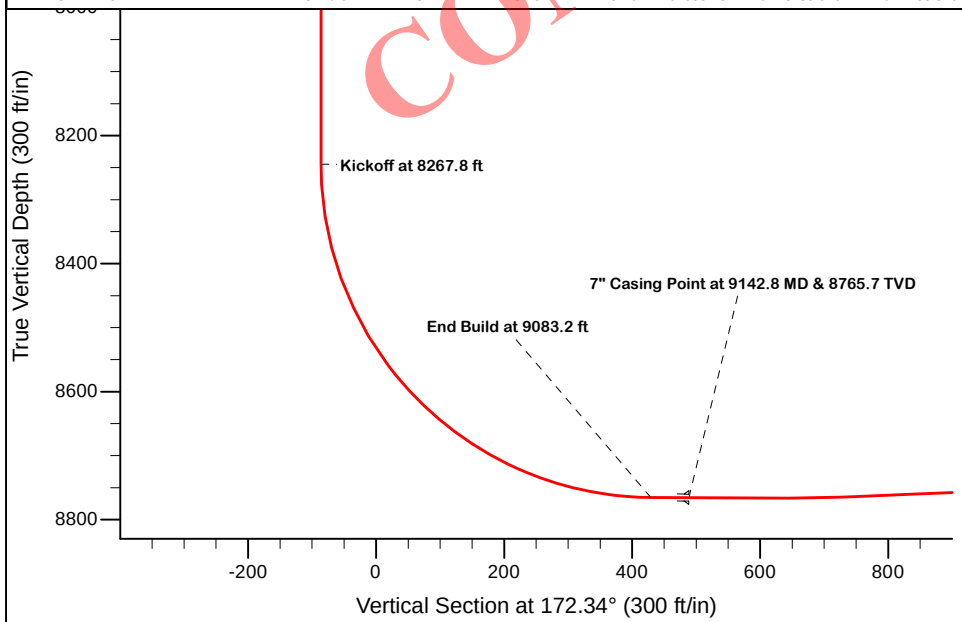
HALLIBURTON
Sperry Drilling

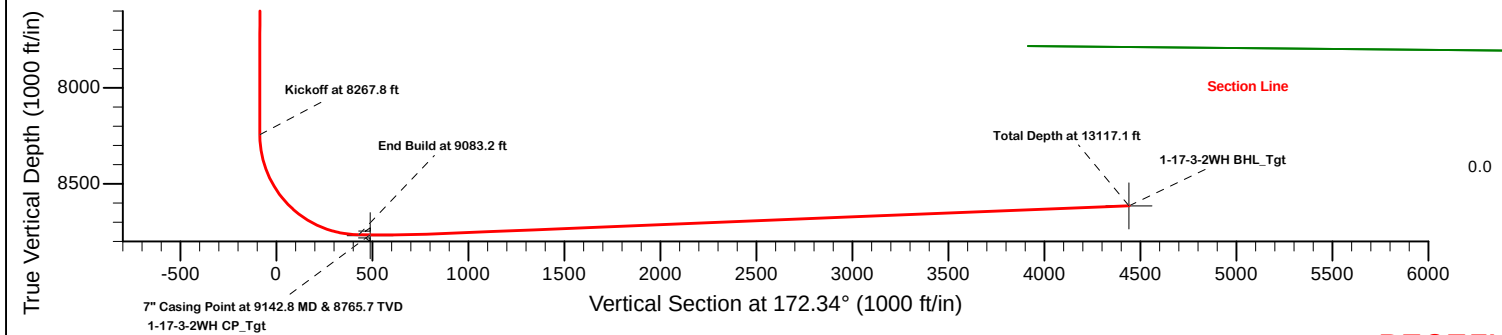
SECTION DETAILS

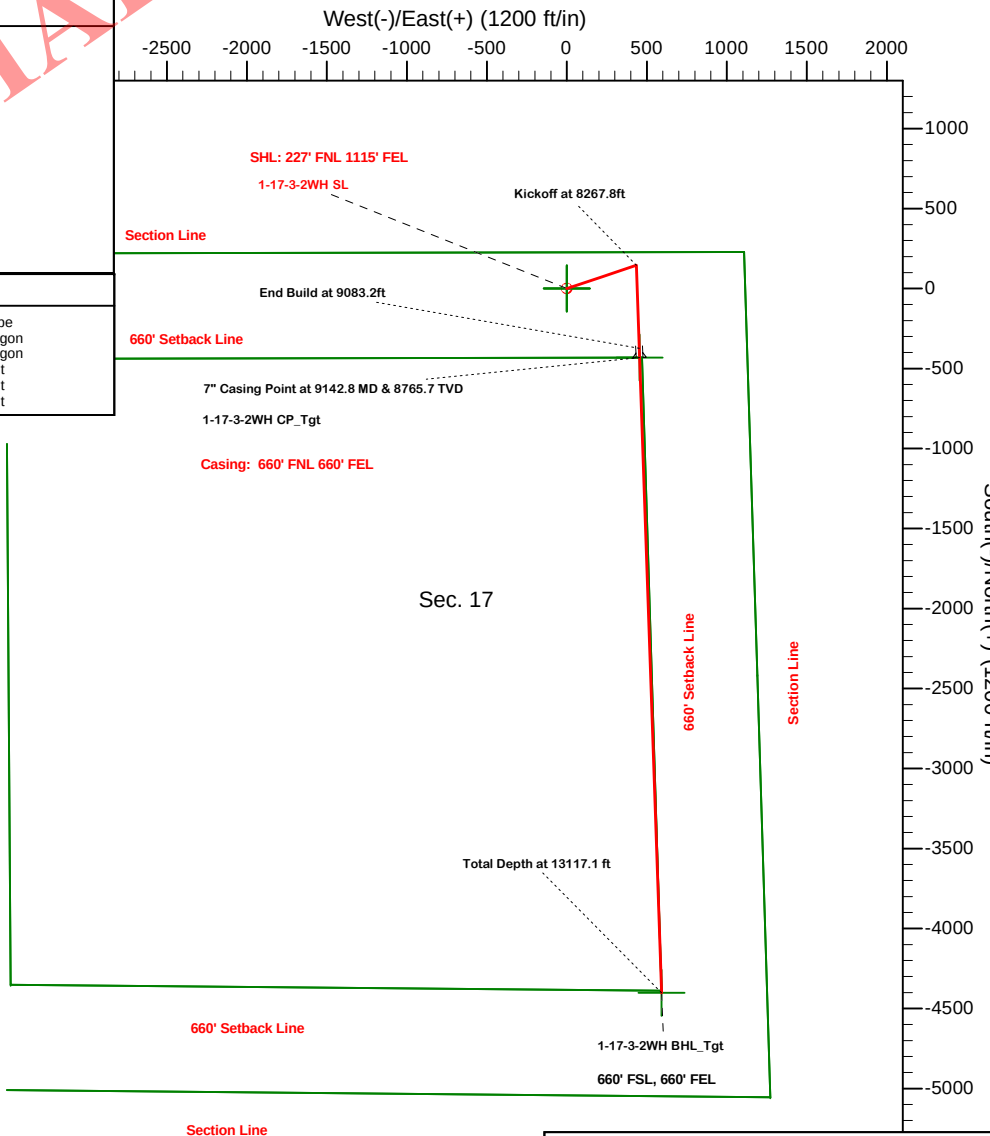
Sec	MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSect	Target
1	0.0	0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.0	
2	3000.0	0.00	0.00	3000.0	0.0	0.0	0.00	0.00	0.0	
3	3400.0	6.00	71.50	3399.3	6.6	19.8	1.50	71.50	-3.9	
4	7380.0	6.00	71.50	7357.5	138.6	414.4	0.00	0.00	-82.2	
5	7780.0	0.00	0.00	7756.7	145.3	434.2	1.50	180.00	-86.1	
6	8267.8	0.00	0.00	8244.5	145.3	434.2	0.00	0.00	-86.1	
7	9083.2	89.70	177.98	8765.4	-372.5	452.4	11.00	177.98	429.5	1-17-3-2WH CP
8	9142.8	89.70	177.98	8765.7	-432.1	454.5	0.00	0.00	488.8	1-17-3-2WH CP
9	9292.8	89.70	177.98	8766.5	-582.0	459.8	0.00	0.00	638.1	
10	9379.5	92.30	178.02	8764.9	-668.6	462.8	3.00	0.76	724.3	1-17-3-2WH BHL
11	13117.1	92.30	178.02	8615.0	-4400.9	591.9	0.00	0.00	4440.6	1-17-3-2WH BHL

WELLBORE TARGET DETAILS (MAP CO-ORDINATES AND LAT/LONG)

Name	TVD	+N/-S	+E/-W	Northing	Easting	Latitude	Longitude	Shape
1-17-3-2WH Section Lines	0.0	0.0	0.0	2211302.75	616740.99	40° 13' 42.810 N	110° 7' 41.400 W	Polygon
1-17-3-2WH Setback Lines	0.0	0.0	0.0	2211302.75	616740.99	40° 13' 42.810 N	110° 7' 41.400 W	Polygon
1-17-3-2WH SL	0.0	0.0	0.0	2211302.75	616740.99	40° 13' 42.810 N	110° 7' 41.400 W	Point
1-17-3-2WH BHL	8615.0	-4400.9	591.9	2209964.37	616941.94	40° 12' 59.320 N	110° 7' 33.770 W	Point
1-17-3-2WH CP	8770.0	-432.1	454.5	2211173.20	616881.52	40° 13' 38.540 N	110° 7' 35.540 W	Point







WELL DETAILS: 1-17-3-2WH

Ground Level: 5213.6

Northing	Easting	Latitude	Longitude
2211302.75	616740.99	40° 13' 42.810 N	110° 7' 41.400 W

0.0

Plan: Proposal Plan A Rev 0 (1-17-3-2WH/Plan A Rev 0)

Created By: Lacy Taylor Date: 10/26/2012

Checked:_____ Date: _____

RECEIVED: November 07, 2012

HALLIBURTON

Plan Report for 1-17-3-2WH - Proposal Plan A Rev 0

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)	Toolface Azimuth (°)
0.00	0.00	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100.00	0.00	0.000	100.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.000	200.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00	0.00	0.000	300.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
400.00	0.00	0.000	400.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
500.00	0.00	0.000	500.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
600.00	0.00	0.000	600.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
700.00	0.00	0.000	700.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
800.00	0.00	0.000	800.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
900.00	0.00	0.000	900.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.000	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,100.00	0.00	0.000	1,100.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,200.00	0.00	0.000	1,200.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,300.00	0.00	0.000	1,300.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,400.00	0.00	0.000	1,400.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,500.00	0.00	0.000	1,500.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,600.00	0.00	0.000	1,600.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,700.00	0.00	0.000	1,700.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,800.00	0.00	0.000	1,800.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1,900.00	0.00	0.000	1,900.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,000.00	0.00	0.000	2,000.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,100.00	0.00	0.000	2,100.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,200.00	0.00	0.000	2,200.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,300.00	0.00	0.000	2,300.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,400.00	0.00	0.000	2,400.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,500.00	0.00	0.000	2,500.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,600.00	0.00	0.000	2,600.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,700.00	0.00	0.000	2,700.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,800.00	0.00	0.000	2,800.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,900.00	0.00	0.000	2,900.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2,999.99	0.00	0.000	2,999.99	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3,100.00	1.50	71.500	3,099.99	0.42	1.24	-0.25	1.50	1.50	0.00	71.50
3,200.00	3.00	71.500	3,199.91	1.66	4.96	-0.98	1.50	1.50	0.00	0.00
3,300.00	4.50	71.500	3,299.69	3.74	11.17	-2.21	1.50	1.50	0.00	0.00
3,399.99	6.00	71.500	3,399.26	6.64	19.84	-3.94	1.50	1.50	0.00	0.00
3,500.00	6.00	71.500	3,498.72	9.96	29.76	-5.90	0.00	0.00	0.00	0.00
3,600.00	6.00	71.500	3,598.17	13.27	39.67	-7.87	0.00	0.00	0.00	0.00
3,700.00	6.00	71.500	3,697.63	16.59	49.58	-9.83	0.00	0.00	0.00	0.00
3,800.00	6.00	71.500	3,797.08	19.91	59.49	-11.80	0.00	0.00	0.00	0.00
3,900.00	6.00	71.500	3,896.53	23.22	69.41	-13.76	0.00	0.00	0.00	0.00
4,000.00	6.00	71.500	3,995.98	26.54	79.32	-15.73	0.00	0.00	0.00	0.00
4,100.00	6.00	71.500	4,095.43	29.86	89.23	-17.70	0.00	0.00	0.00	0.00
4,200.00	6.00	71.500	4,194.89	33.17	99.15	-19.66	0.00	0.00	0.00	0.00
4,300.00	6.00	71.500	4,294.34	36.49	109.06	-21.63	0.00	0.00	0.00	0.00
4,400.00	6.00	71.500	4,393.79	39.81	118.97	-23.59	0.00	0.00	0.00	0.00
4,500.00	6.00	71.500	4,493.24	43.12	128.88	-25.56	0.00	0.00	0.00	0.00
4,600.00	6.00	71.500	4,592.70	46.44	138.80	-27.53	0.00	0.00	0.00	0.00
4,700.00	6.00	71.500	4,692.15	49.76	148.71	-29.49	0.00	0.00	0.00	0.00
4,800.00	6.00	71.500	4,791.60	53.07	158.62	-31.46	0.00	0.00	0.00	0.00
4,900.00	6.00	71.500	4,891.05	56.39	168.53	-33.42	0.00	0.00	0.00	0.00
5,000.00	6.00	71.500	4,990.50	59.71	178.45	-35.39	0.00	0.00	0.00	0.00
5,100.00	6.00	71.500	5,089.96	63.02	188.36	-37.35	0.00	0.00	0.00	0.00
5,200.00	6.00	71.500	5,189.41	66.34	198.27	-39.32	0.00	0.00	0.00	0.00
5,300.00	6.00	71.500	5,288.86	69.66	208.19	-41.29	0.00	0.00	0.00	0.00
5,400.00	6.00	71.500	5,388.31	72.97	218.10	-43.25	0.00	0.00	0.00	0.00
5,500.00	6.00	71.500	5,487.77	76.29	228.01	-45.22	0.00	0.00	0.00	0.00
5,600.00	6.00	71.500	5,587.22	79.61	237.92	-47.18	0.00	0.00	0.00	0.00
5,700.00	6.00	71.500	5,686.67	82.92	247.84	-49.15	0.00	0.00	0.00	0.00
5,800.00	6.00	71.500	5,786.12	86.24	257.75	-51.11	0.00	0.00	0.00	0.00

RECEIVED: November 07, 2012

HALLIBURTON

Plan Report for 1-17-3-2WH - Proposal Plan A Rev 0

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)	Toolface Azimuth (°)
5,900.00	6.00	71.500	5,885.57	89.56	267.66	-53.08	0.00	0.00	0.00	0.00
6,000.00	6.00	71.500	5,985.03	92.87	277.57	-55.05	0.00	0.00	0.00	0.00
6,100.00	6.00	71.500	6,084.48	96.19	287.49	-57.01	0.00	0.00	0.00	0.00
6,200.00	6.00	71.500	6,183.93	99.51	297.40	-58.98	0.00	0.00	0.00	0.00
6,300.00	6.00	71.500	6,283.38	102.83	307.31	-60.94	0.00	0.00	0.00	0.00
6,400.00	6.00	71.500	6,382.83	106.14	317.22	-62.91	0.00	0.00	0.00	0.00
6,500.00	6.00	71.500	6,482.29	109.46	327.14	-64.88	0.00	0.00	0.00	0.00
6,600.00	6.00	71.500	6,581.74	112.78	337.05	-66.84	0.00	0.00	0.00	0.00
6,700.00	6.00	71.500	6,681.19	116.09	346.96	-68.81	0.00	0.00	0.00	0.00
6,800.00	6.00	71.500	6,780.64	119.41	356.88	-70.77	0.00	0.00	0.00	0.00
6,900.00	6.00	71.500	6,880.10	122.73	366.79	-72.74	0.00	0.00	0.00	0.00
7,000.00	6.00	71.500	6,979.55	126.04	376.70	-74.70	0.00	0.00	0.00	0.00
7,100.00	6.00	71.500	7,079.00	129.36	386.61	-76.67	0.00	0.00	0.00	0.00
7,200.00	6.00	71.500	7,178.45	132.68	396.53	-78.64	0.00	0.00	0.00	0.00
7,300.00	6.00	71.500	7,277.90	135.99	406.44	-80.60	0.00	0.00	0.00	0.00
7,379.99	6.00	71.500	7,357.45	138.65	414.37	-82.17	0.00	0.00	0.00	0.00
7,400.00	5.70	71.500	7,377.36	139.29	416.30	-82.56	1.50	-1.50	0.00	180.00
7,500.00	4.20	71.500	7,476.99	142.03	424.48	-84.18	1.50	-1.50	0.00	180.00
7,600.00	2.70	71.500	7,576.80	143.94	430.19	-85.31	1.50	-1.50	0.00	180.00
7,700.00	1.20	71.500	7,676.74	145.02	433.42	-85.95	1.50	-1.50	0.00	180.00
7,779.98	0.00	0.000	7,756.72	145.28	434.21	-86.11	1.50	-1.50	0.00	-180.00
7,800.00	0.00	0.000	7,776.74	145.28	434.21	-86.11	0.00	0.00	0.00	0.00
7,900.00	0.00	0.000	7,876.74	145.28	434.21	-86.11	0.00	0.00	0.00	0.00
8,000.00	0.00	0.000	7,976.74	145.28	434.21	-86.11	0.00	0.00	0.00	0.00
8,100.00	0.00	0.000	8,076.74	145.28	434.21	-86.11	0.00	0.00	0.00	0.00
8,200.00	0.00	0.000	8,176.74	145.28	434.21	-86.11	0.00	0.00	0.00	0.00
8,267.75	0.00	0.000	8,244.48	145.28	434.21	-86.11	0.00	0.00	0.00	0.00
8,267.78	0.00	177.985	8,244.52	145.28	434.21	-86.11	0.00	0.00	0.00	177.98
KOP at 8267.8 MD & 8244.5 TVD										
8,300.00	3.55	177.985	8,276.72	144.29	434.25	-85.12	11.01	11.01	0.00	177.98
8,350.00	9.05	177.985	8,326.39	138.81	434.44	-79.66	11.00	11.00	0.00	0.00
8,400.00	14.55	177.985	8,375.32	128.60	434.80	-69.49	11.00	11.00	0.00	0.00
8,450.00	20.05	177.985	8,423.04	113.74	435.32	-54.70	11.00	11.00	0.00	0.00
8,500.00	25.55	177.985	8,469.12	94.39	436.00	-35.43	11.00	11.00	0.00	0.00
8,550.00	31.05	177.985	8,513.12	70.71	436.83	-11.85	11.00	11.00	0.00	0.00
8,600.00	36.55	177.985	8,554.66	42.92	437.81	15.82	11.00	11.00	0.00	0.00
8,650.00	42.05	177.985	8,593.34	11.29	438.93	47.32	11.00	11.00	0.00	0.00
8,700.00	47.55	177.985	8,628.80	-23.91	440.16	82.37	11.00	11.00	0.00	0.00
8,750.00	53.05	177.985	8,660.73	-62.34	441.52	120.63	11.00	11.00	0.00	0.00
8,800.00	58.55	177.985	8,688.83	-103.65	442.97	161.77	11.00	11.00	0.00	0.00
8,850.00	64.05	177.985	8,712.83	-147.46	444.51	205.40	11.00	11.00	0.00	0.00
8,872.51	66.52	177.985	8,722.24	-167.89	445.23	225.74	11.00	11.00	0.00	0.00
Uteland Butte										
8,900.00	69.55	177.985	8,732.52	-193.37	446.13	251.11	11.00	11.00	0.00	0.00
8,950.00	75.05	177.985	8,747.72	-240.96	447.80	298.50	11.00	11.00	0.00	0.00
9,000.00	80.55	177.985	8,758.28	-289.78	449.52	347.11	11.00	11.00	0.00	0.00
9,050.00	86.05	177.985	8,764.11	-339.39	451.26	396.51	11.00	11.00	0.00	0.00
9,083.18	89.70	177.985	8,765.35	-372.52	452.43	429.50	11.00	11.00	0.00	0.00
End of Build at 9083.2 MD & 8765.4 TVD										
9,083.20	89.70	177.985	8,765.35	-372.54	452.43	429.52	11.00	11.00	0.00	0.00
9,100.00	89.70	177.985	8,765.43	-389.33	453.02	446.24	0.00	0.00	0.00	0.00
9,142.78	89.70	177.985	8,765.66	-432.08	454.53	488.81	0.00	0.00	0.00	0.00
7" Casing Point at 9142.8 MD & 8765.7 TVD - 7"										
9,142.79	89.70	177.985	8,765.66	-432.09	454.53	488.82	0.01	0.00	0.00	0.00
9,142.82	89.70	177.985	8,765.66	-432.12	454.53	488.85	0.00	0.00	0.00	0.00
1-17-3-2WH CP - 1-17-3-2WH CP										
9,200.00	89.70	177.985	8,765.96	-489.26	456.54	545.75	0.00	0.00	0.00	0.00
9,208.24	89.70	177.985	8,766.00	-497.50	456.83	553.95	0.00	0.00	0.00	0.00
Uteland Butte 'C' (Landing Target)										

HALLIBURTON

Plan Report for 1-17-3-2WH - Proposal Plan A Rev 0

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)	Toolface Azimuth (°)
9,274.36	89.70	177.985	8,766.35	-563.57	459.15	619.75	0.00	0.00	0.00	0.00
Intermediate Casing Point										
9,292.79	89.70	177.985	8,766.44	-582.00	459.80	638.09	0.00	0.00	0.00	0.00
9,300.00	89.92	177.988	8,766.47	-589.20	460.05	645.27	3.00	3.00	0.04	0.76
9,379.47	92.30	178.019	8,764.93	-668.60	462.82	724.32	3.00	3.00	0.04	0.76
9,400.00	92.30	178.019	8,764.11	-689.10	463.53	744.74	0.00	0.00	0.00	0.00
9,500.00	92.30	178.019	8,760.09	-788.96	466.99	844.17	0.00	0.00	0.00	0.00
9,600.00	92.30	178.019	8,756.08	-888.82	470.44	943.60	0.00	0.00	0.00	0.00
9,700.00	92.30	178.019	8,752.07	-988.68	473.89	1,043.03	0.00	0.00	0.00	0.00
9,800.00	92.30	178.019	8,748.05	-1,088.54	477.35	1,142.46	0.00	0.00	0.00	0.00
9,900.00	92.30	178.019	8,744.04	-1,188.40	480.80	1,241.88	0.00	0.00	0.00	0.00
10,000.00	92.30	178.019	8,740.03	-1,288.26	484.25	1,341.31	0.00	0.00	0.00	0.00
10,100.00	92.30	178.019	8,736.01	-1,388.12	487.71	1,440.74	0.00	0.00	0.00	0.00
10,200.00	92.30	178.019	8,732.00	-1,487.98	491.16	1,540.17	0.00	0.00	0.00	0.00
10,300.00	92.30	178.019	8,727.99	-1,587.84	494.62	1,639.60	0.00	0.00	0.00	0.00
10,400.00	92.30	178.019	8,723.98	-1,687.70	498.07	1,739.03	0.00	0.00	0.00	0.00
10,500.00	92.30	178.019	8,719.96	-1,787.56	501.52	1,838.46	0.00	0.00	0.00	0.00
10,600.00	92.30	178.019	8,715.95	-1,887.42	504.98	1,937.89	0.00	0.00	0.00	0.00
10,700.00	92.30	178.019	8,711.94	-1,987.28	508.43	2,037.32	0.00	0.00	0.00	0.00
10,800.00	92.30	178.019	8,707.92	-2,087.14	511.88	2,136.75	0.00	0.00	0.00	0.00
10,900.00	92.30	178.019	8,703.91	-2,187.00	515.34	2,236.17	0.00	0.00	0.00	0.00
11,000.00	92.30	178.019	8,699.90	-2,286.86	518.79	2,335.60	0.00	0.00	0.00	0.00
11,100.00	92.30	178.019	8,695.88	-2,386.72	522.25	2,435.03	0.00	0.00	0.00	0.00
11,200.00	92.30	178.019	8,691.87	-2,486.58	525.70	2,534.46	0.00	0.00	0.00	0.00
11,300.00	92.30	178.019	8,687.86	-2,586.44	529.15	2,633.89	0.00	0.00	0.00	0.00
11,400.00	92.30	178.019	8,683.84	-2,686.30	532.61	2,733.32	0.00	0.00	0.00	0.00
11,500.00	92.30	178.019	8,679.83	-2,786.16	536.06	2,832.75	0.00	0.00	0.00	0.00
11,600.00	92.30	178.019	8,675.82	-2,886.02	539.51	2,932.18	0.00	0.00	0.00	0.00
11,700.00	92.30	178.019	8,671.80	-2,985.88	542.97	3,031.61	0.00	0.00	0.00	0.00
11,800.00	92.30	178.019	8,667.79	-3,085.74	546.42	3,131.04	0.00	0.00	0.00	0.00
11,900.00	92.30	178.019	8,663.78	-3,185.60	549.88	3,230.46	0.00	0.00	0.00	0.00
12,000.00	92.30	178.019	8,659.76	-3,285.45	553.33	3,329.89	0.00	0.00	0.00	0.00
12,100.00	92.30	178.019	8,655.75	-3,385.31	556.78	3,429.32	0.00	0.00	0.00	0.00
12,200.00	92.30	178.019	8,651.74	-3,485.17	560.24	3,528.75	0.00	0.00	0.00	0.00
12,300.00	92.30	178.019	8,647.72	-3,585.03	563.69	3,628.18	0.00	0.00	0.00	0.00
12,400.00	92.30	178.019	8,643.71	-3,684.89	567.14	3,727.61	0.00	0.00	0.00	0.00
12,500.00	92.30	178.019	8,639.70	-3,784.75	570.60	3,827.04	0.00	0.00	0.00	0.00
12,600.00	92.30	178.019	8,635.69	-3,884.61	574.05	3,926.47	0.00	0.00	0.00	0.00
12,700.00	92.30	178.019	8,631.67	-3,984.47	577.51	4,025.90	0.00	0.00	0.00	0.00
12,800.00	92.30	178.019	8,627.66	-4,084.33	580.96	4,125.32	0.00	0.00	0.00	0.00
12,900.00	92.30	178.019	8,623.65	-4,184.19	584.41	4,224.75	0.00	0.00	0.00	0.00
13,000.00	92.30	178.019	8,619.63	-4,284.05	587.87	4,324.18	0.00	0.00	0.00	0.00
13,100.00	92.30	178.019	8,615.62	-4,383.91	591.32	4,423.61	0.00	0.00	0.00	0.00
13,117.04	92.30	178.019	8,614.94	-4,400.93	591.91	4,440.56	0.00	0.00	0.00	0.00
Bottom Hole Location at 13117.1 MD & 8615.0 TVD - 1-17-3-2WH BHL - 1-17-3-2WH BHL										

Plan Annotations

Measured Depth (ft)	Vertical Depth (ft)	Local Coordinates +N/-S (ft)	Local Coordinates +E/-W (ft)	Comment
8,267.78	8,244.52	145.28	434.21	KOP at 8267.8 MD & 8244.5 TVD
9,083.18	8,765.35	-372.52	452.43	End of Build at 9083.2 MD & 8765.4 TVD
9,142.78	8,765.66	-432.08	454.53	7" Casing Point at 9142.8 MD & 8765.7 TVD
13,117.05	8,614.94	-4,400.93	591.91	Bottom Hole Location at 13117.1 MD & 8615.0 TVD

RECEIVED: November 07, 2012

HALLIBURTON

Plan Report for 1-17-3-2WH - Proposal Plan A Rev 0

Vertical Section Information

Angle Type	Target	Azimuth (°)	Origin Type	Origin +N/_S (ft)	Origin +E/-W (ft)	Start TVD (ft)
Target	1-17-3-2WH BHL	172.340	Slot	0.00	0.00	0.00

Survey tool program

From (ft)	To (ft)	Survey/Plan	Survey Tool
0.00	13,117.05	Proposal Plan A Rev 0	MWD

Casing Details

Measured Depth (ft)	Vertical Depth (ft)	Name	Casing Diameter (")	Hole Diameter (")
9,142.78	8,765.66	7"	7	8-3/4

Formation Details

Measured Depth (ft)	Vertical Depth (ft)	Name	Lithology	Dip (°)	Dip Direction (°)
	8,796.98	Uteland Butte 'C' Top of Porosity (Horizontal Targ		-2.30	180.000
	8,863.98	Wasatch		-2.30	180.000
8,872.51	8,728.98	Uteland Butte		-2.30	180.000
9,208.24	8,785.98	Uteland Butte 'C' (Landing Target)		-2.30	180.000
9,274.36	8,788.98	Intermediate Casing Point		-2.30	180.000

Targets associated with this wellbore

Target Name	TVD (ft)	+N/-S (ft)	+E/-W (ft)	Shape
1-17-3-2WH SL	0.00	0.00	0.00	Point
1-17-3-2WH Section Lines	0.00	0.00	0.00	Polygon
1-17-3-2WH BHL	8,614.98	-4,400.93	591.91	Point
1-17-3-2WH Setback Lines	0.00	0.00	0.00	Polygon
1-17-3-2WH CP	8,769.98	-432.09	454.53	Point

RECEIVED: November 07, 2012

Newfield Exploration Company

HALLIBURTON

Duchesne County, UT

North Reference Sheet for Sec. 17-T3S-R2W - 1-17-3-2WH - Plan A Rev 0

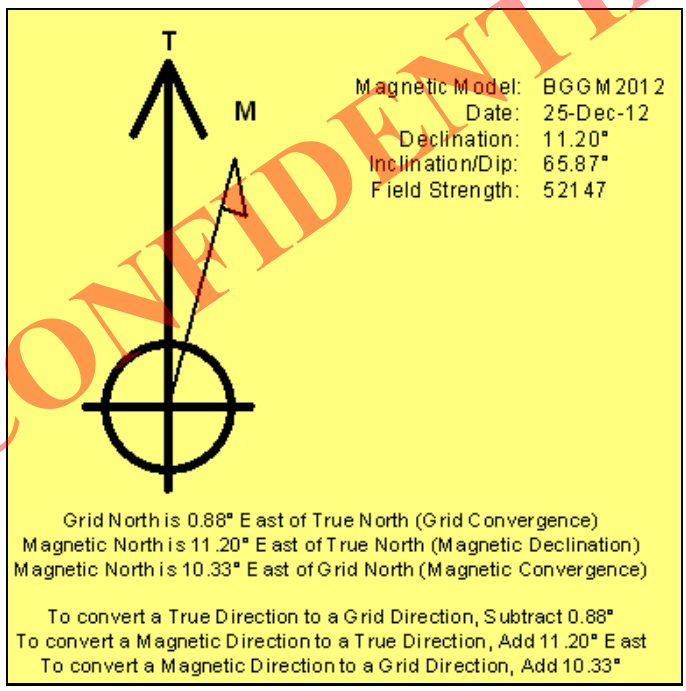
All data is in US Feet unless otherwise stated. Directions and Coordinates are relative to True North Reference.
Vertical Depths are relative to WELL-RKB @ 5231.59ft (Original Well Elev). Northing and Easting are relative to 1-17-3-2WH
Coordinate System is US State Plane 1983, Utah Central Zone using datum North American Datum 1983, ellipsoid GRS 1980

Projection method is Lambert Conformal Conic (2 parallel)
Central Meridian is -111.50°, Longitude Origin:0° 0' 0.000 E°, Latitude Origin:40° 39' 0.000 N°
False Easting: 1,640,416.67ft, False Northing: 6,561,666.67ft, Scale Reduction: 0.99992236

Grid Coordinates of Well: 7,254,915.78 ft N, 2,023,424.40 ft E
Geographical Coordinates of Well: 40° 13' 42.81" N, 110° 07' 41.40" W
Grid Convergence at Surface is: 0.88°

Based upon Minimum Curvature type calculations, at a Measured Depth of 13,117.04ft
the Bottom Hole Displacement is 4,440.56ft in the Direction of 172.34° (True).

Magnetic Convergence at surface is: -10.33° (25 December 2012, , BGGM2012)



RECEIVED: November 07, 2012

AFFIDAVIT OF EASEMENT, RIGHT-OF-WAY AND SURFACE USE AGREEMENT

Peter Burns personally appeared before me, being duly sworn, deposes and with respect to State of Utah R649-3-34.7 says:

1. My name is Peter Burns. I am a Land Associate for Newfield Production Company, whose address is 1001 17th Street, Suite 2000, Denver, CO 80202 ("Newfield").

2. Newfield is the Operator of the proposed Lejeune 1-17-3-2WH well with a surface location to be positioned in the NENE of Section 17, Township 3 South, Range 2 West, Duchesne County, Utah (the "Drillsite Location") and a bottom hole location to be positioned in the SESE of Section 17, Township 3 South, Range 2 West, Duchesne County, Utah. The surface owner of the Drillsite Location is Murray Sheep Ranch, LLC, whose address is P.O. Box 96, Myton, UT 84052 ("Surface Owner").

3. Newfield and the Surface Owner have agreed upon an Easement, Right-of-Way and Surface Use Agreement dated October 3, 2012 covering the Drillsite Location and access to the Drillsite Location.

FURTHER AFFIANT SAYETH NOT.

ACKNOWLEDGEMENT

STATE OF COLORADO §
§
COUNTY OF DENVER §

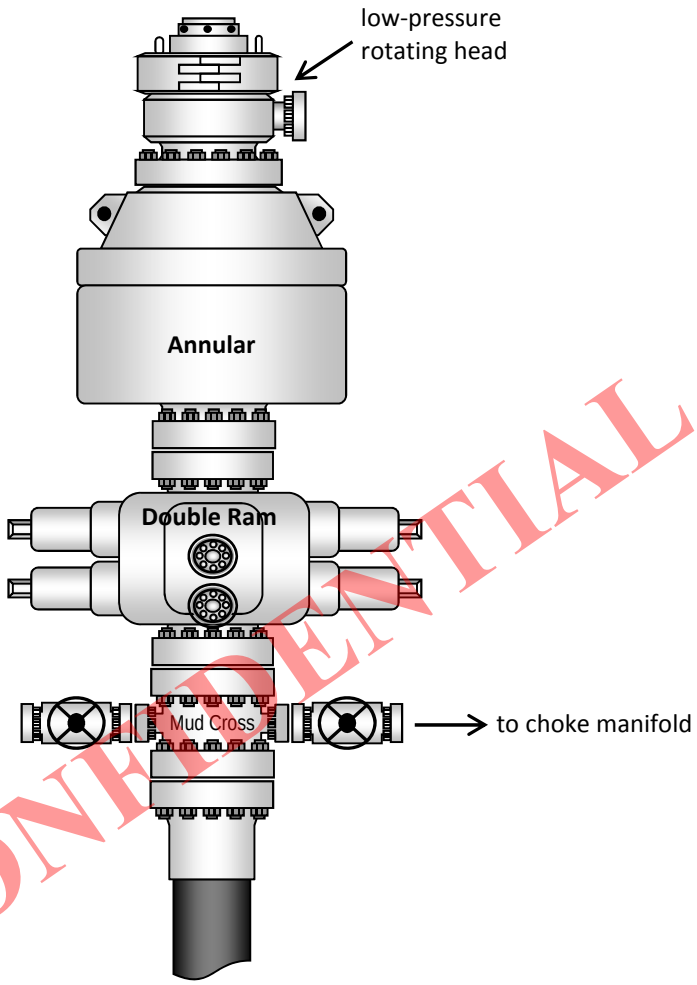
Before me, a Notary Public, in and for the State, on this 4th day of October, 2012, personally appeared Peter Burns, to me known to be the identical person who executed the foregoing instrument, and acknowledged to me that he executed the same as his own free and voluntary act and deed for the uses and purposes therein set forth.

NOTARY PUBLIC

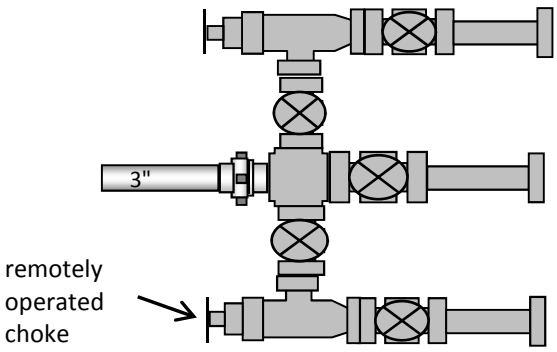
My Commission Expires:

ALAN D. WILD NOTARY PUBLIC STATE OF COLORADO MY COMMISSION EXPIRES 2/17/2015

Typical 5M BOP stack configuration



Typical 5M choke manifold configuration



RECEIVED: November 07, 2012

NEWFIELD
ROCKY MOUNTAINS

November 5, 2012

State of Utah
Division of Oil, Gas & Mining
ATTN: Brad Hill
P O Box 145801
Salt Lake City, UT 84114

RE: **Lejeune 1-17-3-2WH**
Section 17, T3S, R2W
Duchesne County, Utah

Dear Brad,

Newfield Production Company ("Newfield") proposes to drill the Lejeune 1-17-3-2WH from a surface location of 227' FNL & 1,115' FEL of Section 17, T3S, R2W to a bottom hole location of 660' FSL & 660' FEL of Section 17, T3S, R2W. Newfield shall case and cement the Lejeune 1-17-3-2WH wellbore from the surface location to the point where the wellbore reaches the legal setback of 660' FNL of Section 17, T3S, R2W. The cased and cemented portion of the wellbore shall not be perforated nor produced. In the event a future recompletion into the cased and cemented portion of the wellbore is proposed, Newfield shall file the appropriate application with the State. Due to these circumstances, Newfield respectfully requests that DOGM administratively grant an exception location for the Lejeune 1-17-3-2WH.

If you have any questions or require further information, please do not hesitate to contact the undersigned at 303-383-4169 or by email at kharris@newfield.com . Your consideration of this matter is greatly appreciated.

Sincerely,

Kenneth M. Harris
Landman

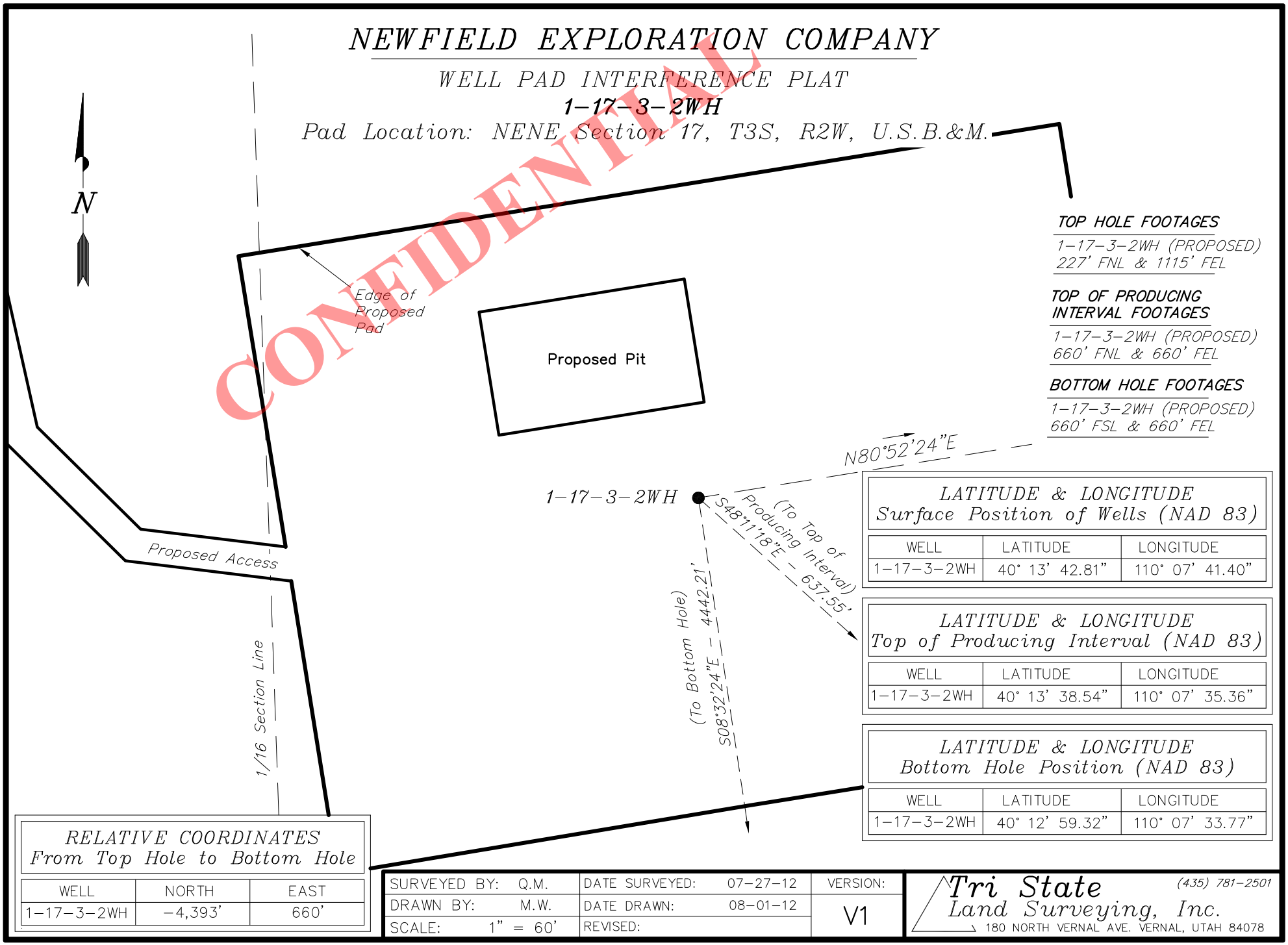
API Well Number: 43013518530000

NEWFIELD EXPLORATION COMPANY

WELL PAD INTERFERENCE PLAT

1-17-3-2WH

Pad Location: NENE Section 17, T3S, R2W, U.S.B.&M.



TOP HOLE FOOTAGES

1-17-3-2WH (PROPOSED)
227' FNL & 1115' FEL

TOP OF PRODUCING INTERVAL FOOTAGES

1-17-3-2WH (PROPOSED)
660' FNL & 660' FEL

BOTTOM HOLE FOOTAGES

1-17-3-2WH (PROPOSED)
660' FSL & 660' FEL

LATITUDE & LONGITUDE
Surface Position of Wells (NAD 83)

WELL	LATITUDE	LONGITUDE
1-17-3-2WH	40° 13' 42.81"	110° 07' 41.40"

LATITUDE & LONGITUDE
Top of Producing Interval (NAD 83)

WELL	LATITUDE	LONGITUDE
1-17-3-2WH	40° 13' 38.54"	110° 07' 35.36"

LATITUDE & LONGITUDE
Bottom Hole Position (NAD 83)

WELL	LATITUDE	LONGITUDE
1-17-3-2WH	40° 12' 59.32"	110° 07' 33.77"

RELATIVE COORDINATES
From Top Hole to Bottom Hole

WELL	NORTH	EAST
1-17-3-2WH	-4,393'	660'

SURVEYED BY: Q.M.	DATE SURVEYED: 07-27-12	VERSION:	Tri State Land Surveying, Inc. (435) 781-2501
DRAWN BY: M.W.	DATE DRAWN: 08-01-12	V1	180 NORTH VERNAL AVE. VERNAL, UTAH 84078
SCALE: 1" = 60'	REVISED:		

RECEIVED: November 07, 2012

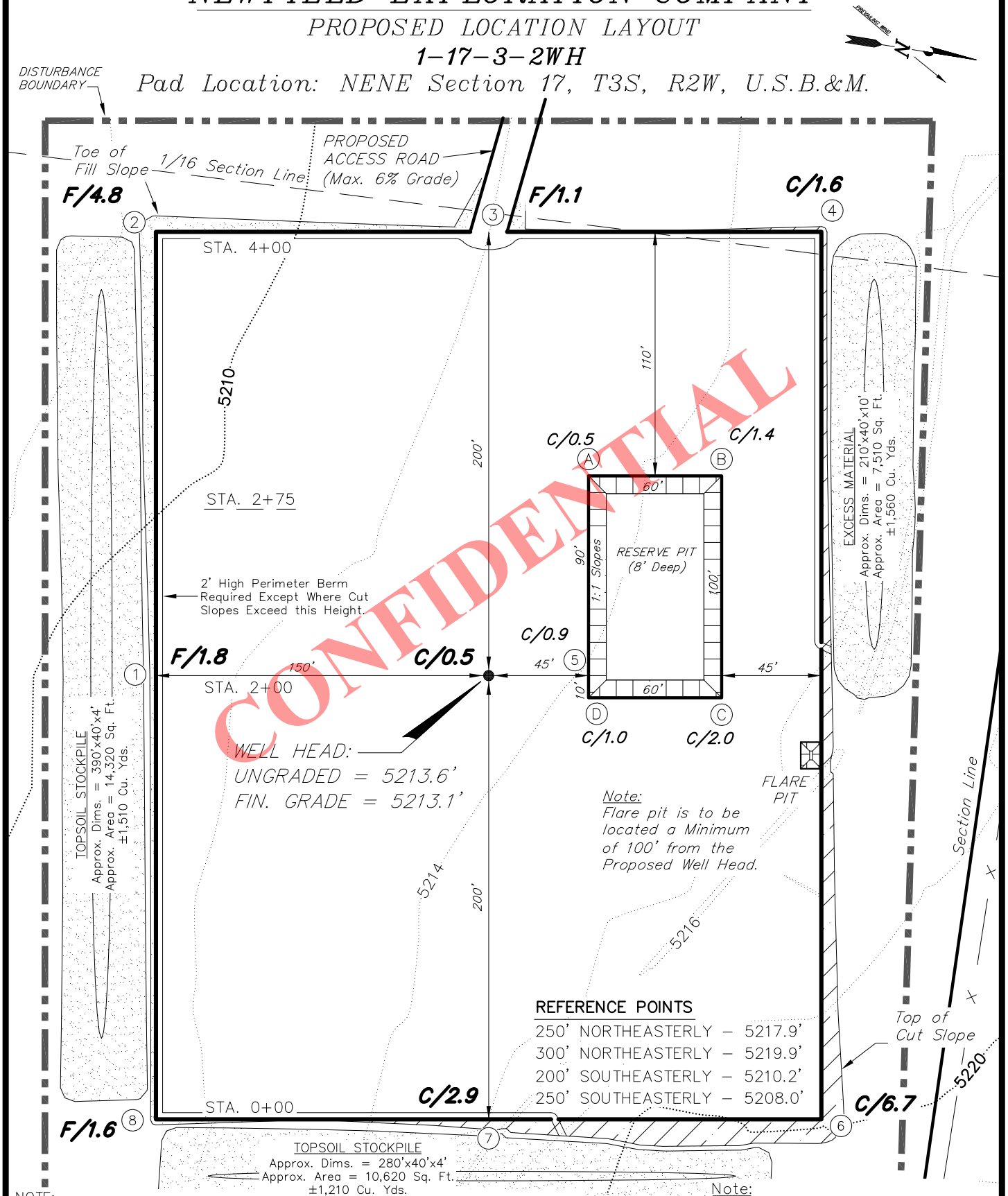
API Well Number: 43013518530000

NEWFIELD EXPLORATION COMPANY

PROPOSED LOCATION LAYOUT

1-17-3-2WH

Pad Location: NENE Section 17, T3S, R2W, U.S.B.&M.



NOTE:
The topsoil & excess material areas are calculated as being mounds containing 4,280 cubic yards of dirt (a 10% fluff factor is included). The mound areas are calculated with push slopes of 1.5:1 & fall slopes of 1.5:1.

Note:
Topsoil to be Stripped From All New Construction Areas and Proposed Stockpile Locations

SURVEYED BY: Q.M.	DATE SURVEYED: 07-27-12	VERSION:	Tri State Land Surveying, Inc. (435) 781-2501
DRAWN BY: M.W.	DATE DRAWN: 08-01-12	V1	180 NORTH VERNAL AVE. VERNAL, UTAH 84078
SCALE: 1" = 60'	REVISED:		

RECEIVED: November 07, 2012

NEWFIELD EXPLORATION COMPANY

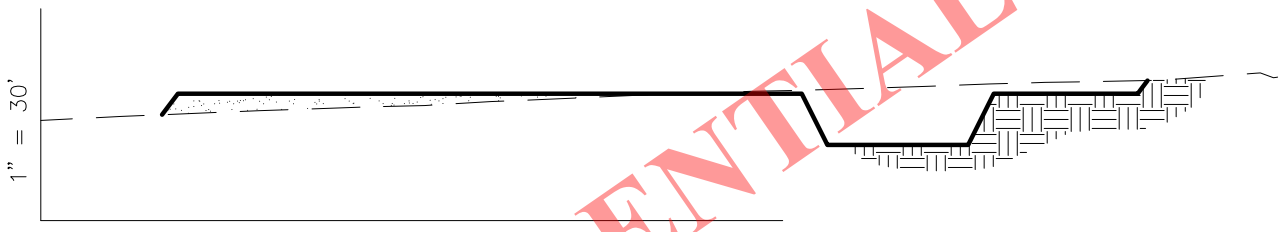
CROSS SECTIONS

1-17-3-2WH

Pad Location: NENE Section 17, T3S, R2W, U.S.B.&M.

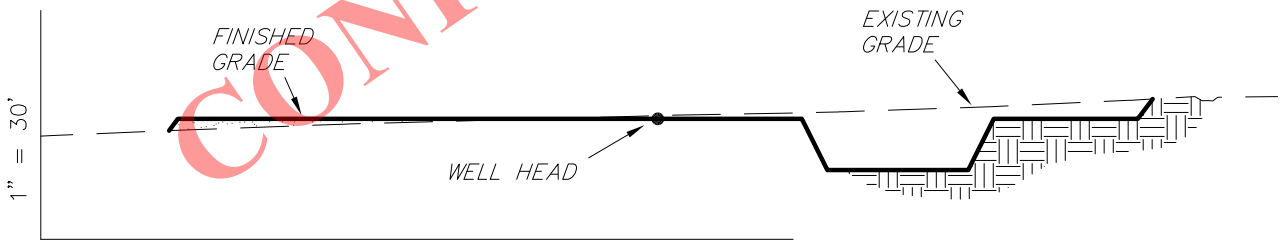
1" = 60'

STA. 4+00



1" = 60'

STA. 2+75



1" = 60'

STA. 2+00

1" = 60'

STA. 0+00

ESTIMATED EARTHWORK QUANTITIES
(No Shrink or swell adjustments have been used)
(Expressed in Cubic Yards)

ITEM	CUT	FILL	6" TOPSOIL	EXCESS
PAD	3,830	3,830	Topsoil is not included in Pad Cut Volume	0
PIT	1,420	0		1,420
TOTALS	5,250	3,830	2,480	1,420

NOTE:
UNLESS OTHERWISE NOTED ALL CUT/FILL SLOPES ARE AT 1.5:1

SURVEYED BY: Q.M.	DATE SURVEYED: 07-27-12	VERSION:	Tri State Land Surveying, Inc. (435) 781-2501
DRAWN BY: M.W.	DATE DRAWN: 08-01-12	V1	180 NORTH VERNAL AVE. VERNAL, UTAH 84078
SCALE: 1" = 60'	REVISED:		

RECEIVED: November 07, 2012

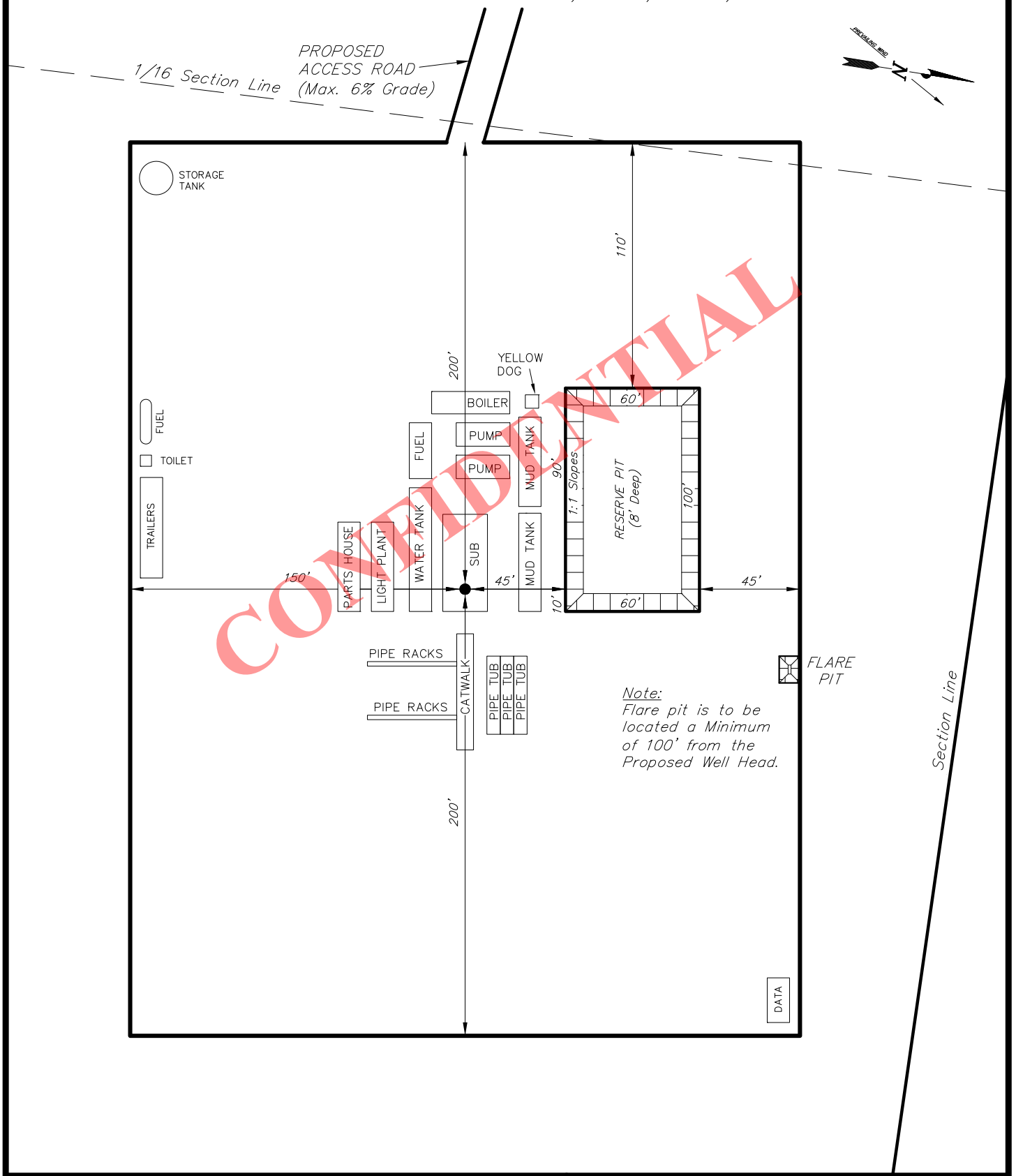
API Well Number: 43013518530000

NEWFIELD EXPLORATION COMPANY

TYPICAL RIG LAYOUT

1-17-3-2WH

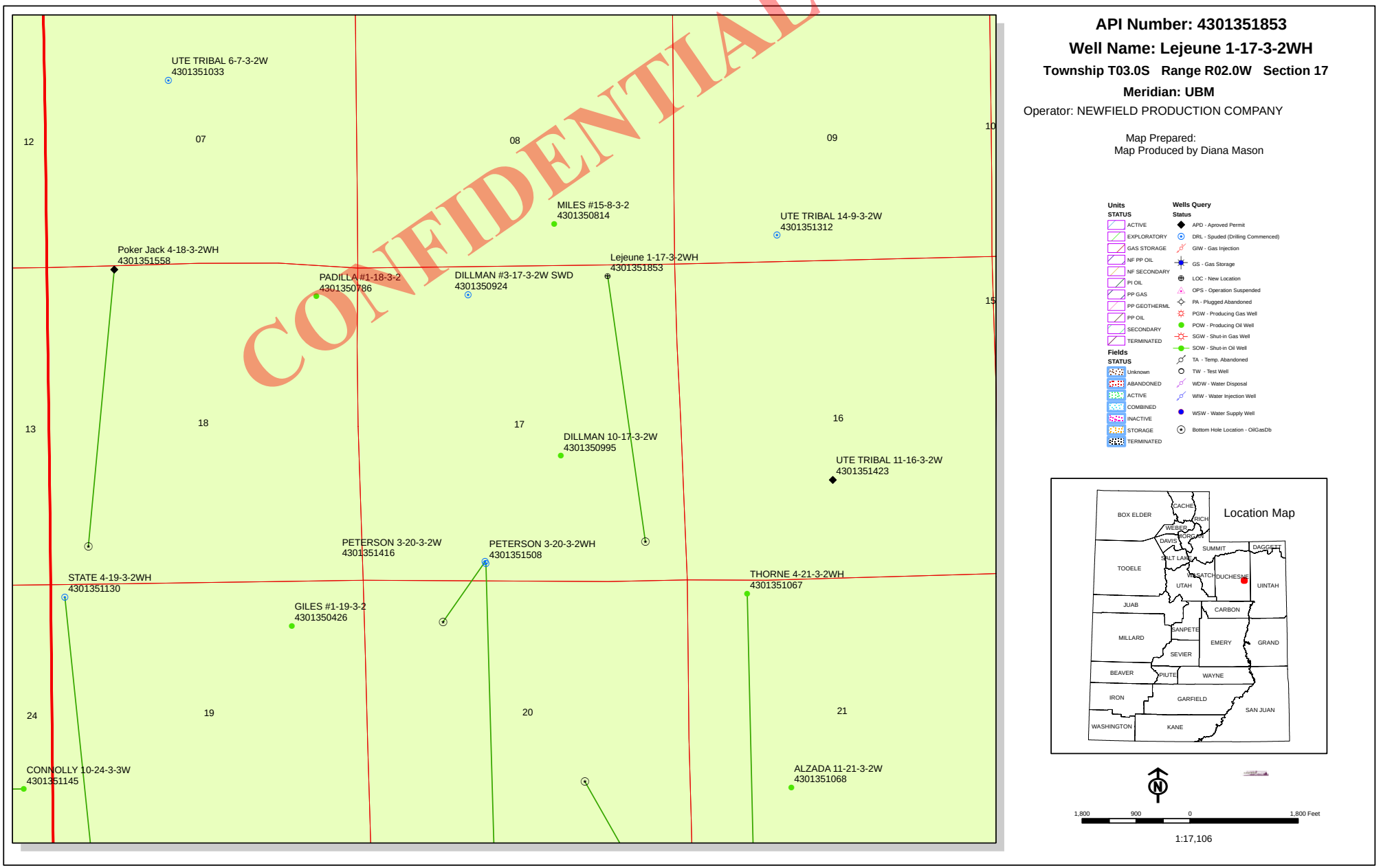
Pad Location: NENE Section 17, T3S, R2W, U.S.B.&M.



SURVEYED BY: Q.M.	DATE SURVEYED: 07-27-12	VERSION:	Tri State Land Surveying, Inc. (435) 781-2501
DRAWN BY: M.W.	DATE DRAWN: 08-01-12	V1	180 NORTH VERNAL AVE. VERNAL, UTAH 84078
SCALE: 1" = 60'	REVISED:		

RECEIVED: November 07, 2012

API Well Number: 43013518530000



API Number: 4301351853

Well Name: Lejeune 1-17-3-2WH

Township T03.0S Range R02.0W Section 17

Meridian: UBM

Operator: NEWFIELD PRODUCTION COMPANY

Map Prepared:
Map Produced by Diana Mason

RECEIVED: November 09, 2012

API Well Number: 43013518530000

BOPE REVIEW NEWFIELD PRODUCTION COMPANY Lejeune 1-17-3-2WH 43013518530000

Well Name	NEWFIELD PRODUCTION COMPANY Lejeune 1-17-3-2WH 43013518			
String	Cond	Surf	I1	Prod
Casing Size(")	14.000	9.625	7.000	4.500
Setting Depth (TVD)	60	2500	8766	8615
Previous Shoe Setting Depth (TVD)	0	60	2500	8766
Max Mud Weight (ppg)	8.3	8.3	11.5	11.5
BOPE Proposed (psi)	0	500	5000	5000
Casing Internal Yield (psi)	1000	3520	9950	12410
Operators Max Anticipated Pressure (psi)	4928			11.0

Calculations	Cond String	14.000	"	
Max BHP (psi)	.052*Setting Depth*MW=	26		
			BOPE Adequate For Drilling And Setting Casing at Depth?	
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	19	NO	
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	13	NO	
			*Can Full Expected Pressure Be Held At Previous Shoe?	
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	13	NO	
Required Casing/BOPE Test Pressure=		60	psi	
*Max Pressure Allowed @ Previous Casing Shoe=		0	psi	*Assumes 1psi/ft frac gradient

Calculations	Surf String	9.625	"	
Max BHP (psi)	.052*Setting Depth*MW=	1079		
			BOPE Adequate For Drilling And Setting Casing at Depth?	
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	779	NO	diverter
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	529	NO	OK
			*Can Full Expected Pressure Be Held At Previous Shoe?	
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	542	NO	OK
Required Casing/BOPE Test Pressure=		2464	psi	
*Max Pressure Allowed @ Previous Casing Shoe=		60	psi	*Assumes 1psi/ft frac gradient

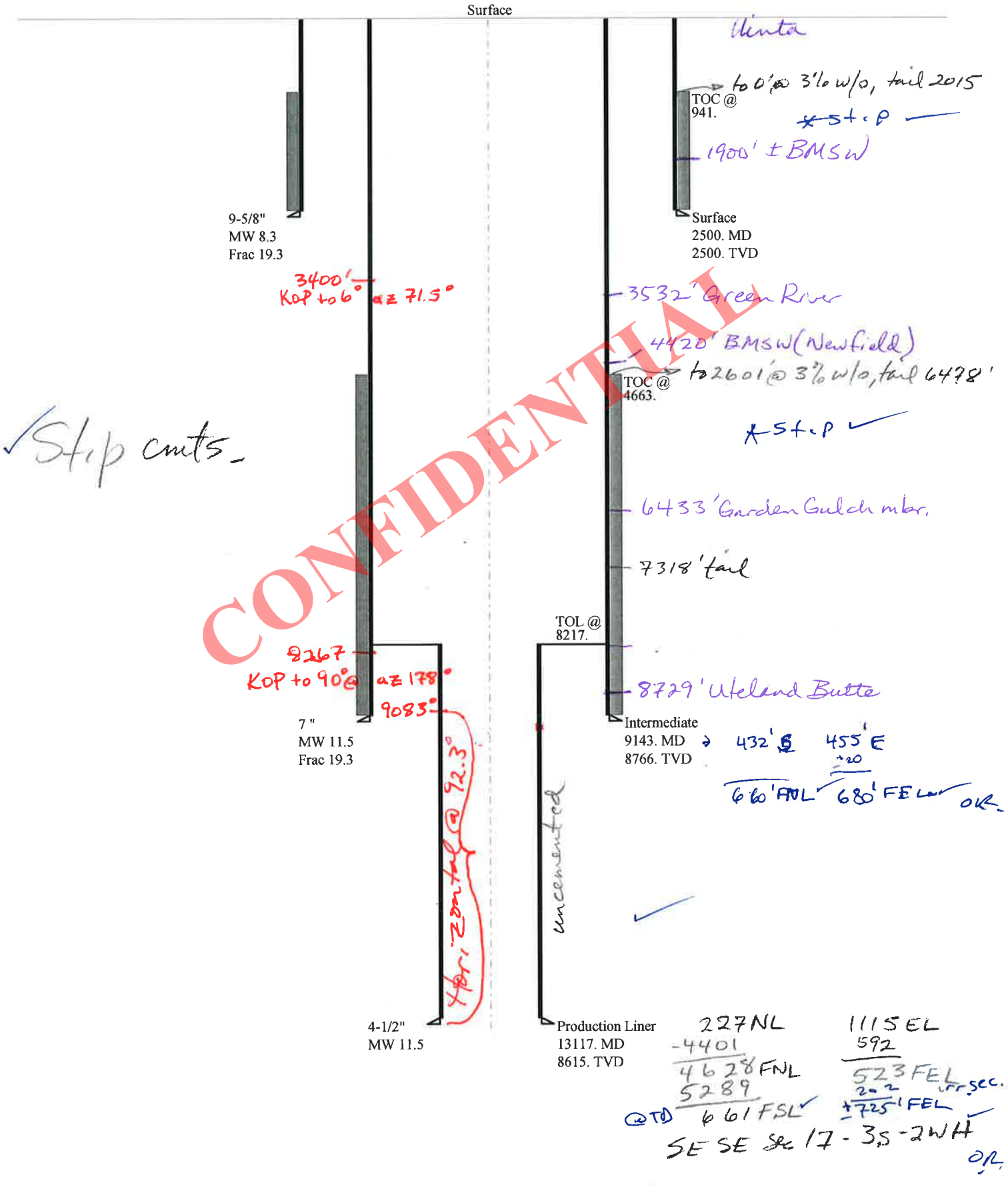
Calculations	I1 String	7.000	"	
Max BHP (psi)	.052*Setting Depth*MW=	5242		
			BOPE Adequate For Drilling And Setting Casing at Depth?	
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	4190	YES	
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	3313	YES	OK
			*Can Full Expected Pressure Be Held At Previous Shoe?	
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	3863	NO	OK
Required Casing/BOPE Test Pressure=		5000	psi	
*Max Pressure Allowed @ Previous Casing Shoe=		2500	psi	*Assumes 1psi/ft frac gradient

Calculations	Prod String	4.500	"	
Max BHP (psi)	.052*Setting Depth*MW=	5152		
			BOPE Adequate For Drilling And Setting Casing at Depth?	
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	4118	YES	
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	3257	YES	OK
			*Can Full Expected Pressure Be Held At Previous Shoe?	
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	5185	YES	
Required Casing/BOPE Test Pressure=		5000	psi	
*Max Pressure Allowed @ Previous Casing Shoe=		8766	psi	*Assumes 1psi/ft frac gradient

RECEIVED: January 08, 2013

43013518530000 Lejeune 1-17-3-2WH

Casing Schematic



Well name:	**43013518530000 Lejeune 1-17-3-2WH**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Surface
Project ID:	43-013-51853
Location:	DUCHESNE COUNTY

Design parameters:

Collapse
Mud weight: 8.330 ppg
Design is based on evacuated pipe.

Burst
Max anticipated surface pressure: 1,950 psi
Internal gradient: 0.220 psi/ft
Calculated BHP 2,500 psi

No backup mud specified.

Minimum design factors:

Collapse:
Design factor 1.125

Burst:
Design factor 1.00

Tension:
8 Round STC: 1.80 (J)
8 Round LTC: 1.70 (J)
Buttress: 1.60 (J)
Premium: 1.50 (J)
Body yield: 1.50 (B)

Tension is based on air weight.
Neutral point: 2,192 ft

Environment:
H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 109 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 100 ft

Cement top: 941 ft

Non-directional string.

Re subsequent strings:
Next setting depth: 8,766 ft
Next mud weight: 11.500 ppg
Next setting BHP: 5,237 psi
Fracture mud wt: 19.250 ppg
Fracture depth: 2,500 ft
Injection pressure: 2,500 psi

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	2500	9.625	36.00	J-55	LT&C	2500	2500	8.796	20443

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	1082	2020	1.867	2500	3520	1.41	90	453	5.03 J

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940
Date: January 8,2013
Salt Lake City, Utah

Remarks:
Collapse is based on a vertical depth of 2500 ft, a mud weight of 8.33 ppg The casing is considered to be evacuated for collapse purposes.
Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Engineering responsibility for use of this design will be that of the purchaser.

Well name:	**43013518530000 Lejeune 1-17-3-2WH**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Intermediate
Project ID:	43-013-51853
Location:	DUCHESNE COUNTY

Design parameters:

Collapse
Mud weight: 11.500 ppg
Design is based on evacuated pipe.

Burst
Max anticipated surface pressure: 3,308 psi
Internal gradient: 0.220 psi/ft
Calculated BHP 5,237 psi

No backup mud specified.

Minimum design factors:

Collapse:
Design factor 1.125

Burst:
Design factor 1.00

Tension:
8 Round STC: 1.80 (J)
8 Round LTC: 1.80 (J)
Buttress: 1.60 (J)
Premium: 1.50 (J)
Body yield: 1.60 (B)

Tension is based on air weight.
Neutral point: 7,267 ft

Environment:
H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 197 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 1,000 ft

Cement top: 4,663 ft

Directional Info - Build & Hold
Kick-off point 3000 ft
Departure at shoe: 627 ft
Maximum dogleg: 11 °/100ft
Inclination at shoe: 89.7 °

Re subsequent strings:
Next setting depth: 8,615 ft
Next mud weight: 11.500 ppg
Next setting BHP: 5,147 psi
Fracture mud wt: 19.250 ppg
Fracture depth: 8,766 ft
Injection pressure: 8,766 psi

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	9143	7	26.00	P-110	Buttress	8766	9143	6.151	101679

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	5237	6230	1.190	5237	9950	1.90	227.9	830.4	3.64 B

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940
Date: January 8,2013
Salt Lake City, Utah

Remarks:
Collapse is based on a vertical depth of 8766 ft, a mud weight of 11.5 ppg The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.
Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

Well name:	**43013518530000 Lejeune 1-17-3-2WH**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Production Liner
Project ID:	43-013-51853
Location:	DUCHESNE COUNTY

Design parameters:

Collapse
Mud weight: 11.500 ppg
Design is based on evacuated pipe.

Burst
Max anticipated surface pressure: 3,251 psi
Internal gradient: 0.220 psi/ft
Calculated BHP 5,147 psi

No backup mud specified.

Minimum design factors:

Collapse:
Design factor 1.125

Burst:
Design factor 1.00

Tension:
8 Round STC: 1.80 (J)
8 Round LTC: 1.80 (J)
Buttress: 1.60 (J)
Premium: 1.50 (J)
Body yield: 1.60 (B)

Tension is based on air weight.
Neutral point: 8,584 ft

Environment:
H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 195 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 1,000 ft

Liner top: 8,217 ft
Directional Info - Build & Hold
Kick-off point 3000 ft
Departure at shoe: 4440 ft
Maximum dogleg: 11 °/100ft
Inclination at shoe: 92.3 °

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	4917	4.5	13.50	P-110	Buttress	8615	13117	3.795	29499

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	5147	10680	2.075	5180	12410	2.40	5.9	421.9	71.32 B

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940
Date: January 8,2013
Salt Lake City, Utah

Remarks:
For this liner string, the top is rounded to the nearest 100 ft.Collapse is based on a vertical depth of 8615 ft, a mud weight of 11.5 ppg The Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.
Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

ON-SITE PREDRILL EVALUATION
Utah Division of Oil, Gas and Mining

Operator NEWFIELD PRODUCTION COMPANY
Well Name Lejeune 1-17-3-2WH
API Number 43013518530000 **APD No** 7104 **Field/Unit** WILDCAT
Location: 1/4,1/4 NENE **Sec** 17 **Tw** 3.0S **Rng** 2.0W 227 FNL 1115 FEL
GPS Coord (UTM) 574169 4453491 **Surface Owner** Murray Sheep Ranch, LLC

Participants

T. Eaton, F. Bird, Z. Mc Intyre, J. Henderson– Newfield; S. Wysong, -BLM; D. Petty, Paul Hawks ,- Tristate; Todd Sherman, Randy Freston - Outlaw Engineering

Regional/Local Setting & Topography

The proposed action is in the Arcadia area in Duchesne County in a river floodplain below the North Myton bench. The location is bordered on 2 sides by theDry gulch Canal system. The city of Myton can be found approximately 4 miles South East. The area is characterized by clayey sandy soils with slopes of < 2% and a high water table surrounded by terracing and benches, both North and South, of several different elevations capped by sandstone cliffs over highly erodible soils consistent with river floodplain profiles. The occasional Butte can also be found. The immediate area is cris-crossed with numerous canals and associated laterals from the Lake Fork and Duchesne Rivers and Lake Boreham. The area has long been used for farming and ranching operations and has recently seen increasing development for petroleum extraction. The New Hope, South Lateral and Dry Gulch canals, Western slopes of the Flattop Butte can all be found in a one mile radius.

Surface Use Plan

Current Surface Use
Grazing

New Road Miles	Well Pad	Src Const Material	Surface Formation
0.13	**Width** 300 **Length** 400	Offsite	UNTA

Ancillary Facilities N

Well pad will need pit run and Aggregate base course imported. Verified by Forrest Bird and was assured this was planned

Waste Management Plan Adequate? Y

Environmental Parameters

Affected Floodplains and/or Wetlands N

Flora / Fauna

High desert shrubland ecosystem adjacent. Expected vegetation consists of black sagebrush, shadscale, Atriplex spp., mustard spp, rabbit brush, horsebrush, broom snakeweed, Opuntia spp and spring annuals. This location is Fallow cultivated grazing
Dominant vegetation;
Willow and weed though mostly barren, describe the proposed site.
Wildlife;
Disturbed soils onsite do not support habitat for wildlife.

RECEIVED: January 09, 2013

Adjacent habitat contains forbs that may be suitable browse for deer, antelope, prairie dogs or rabbits, though none were observed.

Soil Type and Characteristics

previously cultivated silty sands that gently slopes north. Though surrounded by buttes

Erosion Issues Y

Soils are highly erodible and present a threat under heavy precipitation events

Sedimentation Issues Y

Soils are highly erodible and present a threat under heavy precipitation events

Site Stability Issues Y

Drainage Diverson Required? N

Berm Required? Y

Erosion Sedimentation Control Required? N

Paleo Survey Run? N **Paleo Potental Observed?** N **Cultural Survey Run?** N **Cultural Resources?** N

Reserve Pit

Site-Specific Factors		Site Ranking	
Distance to Groundwater (feet)	100 to 200	5	
Distance to Surface Water (feet)	300 to 1000	2	
Dist. Nearest Municipal Well (ft)	>5280	0	
Distance to Other Wells (feet)	>1320	0	
Native Soil Type	Mod permeability	10	
Fluid Type	Fresh Water	5	
Drill Cuttings	Normal Rock	0	
Annual Precipitation (inches)		0	
Affected Populations			
Presence Nearby Utility Conduits	Not Present	0	
	Final Score	22	1 Sensitivity Level

Characteristics / Requirements

A 60’ x 100' x 8' deep reserve pit is planned in an area of cut on the northwest side of the location. A pit liner is required. Newfield commonly uses a 30 mil liner with a felt underliner. Pit should be fenced to prevent entry by deer, other wildlife and domestic animals. Pit to be closed within one year after drilling activities are complete.

Closed Loop Mud Required? N **Liner Required?** Y **Liner Thickness** 16 **Pit Underlayment Required?** Y

Other Observations / Comments

Chris Jensen 11/28/2012

RECEIVED: January 09, 2013

Evaluator **Date / Time**

RECEIVED: January 09, 2013

Application for Permit to Drill
Statement of Basis
Utah Division of Oil, Gas and Mining

APD No	API WellNo	Status	Well Type	Surf Owner	CBM
7104	43013518530000	LOCKED	OW	P	No
Operator	NEWFIELD PRODUCTION COMPANY		**Surface Owner-APD**	Murray Sheep Ranch, LLC	
Well Name	Lejeune 1-17-3-2WH		**Unit**		
Field	WILDCAT		**Type of Work**	DRILL	
Location	NENE 17 3S 2W U 227 FNL 1115 FEL GPS Coord (UTM) 574168E 4453504N				

Geologic Statement of Basis

Newfield proposes to set 60' of conductor and 2,500' of surface casing at this location. The base of the moderately saline water at this location is estimated to be at a depth o 1,900'. A search of Division of Water Rights records shows 10 water wells within a 10,000 foot radius of the center of Section 17. All wells are located over a mile from the proposed location. All wells are privately owned. Depth is listed as ranging from 65 to 150 feet. Average depth is less than 100 feet. Water use is listed as irrigation, stock watering, and domestic use. The surface formation at this site is the Uinta Formation. The Uinta Formation is made up of interbedded shales and sandstones. The sandstones are mostly lenticular and discontinuous and should not be a significant source of useable ground water. The proposed surface casing should adequately protect useable ground water in this area.

Brad Hill — **APD Evaluator**

12/27/2012 — **Date / Time**

Surface Statement of Basis

Location is proposed in a good location although outside the spacing window typical for a horizontal well. Access road enters the pad from the West. The landowner and its representative was not in attendance for the pre-site inspection.
The soil type and topography at present do combine to pose a significant threat to erosion or sediment/ pollution transport in these regional climate conditions.
Construction standards of the Operator appear to be adequate for the proposed purpose as submitted. Operator gave verbal notice of intention to import materials for stability.
I recognize no special flora or animal species or cultural resources on site that the proposed action may harm. A riparian area can be found adjacent the site to the East. The location was previously surveyed for cultural and paleontological resources as the operator saw fit. I have advised an ESA consultation to be initiated to insure no disturbance to TES species that may have not been seen during onsite visit.
The location should be bermed to prevent spills from leaving the confines of the pad.
Fencing around the reserve pit will be necessary once the well is drilled to prevent wildlife and livestock from entering. A synthetic liner of 30 mils (minimum) should be utilized in the reserve pit.

Chris Jensen — **Onsite Evaluator**

11/28/2012 — **Date / Time**

Conditions of Approval / Application for Permit to Drill

RECEIVED: January 09, 2013

Category	Condition
Pits	A synthetic liner with a minimum thickness of 16 mils with a felt subliner shall be properly installed and maintained in the reserve pit.
Surface	The well site shall be bermed to prevent fluids from leaving the pad.
Surface	The reserve pit shall be fenced upon completion of drilling operations.

RECEIVED: January 09, 2013

API Well Number: 43013518530000

WORKSHEET
APPLICATION FOR PERMIT TO DRILL

APD RECEIVED: 11/7/2012 **API NO. ASSIGNED:** 43013518530000

WELL NAME: Lejeune 1-17-3-2WH

OPERATOR: NEWFIELD PRODUCTION COMPANY (N2695) **PHONE NUMBER:** 435 719-2018

CONTACT: Don Hamilton

PROPOSED LOCATION: NENE 17 030S 020W **Permit Tech Review:** ☑

SURFACE: 0227 FNL 1115 FEL **Engineering Review:** ☑

BOTTOM: 0660 FSL 0660 FEL **Geology Review:** ☑

COUNTY: DUCHESNE

LATITUDE: 40.22868 **LONGITUDE:** -110.12821

UTM SURF EASTINGS: 574168.00 **NORTHINGS:** 4453504.00

FIELD NAME: WILDCAT

LEASE TYPE: 4 - Fee

LEASE NUMBER: Patented **PROPOSED PRODUCING FORMATION(S):** GREEN RIVER

SURFACE OWNER: 4 - Fee **COALBED METHANE:** NO

RECEIVED AND/OR REVIEWED:

- ☑ **PLAT**
- ☑ **Bond:** STATE/FEE - B001834
- ☐ **Potash**
- ☐ **Oil Shale 190-5**
- ☐ **Oil Shale 190-3**
- ☐ **Oil Shale 190-13**
- ☑ **Water Permit:** 437478
- ☐ **RDCC Review:**
- ☑ **Fee Surface Agreement**
- ☐ **Intent to Commingle**

Commingling Approved

LOCATION AND SITING:

- ☐ **R649-2-3.**

Unit:

- ☐ **R649-3-2. General**
- ☑ **R649-3-3. Exception**
- ☑ **Drilling Unit**

Board Cause No: Cause 139-90

Effective Date: 5/9/2012

Siting: 4 Prod LGRRV-WSTC Wells

- ☐ **R649-3-11. Directional Drill**

Comments: Presite Completed

Stipulations:

1 - Exception Location - bhill
5 - Statement of Basis - bhill
12 - Cement Volume (3) - hmacdonald
25 - Surface Casing - hmacdonald
27 - Other - bhill

RECEIVED: January 09, 2013

GARY R. HERBERT
Governor
GREGORY S. BELL
Lieutenant Governor

State of Utah
DEPARTMENT OF NATURAL RESOURCES
MICHAEL R. STYLER
Executive Director
Division of Oil, Gas and Mining
JOHN R. BAZA
Division Director

Permit To Drill

****

Well Name: Lejeune 1-17-3-2WH
API Well Number: 43013518530000
Lease Number: Patented
Surface Owner: FEE (PRIVATE)
Approval Date: 1/9/2013

Issued to:
NEWFIELD PRODUCTION COMPANY , Rt 3 Box 3630 , Myton, UT 84052

Authority:
Pursuant to Utah Code Ann. 40-6-1 et seq., and Utah Administrative Code R649-3-1 et seq., the Utah Division of Oil, Gas and Mining issues conditions of approval, and permit to drill the listed well. This permit is issued in accordance with the requirements of Cause 139-90. The expected producing formation or pool is the GREEN RIVER Formation(s), completion into any other zones will require filing a Sundry Notice (Form 9). Completion and commingling of more than one pool will require approval in accordance with R649-3-22.

Duration:
This approval shall expire one year from the above date unless substantial and continuous operation is underway, or a request for extension is made prior to the expiration date

Exception Location:
Appropriate information has been submitted to DOGM and administrative approval of the requested exception location is hereby granted.

General:
Compliance with the requirements of Utah Admin. R. 649-1 et seq., the Oil and Gas Conservation General Rules, and the applicable terms and provisions of the approved Application for permit to drill.

Conditions of Approval:
Compliance with the Conditions of Approval/Application for Permit to Drill outlined in the Statement of Basis (copy attached).

In accordance with Utah Admin. R.649-3-21, the operator shall submit a complete angular deviation and directional survey report to the Division within 30 days following completion of the well.

Cement volume for the 7" intermediate production string shall be determined from actual hole diameter in order to place cement from the pipe setting depth back to 2300' MD as indicated in the submitted drilling plan.

Surface casing shall be cemented to the surface.

Additional Approvals:
The operator is required to obtain approval from the Division of Oil, Gas and mining before performing any of the following actions during the drilling of this well:

- Any changes to the approved drilling plan - contact Dustin Doucet
- Significant plug back of the well - contact Dustin Doucet
- Plug and abandonment of the well - contact Dustin Doucet

Notification Requirements:
The operator is required to notify the Division of Oil, Gas and Mining of the following actions during drilling of this well:

- Within 24 hours following the spudding of the well - contact Carol Daniels
  OR
  submit an electronic sundry notice (pre-registration required) via the Utah Oil & Gas website
  at http://oilgas.ogm.utah.gov
- 24 hours prior to testing blowout prevention equipment - contact Dan Jarvis
- 24 hours prior to cementing or testing casing - contact Dan Jarvis
- Within 24 hours of making any emergency changes to the approved drilling program
  - contact Dustin Doucet
- 24 hours prior to commencing operations to plug and abandon the well - contact Dan Jarvis

Contact Information:
The following are Division of Oil, Gas and Mining contacts and their telephone numbers (please leave a voicemail message if the person is not available to take the call):

- Carol Daniels 801-538-5284 - office
- Dustin Doucet 801-538-5281 - office
  801-733-0983 - after office hours
- Dan Jarvis 801-538-5338 - office
  801-231-8956 - after office hours

Reporting Requirements:
All reports, forms and submittals as required by the Utah Oil and Gas Conservation General Rules will be promptly filed with the Division of Oil, Gas and Mining, including but not limited to:

- Entity Action Form (Form 6) - due within 5 days of spudding the well
- Monthly Status Report (Form 9) - due by 5th day of the following calendar month
- Requests to Change Plans (Form 9) - due prior to implementation
- Written Notice of Emergency Changes (Form 9) - due within 5 days
- Notice of Operations Suspension or Resumption (Form 9) - due prior to implementation
- Report of Water Encountered (Form 7) - due within 30 days after completion
- Well Completion Report (Form 8) - due within 30 days after completion or plugging

Approved By:

Approved By:

For John Rogers
Associate Director, Oil & Gas

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS, AND MINING

FORM 9

5.LEASE DESIGNATION AND SERIAL NUMBER: Patented

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

7.UNIT or CA AGREEMENT NAME:

1. TYPE OF WELL
Oil Well

8. WELL NAME and NUMBER:
Lejeune 1-17-3-2WH

2. NAME OF OPERATOR:
NEWFIELD PRODUCTION COMPANY

9. API NUMBER:
43013518530000

3. ADDRESS OF OPERATOR:
Rt 3 Box 3630 , Myton, UT, 84052

PHONE NUMBER:
435 646-4825 Ext

9. FIELD and POOL or WILDCAT:
WILDCAT

4. LOCATION OF WELL
FOOTAGES AT SURFACE:
0227 FNL 1115 FEL
QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN:
Qtr/Qtr: NENE Section: 17 Township: 03.0S Range: 02.0W Meridian: U

COUNTY:
DUCHESNE

STATE:
UTAH

11.
CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

TYPE OF SUBMISSION	TYPE OF ACTION		
✓ NOTICE OF INTENT Approximate date work will start: 2/12/2013	☐ ACIDIZE	☐ ALTER CASING	☐ CASING REPAIR
	✓ CHANGE TO PREVIOUS PLANS	☐ CHANGE TUBING	☐ CHANGE WELL NAME
	☐ CHANGE WELL STATUS	☐ COMMINGLE PRODUCING FORMATIONS	☐ CONVERT WELL TYPE
☐ SUBSEQUENT REPORT Date of Work Completion:	☐ DEEPEN	☐ FRACTURE TREAT	☐ NEW CONSTRUCTION
	☐ OPERATOR CHANGE	☐ PLUG AND ABANDON	☐ PLUG BACK
	☐ PRODUCTION START OR RESUME	☐ RECLAMATION OF WELL SITE	☐ RECOMPLETE DIFFERENT FORMATION
☐ SPUD REPORT Date of Spud:	☐ REPERFORATE CURRENT FORMATION	☐ SIDETRACK TO REPAIR WELL	☐ TEMPORARY ABANDON
	☐ TUBING REPAIR	☐ VENT OR FLARE	☐ WATER DISPOSAL
☐ DRILLING REPORT Report Date:	☐ WATER SHUTOFF	☐ SI TA STATUS EXTENSION	☐ APD EXTENSION
	☐ WILDCAT WELL DETERMINATION	☐ OTHER	OTHER:

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

Newfield respectfully requests to amend the permit for the Lejeune 1-17-3-2WH. An updated drilling plan and exception to spacing is attached. If granted approval, Newfield would like to update the casing design with 13-3/8" surface casing to 1,000', 9-5/8" Intermediate casing to 6,000', and 5.5" long string from 13,117' MD to surface. Also an oil based mud (OBM) will be used from 6,000' to TD. The location will be modified for a closed loop circulating system with a cuttings pit. OBM cuttings will be reclaimed as per updated drilling plan.

Approved by the Utah Division of Oil, Gas and Mining

Date: February 11, 2013

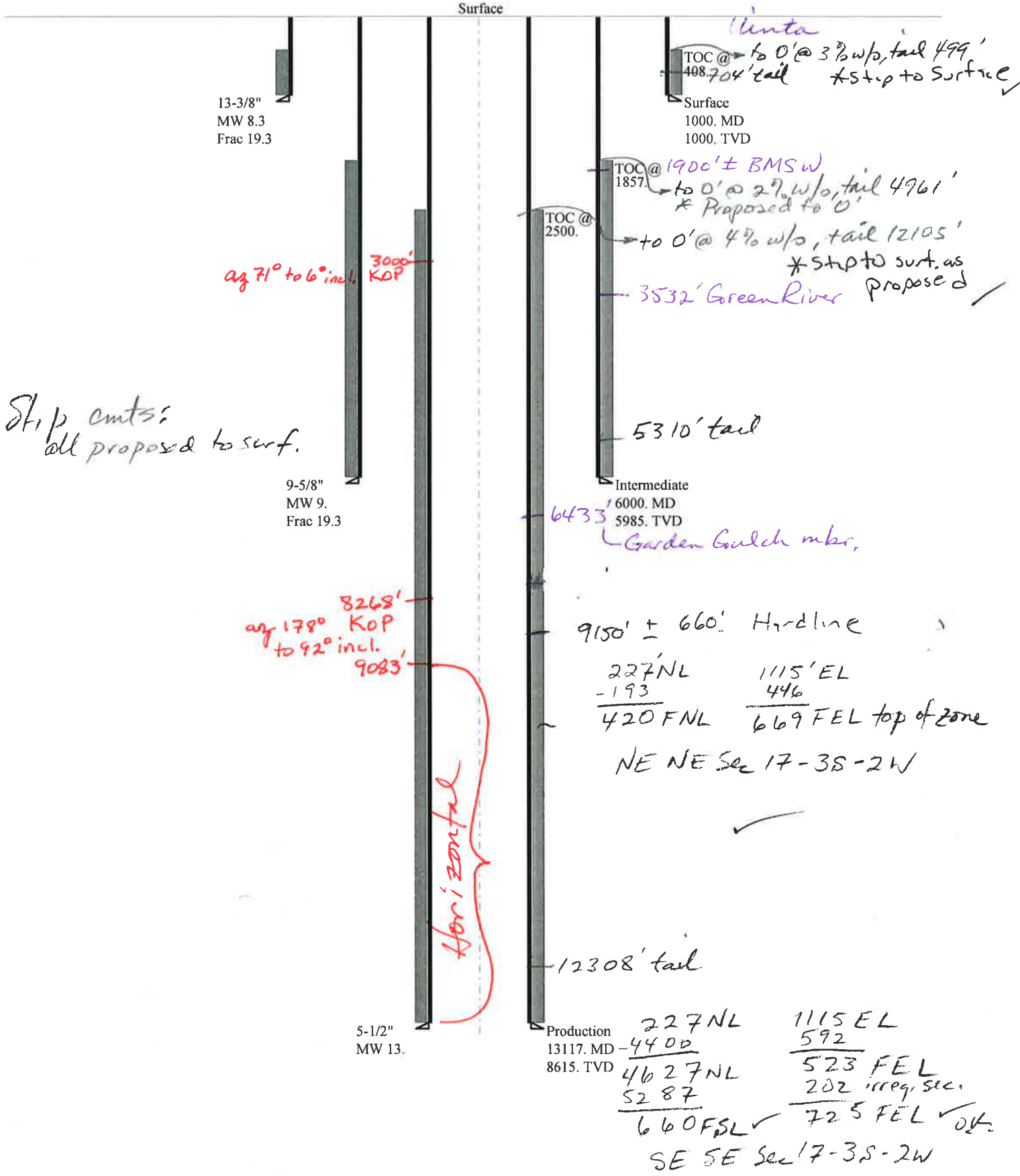
By: Dark K Quist

NAME (PLEASE PRINT)	PHONE NUMBER	TITLE
Don Hamilton	435 719-2018	Permitting Agent
SIGNATURE		**DATE**
N/A		1/11/2013

RECEIVED: Jan. 11, 2013

43013518530000 Lejeune 1-17-3-2WHrev

Casing Schematic



Well name:	**43013518530000 Lejeune 1-17-3-2WHrev**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Surface
Project ID:	43-013-51853
Location:	DUCHESNE COUNTY

Design parameters:

Collapse
Mud weight: 8.330 ppg
Design is based on evacuated pipe.

Burst
Max anticipated surface pressure: 780 psi
Internal gradient: 0.220 psi/ft
Calculated BHP 1,000 psi

No backup mud specified.

Minimum design factors:

Collapse:
Design factor 1.125

Burst:
Design factor 1.00

Tension:
8 Round STC: 1.80 (J)
8 Round LTC: 1.70 (J)
Buttress: 1.60 (J)
Premium: 1.50 (J)
Body yield: 1.50 (B)

Tension is based on air weight.
Neutral point: 876 ft

Environment:
H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 88 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 100 ft

Cement top: 408 ft

Non-directional string.

Re subsequent strings:
Next setting depth: 5,985 ft
Next mud weight: 9.000 ppg
Next setting BHP: 2,798 psi
Fracture mud wt: 19.250 ppg
Fracture depth: 1,000 ft
Injection pressure: 1,000 psi

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	1000	13.375	68.00	J-55	ST&C	1000	1000	12.29	14585

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	433	1950	4.507	1000	3450	3.45	68	675	9.93 J

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940
Date: January 20,2013
Salt Lake City, Utah

Remarks:
Collapse is based on a vertical depth of 1000 ft, a mud weight of 8.33 ppg The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Engineering responsibility for use of this design will be that of the purchaser.

Well name:	**43013518530000 Lejeune 1-17-3-2WHrev**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Intermediate
Project ID:	43-013-51853
Location:	DUCHESNE COUNTY

Design parameters:

Collapse
- Mud weight: 9.000 ppg
- Internal fluid density: 1.000 ppg

Burst
- Max anticipated surface pressure: 3,991 psi
- Internal gradient: 0.220 psi/ft
- Calculated BHP 5,308 psi

No backup mud specified.

Minimum design factors:

Collapse:
- Design factor 1.125

Burst:
- Design factor 1.00

Tension:
- 8 Round STC: 1.80 (J)
- 8 Round LTC: 1.80 (J)
- Buttress: 1.60 (J)
- Premium: 1.50 (J)
- Body yield: 1.60 (B)

Tension is based on air weight.
Neutral point: 5,194 ft

Environment:
- H2S considered? No
- Surface temperature: 74 °F
- Bottom hole temperature: 158 °F
- Temperature gradient: 1.40 °F/100ft
- Minimum section length: 1,000 ft
- Cement top: 1,857 ft

Directional well information:
- Kick-off point 3000 ft
- Departure at shoe: 293 ft
- Maximum dogleg: 1.5 °/100ft
- Inclination at shoe: 6 °

Re subsequent strings:
- Next setting depth: 8,766 ft
- Next mud weight: 13.000 ppg
- Next setting BHP: 5,920 psi
- Fracture mud wt: 19.250 ppg
- Fracture depth: 5,985 ft
- Injection pressure: 5,985 psi

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	6000	9.625	40.00	N-80	Buttress	5985	6000	8.75	81695

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	2487	3090	1.242	5308	5750	1.08	239.4	916.3	3.83 B

Prepared by: Helen Sadik-Macdonald, Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940
Date: January 20,2013
Salt Lake City, Utah

Remarks:
Collapse is based on a vertical depth of 5985 ft, a mud weight of 9 ppg An internal gradient of .052 psi/ft was used for collapse from TD to
Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.
Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

Well name:	**43013518530000 Lejeune 1-17-3-2WHrev**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Production
Project ID:	43-013-51853
Location:	DUCHESNE COUNTY

Design parameters:

Collapse
Mud weight: 13.000 ppg
Design is based on evacuated pipe.

Burst
Max anticipated surface pressure: 3,923 psi
Internal gradient: 0.220 psi/ft
Calculated BHP 5,818 psi

No backup mud specified.

Minimum design factors:

Collapse:
Design factor 1.125

Burst:
Design factor 1.00

Tension:
8 Round STC: 1.80 (J)
8 Round LTC: 1.80 (J)
Buttress: 1.60 (J)
Premium: 1.50 (J)
Body yield: 1.60 (B)

Tension is based on air weight.
Neutral point: 6,940 ft

Environment:
H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 195 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 1,000 ft

Cement top: 2,500 ft

Directional well information:
Kick-off point 3000 ft
Departure at shoe: 4440 ft
Maximum dogleg: 11 °/100ft
Inclination at shoe: 92.3 °

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	13117	5.5	20.00	P-110	LT&C	8615	13117	4.653	101636

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	5818	11100	1.908	5851	12630	2.16	172.3	548	3.18 J

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940
Date: January 20,2013
Salt Lake City, Utah

Remarks:
Collapse is based on a vertical depth of 8615 ft, a mud weight of 13 ppg The casing is considered to be evacuated for collapse purposes.
Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.
Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

Newfield Production Company
1-17-3-2WH
Surface Hole Location: 227' FNL, 1115' FEL, Section 17, T3S, R2W
Bottom Hole Location: 660' FSL, 660' FEL, Section 17, T3S, R2W
Duchesne County, UT

Drilling Program

1. Formation Tops

Uinta	Surface
Green River	3,532'
Garden Gulch member	6,433'
Wasatch	8,729'
Lateral TD	8,615' TVD / 13,117' MD

2. Depth to Oil, Gas, Water, or Minerals

Base of moderately saline	4,420'	(water)
Green River	6,433' - 8,729'	(oil)
Wasatch	8,729' - 8,615'	(oil)

3. Pressure Control

Section	BOP Description
Surface	No control
Intermediate	The BOP and related equipment shall meet the minimum requirements of Onshore Oil and Gas Order No. 2 for equipment and testing requirements, procedures, etc for a 2M system.
Prod/Prod Liner	The BOP and related equipment shall meet the minimum requirements of Onshore Oil and Gas Order No. 2 for equipment and testing requirements, procedures, etc for a 5M system. A 5M BOP system will consist of 2 ram preventers (double or two singles) and an annular preventer (see attached diagram). A choke manifold rated to at least 5,000 psi will be used.

4. Casing

Description	Interval		Weight (ppf)	Grade	Coup	Pore Press @ Shoe	MW @ Shoe	Frac Grad @ Shoe	Safety Factors		
	Top	Bottom (TVD/MD)							Burst	Collapse	Tension
Conductor 20	0'	60'	--	--	Weld	--	--	--	--	--	--
									--	--	--
Surface 13 3/8	0'	1,000'	68	J-55	LTC	8.33	8.33	12	3,450	1,950	1,069,000
									6.15	6.13	15.72
Intermediate 9 5/8	0'	6,000'	40	N-80	BTC	9	9.5	15	5,750	3,090	630,000
									2.40	2.09	2.63
Production Casing 5 1/2	0'	8,615' 13,117'	20	P-110	Tenaris Blue	12.5	13	--	12,640	11,080	641,000
									2.74	2.23	2.44

RECEIVED: Jan. 11, 2013

Assumptions:

Surface casing MASP = (frac gradient + 1.0 ppg) - (gas gradient)
Intermediate casing MASP = (frac gradient + 1.0 PPG) - (water gradient)
Production casing MASP = (reservoir pressure) - (gas gradient)
Intermediate collapse calculations assume lost returns and casing half evacuated.
Production collapse calculations assume fully evacuated casing with a gas gradient
All tension calculations assume air weight of casing
Gas gradient = 0.115 psi/ft

All casing shall be new.
All casing strings shall have a minimum of 1 centralizer on each of the bottom 3 joints.

5. Cement

Job	Hole Size	Fill	Slurry Description	ft^3 / sacks	OH excess	Weight (ppg)	Yield (ft^3/sk)
Conductor	24	60'	Class G w/ 2% KCl + 0.25 lbs/sk Cello Flake	66 / 57	15%	15.8	1.17
Surface Lead	17 1/2	500'	Varicem (Type III) + .125 lbs/sk Cello Flakes	399 / 120	15%	11.0	3.33
Surface Tail	17 1/2	500'	Varicem (Type III) + .125 lbs/sk Cello Flakes	399 / 210	15%	13.0	1.9
Intermediate Lead	12 1/4	5,000'	HLC Premium - 35% Poz/65% Glass G + 10% bentonite	1801 / 510	15%	11.0	3.53
Intermediate Tail	12 1/4	1,000'	50/50 Poz/Class G + 1% bentonite	360 / 279	15%	14.0	1.29
Production Lead	8 3/4	12,117'	50/50 Poz/Class G + 1% bentonite (foamed with nitrogen to 12.5 ppg)	3520 / 997	15%	11.0	3.53
Production Tail	8 3/4	1,000'	50/50 Poz/Class G + 1% bentonite	291 / 225	15%	14.0	1.29

The surface casing will be cemented to surface. In the event that cement does not reach surface during the primary cement job, a remedial job will be performed.

Actual cement volumes for the intermediate casing string will be calculated from an open hole caliper log, plus 15% excess.

The cement slurries will be adjusted for hole conditions and blend test results.

6. Type and Characteristics of Proposed Circulating Medium

Interval	Description
Surface - 1,000'	An air and/or fresh water system will be utilized. If an air rig is used, the blooie line discharge may be less than 100' from the wellbore in order to minimize location size. The blooie line is not equipped with an automatic igniter. The air compressor may be located less than 100' from the well bore due to the low possibility of combustion with the air/dust mixture. Water will be on location to be used as kill fluid, if necessary.

RECEIVED: Jan. 11, 2013

1,000'	- 6,000'	A water based mud system will be utilized. Hole stability may be improved with additions of KCl or a similar inhibitive substance. In order to control formation pressure the system will be weighted with additions of bentonite, and if conditions warrant, with barite. Anticipated maximum mud weight is 9.5 ppg.
6,000'	- TD	One of two possible mud systems may be used depending on offset well performance on ongoing wells: A water based mud: Hole stability may be improved with additions of KCl or a similar inhibitive substance. In order to control formation pressure the system will be weighted with additions of bentonite, and if conditions warrant, with barite. -or- A diesel based OBM system: with an oil to water ratio between 70/30 and 80/20. Emulsifiers and wetting agents will be used to maintain adequate mud properties. A water phase salinity will be maintained in the range of 25% using CaCl (Calcium Chloride). Anticipated maximum mud weight is 13.0 ppg.

7. Logging, Coring, and Testing

Logging: A dual induction, gamma ray, and caliper log will be run from KOP to the base of the surface casing. A compensated neutron/formation density log will be run from TD to the top of the Garden Gulch formation. A cement bond log will be run from KOP to the cement top behind the production casing.

Cores: As deemed necessary.

DST: There are no DST's planned for this well.

8. Anticipated Abnormal Pressure or Temperature

Maximum anticipated bottomhole pressure will be approximately equal to total depth (feet) multiplied by a 0.65 psi/ft gradient.

8,615' x 0.65 psi/ft = 5600 psi

No abnormal temperature is expected. No H_2S is expected.

9. Other Aspects

After setting 9-5/8" casing, an 8-3/4" vertical hole will be drilled to a kick off point of 8,267' .
Directional tools will then be used to build to 92.30 degrees inclination.
The lateral will be drilled to the bottomhole location shown on the plat.
A 5.5" Longstring will be run and cemented in place.

Newfield requests the following variances from Onshore Order #2:
- Variance from Onshoer Order #2, III.E.1
  Refer to Newfield Production Company Standard Operating Practices "Ute Tribal

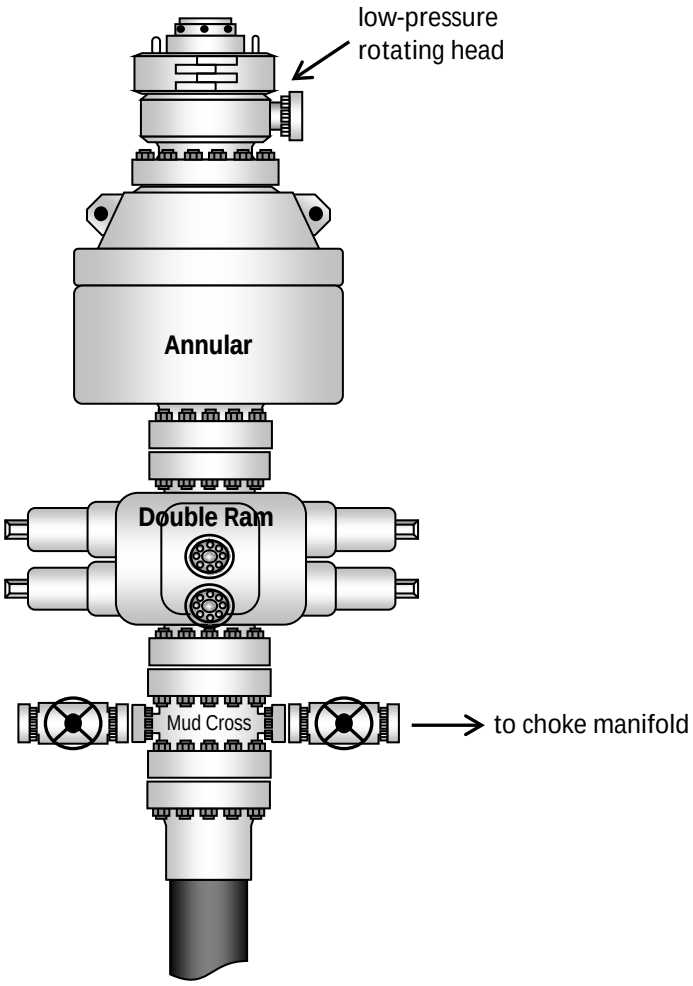
RECEIVED: Jan. 11, 2013

Green River Development Program" paragraph 9.0

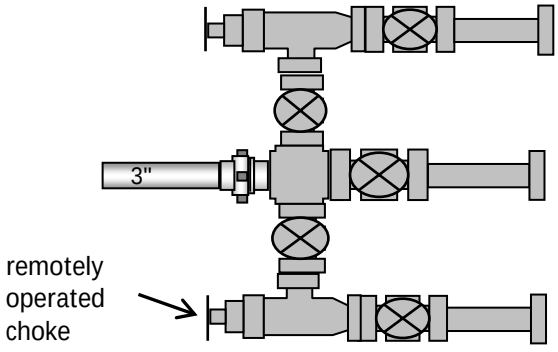
If oil based mud (OBM) is used, all processed OBM drill cuttings would be removed from the well bore using a closed loop system. OBM cuttings would be dried and centrifuged and then temporarily stored within a lined pit that would be constructed inboard of the pad area. The pit would be lined with 16 mil (minimum) thickness polyethylene nylon reinforced liner material. The liner(s) would overlay straw, dirt and/or bentonite if rock is encountered during excavation. The liner would overlap the pit walls and be covered with dirt and/or rocks to hold them in place. No trash, scrap pipe, or other materials that could puncture the liner would be discarded in the pit, and a minimum of two feet of free board would be maintained between the maximum fluid level and the top of the pit at all times. All OBM cuttings will be mechanically dried and centrifuged so that they can be easily transferred to a lined cuttings pit with little to no free fluid on them. Samples of the mechanically dried OBM cuttings will be taken for chemical analysis. The OBM cuttings will then be mixed with a chemical drying agent and the chemically dried OBM cuttings will be placed in a lined cuttings pit on the generating location that is separated from the water based cuttings. The pit will be of sufficient size to contain all cuttings generated in the drilling process. At this point, the chemically dried OBM cuttings are ready for the Firmus® construction process or the OBM cuttings may also be transported to a state approved disposal facility. If an oil based mud is not used, a conventional reserve pit will be utilized. The pit will be reclaimed using UDOGM and BLM approved procedures.

RECEIVED: Jan. 11, 2013

Typical 5M BOP stack configuration



Typical 5M choke manifold configuration



RECEIVED: Jan. 11, 2013

NEWFIELD

February 8, 2013

Newfield Exploration Company
1001 17th Street | Suite 2000
Denver, Colorado 80202
PH 303-893-0102 | FAX 303-893-0103

State of Utah
Division of Oil, Gas & Mining
ATTN: Brad Hill
P O Box 145801
Salt Lake City, UT 84114

RE: **Lejeune 1-17-3-2WH**
Section 17, T3S, R2W
Duchesne County, Utah

Dear Brad,

Newfield Production Company ("Newfield") proposes to directionally drill the Lejeune 1-17-3-2WH from a surface location of 227' FNL & 1,115' FEL of Section 17, T3S, R2W to a bottom hole location of 660' FSL & 660' FEL of Section 17, T3S, R2W. Newfield shall case and cement the Lejeune 1-17-3-2WH 5 ½ production casing from total depth to the surface. The cased and cemented portion of the wellbore shall not be perforated and produced closer than the 660' legal setback of Section 17, T3S, R2W. In the event a future recompletion into the cased and cemented portion of the wellbore is proposed that is closer than the 660' legal setback, Newfield shall file the appropriate application with the State. Due to these circumstances, Newfield respectfully requests that DOGM administratively grant an exception location for the Lejeune 1-17-3-2WH.

If you have any questions or require further information, please do not hesitate to contact the undersigned at 303-383-4169 or by email at kharris@newfield.com . Your consideration of this matter is greatly appreciated.

Sincerely,

Kenneth M. Harris
Landman

CONFIDENTIAL

BLM - Vernal Field Office - Notification Form

Operator Newfield Exploration Rig Name/# Pete Martin 11
Submitted By Branden Arnold Phone Number 435-401-0223
Well Name/Number Lejeune 1-17-3-2WH
Qtr/Qtr NE/NE Section 17 Township 3S Range 2W
Lease Serial Number Patented
API Number 43-013-51853

Spud Notice – Spud is the initial spudding of the well, not drilling out below a casing string.

Date/Time 2/14/13 8:00 AM ☒ PM ☐

Casing – Please report time casing run starts, not cementing times.

- ☐ Surface Casing
- ☐ Intermediate Casing
- ☐ Production Casing
- ☐ Liner
- ☐ Other

Date/Time 2/14/13 1:00 AM ☐ PM ☒

BOPE

- ☐ Initial BOPE test at surface casing point
- ☐ BOPE test at intermediate casing point
- ☐ 30 day BOPE test
- ☐ Other

Date/Time _____ _____ AM ☐ PM ☐

Remarks _____

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS, AND MINING

FORM 9

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

5.LEASE DESIGNATION AND SERIAL NUMBER: Patented

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

7.UNIT or CA AGREEMENT NAME:

1. TYPE OF WELL Oil Well

8. WELL NAME and NUMBER: Lejeune 1-17-3-2WH

2. NAME OF OPERATOR: NEWFIELD PRODUCTION COMPANY

9. API NUMBER: 43013518530000

3. ADDRESS OF OPERATOR: Rt 3 Box 3630 , Myton, UT, 84052

PHONE NUMBER: 435 646-4825 Ext

9. FIELD and POOL or WILDCAT: WILDCAT

4. LOCATION OF WELL
FOOTAGES AT SURFACE: 0227 FNL 1115 FEL
QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: Qtr/Qtr: NENE Section: 17 Township: 03.0S Range: 02.0W Meridian: U

COUNTY: DUCHESNE

STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

TYPE OF SUBMISSION	TYPE OF ACTION		
☐ NOTICE OF INTENT Approximate date work will start:	☐ ACIDIZE	☐ ALTER CASING	☐ CASING REPAIR
☐ SUBSEQUENT REPORT Date of Work Completion:	☐ CHANGE TO PREVIOUS PLANS	☐ CHANGE TUBING	☐ CHANGE WELL NAME
☑ SPUD REPORT Date of Spud: 2/14/2013	☐ CHANGE WELL STATUS	☐ COMMINGLE PRODUCING FORMATIONS	☐ CONVERT WELL TYPE
☐ DRILLING REPORT Report Date:	☐ DEEPEN	☐ FRACTURE TREAT	☐ NEW CONSTRUCTION
	☐ OPERATOR CHANGE	☐ PLUG AND ABANDON	☐ PLUG BACK
	☐ PRODUCTION START OR RESUME	☐ RECLAMATION OF WELL SITE	☐ RECOMPLETE DIFFERENT FORMATION
	☐ REPERFORATE CURRENT FORMATION	☐ SIDETRACK TO REPAIR WELL	☐ TEMPORARY ABANDON
	☐ TUBING REPAIR	☐ VENT OR FLARE	☐ WATER DISPOSAL
	☐ WATER SHUTOFF	☐ SI TA STATUS EXTENSION	☐ APD EXTENSION
	☐ WILDCAT WELL DETERMINATION	☐ OTHER	OTHER:

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

Pete Martin Rig #11 spudded 26" hole on 02/14/2013 and drilled to 60' GL. Set 20", 52.78# (0.250" wall), A52A conductor pipe at 60' GL and cemented to surface with 90 sks of Class G neat cement 15.8# & 1.17 yield.

Accepted by the Utah Division of Oil, Gas and Mining
FOR RECORD ONLY
April 18, 2013

NAME (PLEASE PRINT)	PHONE NUMBER	TITLE
Cherei Neilson	435 646-4883	Drilling Techinacian
SIGNATURE N/A		**DATE** 4/18/2013

RECEIVED: Apr. 18, 2013

Casing / Liner Detail

Well	Lejeune 1-17-3-2WH
Prospect	Central Basin
Foreman	
Run Date:	2/14/2013
String Type	Conductor, 20'', 52.78#, A52A, W (Welded)

- Detail From Top To Bottom -

Depth	*Length*	*JTS*	*Description*	*OD*	*ID*
0.00	60.00	2	20" Conductor Pipe	20.000	19.500

Cement Detail

Cement Company: Other

Slurry	# of Sacks	Weight (ppg)	Yield	Volume (ft^3)	Description - Slurry Class and Additives
Slurry 1					Redi Mix to Surface

Stab-In-Job?	No	Cement To Surface?	Yes
BHT:	0	Est. Top of Cement:	0
Initial Circulation Pressure:		Plugs Bumped?	No
Initial Circulation Rate:		Pressure Plugs Bumped:	
Final Circulation Pressure:		Floats Holding?	No
Final Circulation Rate:		Casing Stuck On / Off Bottom?	No
Displacement Fluid:		Casing Reciprocated?	No
Displacement Rate:		Casing Rotated?	No
Displacement Volume:		CIP:	14:00
Mud Returns:		Casing Wt Prior To Cement:	
Centralizer Type And Placement:		Casing Weight Set On Slips:	

RECEIVED: Apr. 18, 2013

Casing / Liner Detail

Well	Lejeune 1-17-3-2WH
Prospect	Central Basin
Foreman	
Run Date:	2/20/2013
String Type	Surface, 13.375", 68#, J-55, BTC (Generic)

- Detail From Top To Bottom -

Depth	*Length*	*JTS*	*Description*	*OD*	*ID*
0.00	979.18	22	13 3/8" Casing	13.375	12.415
979.18	1.46		Float Collar	13.375	
980.64	45.14	1	Shoe Joint	13.375	12.415
1,025.78	1.01		Guide Shoe		
1,026.79			-		

Cement Detail

Cement Company: Other

Slurry	# of Sacks	Weight (ppg)	Yield	Volume (ft^3)	Description - Slurry Class and Additives
Slurry 1	1280	15.8	1.15	1472	Premium Class G Cement with 1% CaCl2, and 1/4 lb/sk flocele.

Stab-In-Job?	No	Cement To Surface?	Yes
BHT:	0	Est. Top of Cement:	0
Initial Circulation Pressure:	30	Plugs Bumped?	Yes
Initial Circulation Rate:	4	Pressure Plugs Bumped:	700
Final Circulation Pressure:	400	Floats Holding?	Yes
Final Circulation Rate:	4	Casing Stuck On / Off Bottom?	No
Displacement Fluid:	Water	Casing Reciprocated?	No
Displacement Rate:	6	Casing Rotated?	No
Displacement Volume:	147	CIP:	6:57
Mud Returns:	Full	Casing Wt Prior To Cement:	
Centralizer Type And Placement:		Casing Weight Set On Slips:	

9 centralizers spaced 10' from the shoe, on top of joints #2 and #3 then every 3rd collar to surface.

RECEIVED: Apr. 18, 2013

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS, AND MINING

FORM 9

5.LEASE DESIGNATION AND SERIAL NUMBER:
Patented

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

7.UNIT or CA AGREEMENT NAME:

1. TYPE OF WELL
Oil Well

8. WELL NAME and NUMBER:
Lejeune 1-17-3-2WH

2. NAME OF OPERATOR:
NEWFIELD PRODUCTION COMPANY

9. API NUMBER:
43013518530000

3. ADDRESS OF OPERATOR:
Rt 3 Box 3630 , Myton, UT, 84052

PHONE NUMBER:
435 646-4825 Ext

9. FIELD and POOL or WILDCAT:
WILDCAT

4. LOCATION OF WELL
FOOTAGES AT SURFACE:
0227 FNL 1115 FEL
QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN:
Qtr/Qtr: NENE Section: 17 Township: 03.0S Range: 02.0W Meridian: U

COUNTY:
DUCHESNE

STATE:
UTAH

11.
CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

TYPE OF SUBMISSION	TYPE OF ACTION		
✓ NOTICE OF INTENT Approximate date work will start: 6/15/2013	☐ ACIDIZE	☐ ALTER CASING	☐ CASING REPAIR
	✓ CHANGE TO PREVIOUS PLANS	☐ CHANGE TUBING	☐ CHANGE WELL NAME
	☐ CHANGE WELL STATUS	☐ COMMINGLE PRODUCING FORMATIONS	☐ CONVERT WELL TYPE
☐ SUBSEQUENT REPORT Date of Work Completion:	☐ DEEPEN	☐ FRACTURE TREAT	☐ NEW CONSTRUCTION
	☐ OPERATOR CHANGE	☐ PLUG AND ABANDON	☐ PLUG BACK
	☐ PRODUCTION START OR RESUME	☐ RECLAMATION OF WELL SITE	☐ RECOMPLETE DIFFERENT FORMATION
☐ SPUD REPORT Date of Spud:	☐ REPERFORATE CURRENT FORMATION	☐ SIDETRACK TO REPAIR WELL	☐ TEMPORARY ABANDON
	☐ TUBING REPAIR	☐ VENT OR FLARE	☐ WATER DISPOSAL
☐ DRILLING REPORT Report Date:	☐ WATER SHUTOFF	☐ SI TA STATUS EXTENSION	☐ APD EXTENSION
	☐ WILDCAT WELL DETERMINATION	☐ OTHER	OTHER:

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

Newfield Production Company respectfully requests to increase the depth of the 9-5/8" intermediate casing on the subject well from the previously approved depth of 6,000' to 8,382'. This places the 9-5/8" shoe 50' into the Lower Black Shale formation. Offset well data shows the integrity of this shoe provides the best integrity to withstand the expected mud weight of 14 ppg at TD. The target formation remains unchanged. Updated drilling plan and horizontal plan are attached. This well is intended to spud this weekend.

NAME (PLEASE PRINT)	PHONE NUMBER	TITLE
Don Hamilton	435 719-2018	Permitting Agent
SIGNATURE		**DATE**
N/A		6/14/2013

RECEIVED: Jun. 14, 2013

Newfield Production Company
1-17-3-2WH
Surface Hole Location: 227' FNL, 1115' FEL, Section 17, T3S, R2W
Bottom Hole Location: 660' FSL, 660' FEL, Section 17, T3S, R2W
Duchesne County, UT

Drilling Program

1. Formation Tops

Uinta	surface
Green River	3,514'
Garden Gulch member	6,430'
Uteland Butte member	8,711'
Wasatch	8,846'
Lateral TD	8,614' TVD / 13,238' MD

2. Depth to Oil, Gas, Water, or Minerals

Base of moderately saline	866'	(water)
Green River	6,430' - 8,846'	(oil)
Wasatch	8,846' - 8,614'	(oil)

3. Pressure Control

Section	BOP Description
Surface	12-1/4" diverter
Intermediate	The BOP and related equipment shall meet the minimum requirements of Onshore Oil and Gas Order No. 2 for equipment and testing requirements, procedures, etc for a 5M system.
Prod/Prod Liner	The BOP and related equipment shall meet the minimum requirements of Onshore Oil and Gas Order No. 2 for equipment and testing requirements, procedures, etc for a 5M system. A 5M BOP system will consist of 2 ram preventers (double or two singles) and an annular preventer (see attached diagram). A choke manifold rated to at least 5,000 psi will be used.

4. Casing

Description	Interval		Weight (ppf)	Grade	Coup	Pore Press @ Shoe	MW @ Shoe	Frac Grad @ Shoe	Safety Factors		
	Top	Bottom (TVD/MD)							Burst	Collapse	Tension
Conductor	0'	60'	--	--	Weld	--	--	--	--	--	--
20									--	--	--
Surface	0'	1,000'	54.5	J-55	STC	8.33	8.33	12	2,730	1,130	514,000
13 3/8									4.74	3.39	9.43
Intermediate	0'	8,360'	40	N-80	BTC	10	10.5	15	5,750	3,090	916,000
9 5/8		8,382'							1.09	1.35	2.73
Production	0'	8,614'	20	P-110	BTC	14	14.5	16	12,360	11,080	641,000
5 1/2		13,238'							2.28	1.97	2.42

RECEIVED: Jun. 14, 2013

Assumptions:

Surface casing MASP = (frac gradient + 1.0 ppg) - (gas gradient)
Intermediate casing MASP = (reservoir pressure) - (gas gradient)
Production casing MASP = (reservoir pressure) - (gas gradient)
Intermediate collapse calculations assume 50% evacuated
Maximum intermediate csg collapse load assumes loss of mud to a fluid level of 4,191'
Intermediate csg run from surface to 8,382' and will not experience full evacuation
Production csg run from surface to TD will isolate intermediate csg from production loads
Production csg withstands burst and collapse loads for anticipated production conditions
Surface & production collapse calcs assume fully evacuated casing w/ a gas gradient
All tension calculations assume air weight of casing
Gas gradient = 0.1 psi/ft

All casing shall be new.
All casing strings shall have a minimum of 1 centralizer on each of the bottom 3 joints.

5. Cement

Job	Hole Size	Fill	Slurry Description	ft^3 / sacks	OH excess	Weight (ppg)	Yield (ft^3/sk)
Conductor	24	60'	Class G w/ 2% KCl + 0.25 lbs/sk Cello Flake	66 / 57	15%	15.8	1.17
Surface Lead	17 1/2	500'	Varicem (Type III) + .125 lbs/sk Cello Flakes	399 / 120	15%	11.0	3.33
Surface Tail	17 1/2	1,000'	Varicem (Type III) + .125 lbs/sk Cello Flakes	799 / 420	15%	13.0	1.9
Intermediate Lead	12 1/4	6,430'	HLC Premium - 35% Poz/65% Glass G + 10% bentonite	2316 / 656	15%	11.0	3.53
Intermediate Tail	12 1/4	1,952'	50/50 Poz/Class G + 1% bentonite	703 / 545	15%	14.0	1.29
Production Tail	8 3/4	5,856'	50/50 Poz/Class G + 1% bentonite	1701 / 1319	15%	14.0	1.29

The surface casing will be cemented to surface. In the event that cement does not reach surface during the primary cement job, a remedial job will be performed.

Actual cement volumes for the intermediate casing string will be calculated from an open hole caliper log, plus 15% excess.

The cement slurries will be adjusted for hole conditions and blend test results.

6. Type and Characteristics of Proposed Circulating Medium

Interval **Description**

Surface - 1,000'

An air and/or fresh water system will be utilized. If an air rig is used, the blooie line discharge may be less than 100' from the wellbore in order to minimize location size. The blooie line is not equipped with an automatic igniter. The air compressor may be located less than 100' from the well bore due to the low possibility of combustion with the air/dust mixture. Water will be on location to be used as kill fluid, if necessary

to be used as kill fluid, if necessary.

1,000' - 8,382'	A water based mud system will be utilized. Hole stability may be improved with additions of KCl or a similar inhibitive substance. In order to control formation pressure the system will be weighted with additions of bentonite, and if conditions warrant, with barite. Anticipated maximum mud weight is 10.5 ppg.
8,382' - TD	One of two possible mud systems may be used depending on offset well performance on ongoing wells: A water based mud: Hole stability may be improved with additions of KCl or a similar inhibitive substance. In order to control formation pressure the system will be weighted with additions of bentonite, and if conditions warrant, with barite. -or- A diesel based OBM system: with an oil to water ratio between 70/30 and 80/20. Emulsifiers and wetting agents will be used to maintain adequate mud properties. A water phase salinity will be maintained in the range of 25% using CaCl (Calcium Chloride). All cuttings will be dried and centrifuged so that they can be easily transferred to a lined cuttings pit with little to no free fluid on them. The cuttings will be mixed with fly ash prior to transportation to a location on Newfield owned surface. Once on Newfield owned surface, the cuttings will be treated with the previously approved FIRMUS process and used as a construction material on future location and/or roads on Newfield owned surface. The cuttings may also be transported to a state approved disposal facility. Anticipated maximum mud weight is 14.5 ppg.

7. Logging, Coring, and Testing

Logging: A dual induction, gamma ray, and caliper log will be run from KOP to the base of the surface casing. A compensated neutron/formation density log will be run from TD to the top of the Garden Gulch formation. A cement bond log will be run from KOP to the cement top behind the production casing and or intermediate casing.

Cores: As deemed necessary.

DST: There are no DST's planned for this well.

8. Anticipated Abnormal Pressure or Temperature

Maximum anticipated bottomhole pressure will be approximately equal to total depth (feet) multiplied by a 0.73 psi/ft gradient.

8,614' x 0.73 psi/ft = 6271 psi

No abnormal temperature is expected. No H_2S is expected.

RECEIVED: Jun. 14, 2013

9. Other Aspects

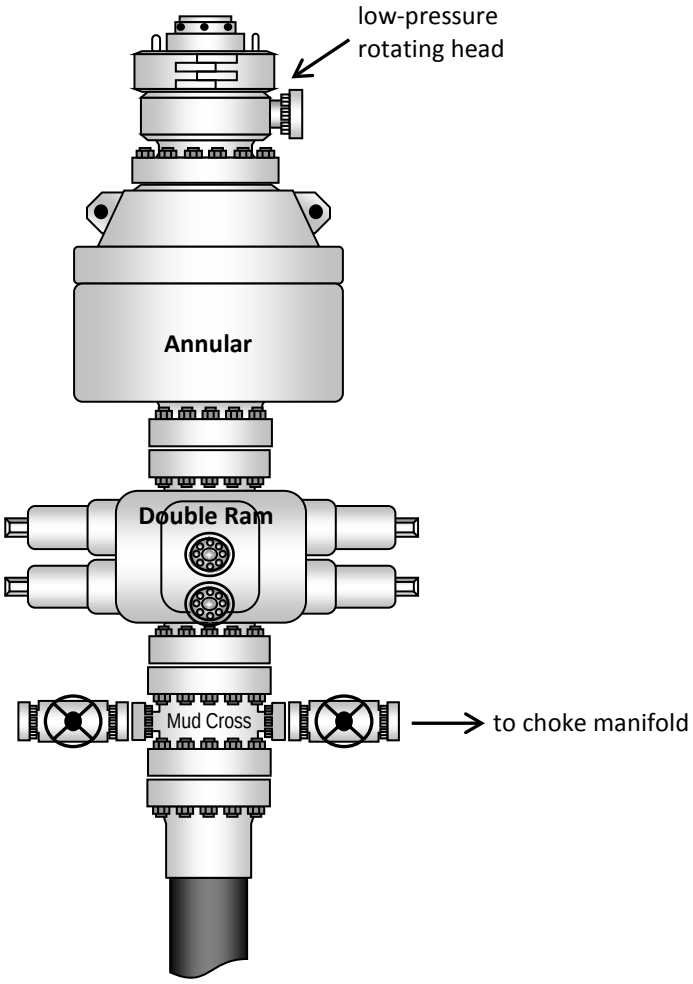
After setting 9-5/8" casing, an 8-3/4" vertical hole will be drilled to a kick off point of 8,411' .
Directional tools will then be used to build to 92.37 degrees inclination.
The lateral will be drilled to the bottomhole location shown on the plat.
A long string will be run and cemented in place.

Newfield requests the following variances from Onshore Order #2:
- Variance from Onshoer Order #2, III.E.1
  Refer to Newfield Production Company Standard Operating Practices "Ute Tribal Green River Development Program" paragraph 9.0

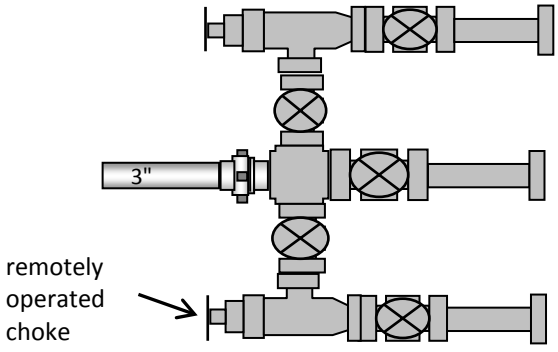
If oil based mud (OBM) is used and If Newfield owns the surface rights on the same drilling site at a location where construction is desired, the cuttings may be used for construction by a Firmus® process at that location. Otherwise, after the cuttings have been made safe for transport as described in paragraph 6, they will be transported to another location on which Newfield owns surface rights and there mixed, as part of a Firmus® process, with at least one additional chemical that will convert them to a temporarily uncured cementitious mixture that will be placed and shaped into a temporary desired final structure that will spontaneously harden within seven days after placement to form the desired structure. Samples of the temporary desired final structure may be taken for testing as described below (after the samples have hardened), or samples of the starting pretreated cuttings and mud will be taken during the construction and later mixed in a laboratory, molded, and cured to simulate the final structure as well as reasonably possible. Either these laboratory-made simulations of the final structure or samples of the temporary mixture itself after hardening, will be mechanically tested directly to determine their unconfined compressive strength and their hydraulic conductivity. Leachates of the mechanically tested structures themselves or of finer particles made by crushing and size-grading of the mechanically tested structures themselves to a specified particle size range will be analyzed, according to specified methods, for their contents of arsenic, barium, cadmium, chromium, lead, mercury, selenium, silver, zinc, benzene, total petroleum hydrocarbons (TPH), and chlorides, and the pH of these leachates will also be measured. The results of all these tests will be reported by Newfield to UDOGM at intervals as requested, along with the latitude and longitude (or other comparable location data) of the site of the useful constructions built.

RECEIVED: Jun. 14, 2013

Typical 5M BOP stack configuration



Typical 5M choke manifold configuration



RECEIVED: Jun. 14, 2013

LEAM Drilling Systems, Inc.
FOR
NEWFIELD EXPLORATION ROCKY MOUNTAINS
WELL: 1-17-3-2WH "LEJEUNE" (Plan: REV02)
SEC. 17, T3S-R2W, DUCHESNE COUNTY, UTAH
DATE: JUNE 11, 2013 -- WELL PLAN PLOT

LEAM Drilling Systems LLC

NEWFIELD ROCKY MOUNTAINS

WELL DETAILS: 1-17-3-2WH
Ground Level: 5214.00

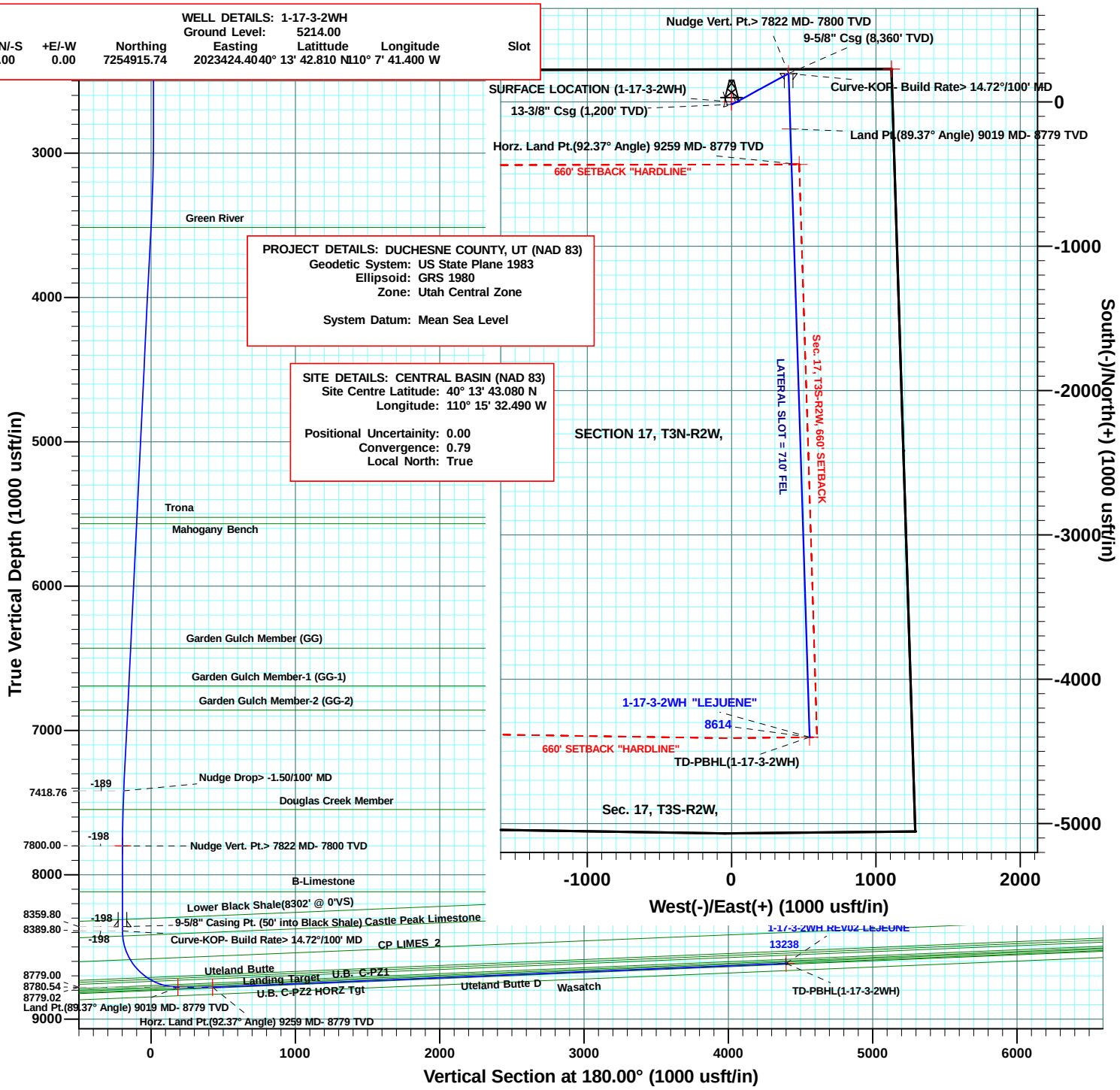
+N/-S	+E/-W	Northing	Easting	Latitude	Longitude	Slot
0.00	0.00	7254915.74	2023424.40	40° 13' 42.810 N	110° 7' 41.400 W	

PROJECT DETAILS: DUCHESNE COUNTY, UT (NAD 83)
Geodetic System: US State Plane 1983
Ellipsoid: GRS 1980
Zone: Utah Central Zone

System Datum: Mean Sea Level

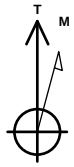
SITE DETAILS: CENTRAL BASIN (NAD 83)
Site Centre Latitude: 40° 13' 43.080 N
Longitude: 110° 15' 32.490 W

Positional Uncertainity: 0.00
Convergence: 0.79
Local North: True



SECTION DETAILS

MD	Inc	Azi	TVD	+N/-S	+E/-W	DLeg	TFace	VSect	Target
968.00	1.54	161.71	967.89	-10.22	-0.34	0.00	0.00	10.22	
1200.00	1.54	161.71	1199.81	-16.15	1.62	0.00	0.00	16.15	
1277.12	0.00	0.00	1276.92	-17.13	1.94	2.00	180.00	17.13	
3000.00	0.00	0.00	2999.80	-17.13	1.94	0.00	0.00	17.13	
3286.41	5.73	61.33	3285.73	-10.27	14.49	2.00	61.33	10.27	
7440.18	5.73	61.33	7418.76	188.60	378.26	0.00	0.00	-188.60	
7822.05	0.00	0.00	7800.00	197.75	395.00	1.50	180.00	-197.75	
8381.85	0.00	0.00	8359.80	197.75	395.00	0.00	0.00	-197.75	
8411.85	0.00	0.00	8389.80	197.75	395.00	0.00	0.00	-197.75	
9018.97	89.37	178.18	8779.00	-187.00	407.23	14.72	178.18	187.00	
9158.97	89.37	178.18	8780.54	-326.92	411.67	0.00	0.00	326.92	
9258.97	92.37	178.18	8779.02	-426.85	414.85	3.00	0.00	426.85	
13238.31	92.37	178.18	8614.47	-4400.79	541.12	0.00	0.00	4400.79	TD-PBHL(1-17-3-2WH)



Azimuths to True North
Magnetic North: 11.11°

Magnetic Field
Strength: 52165.7snT
Dip Angle: 65.88°
Date: 6/14/2013
Model: IGRF2010

Plan: 1-17-3-2WH REV02 LEJEUNE (1-17-3-2WH/1-17-3-2WH "LEJEUNE")
Created By: LYNN HULIN Date: 15:51, June 11 2013

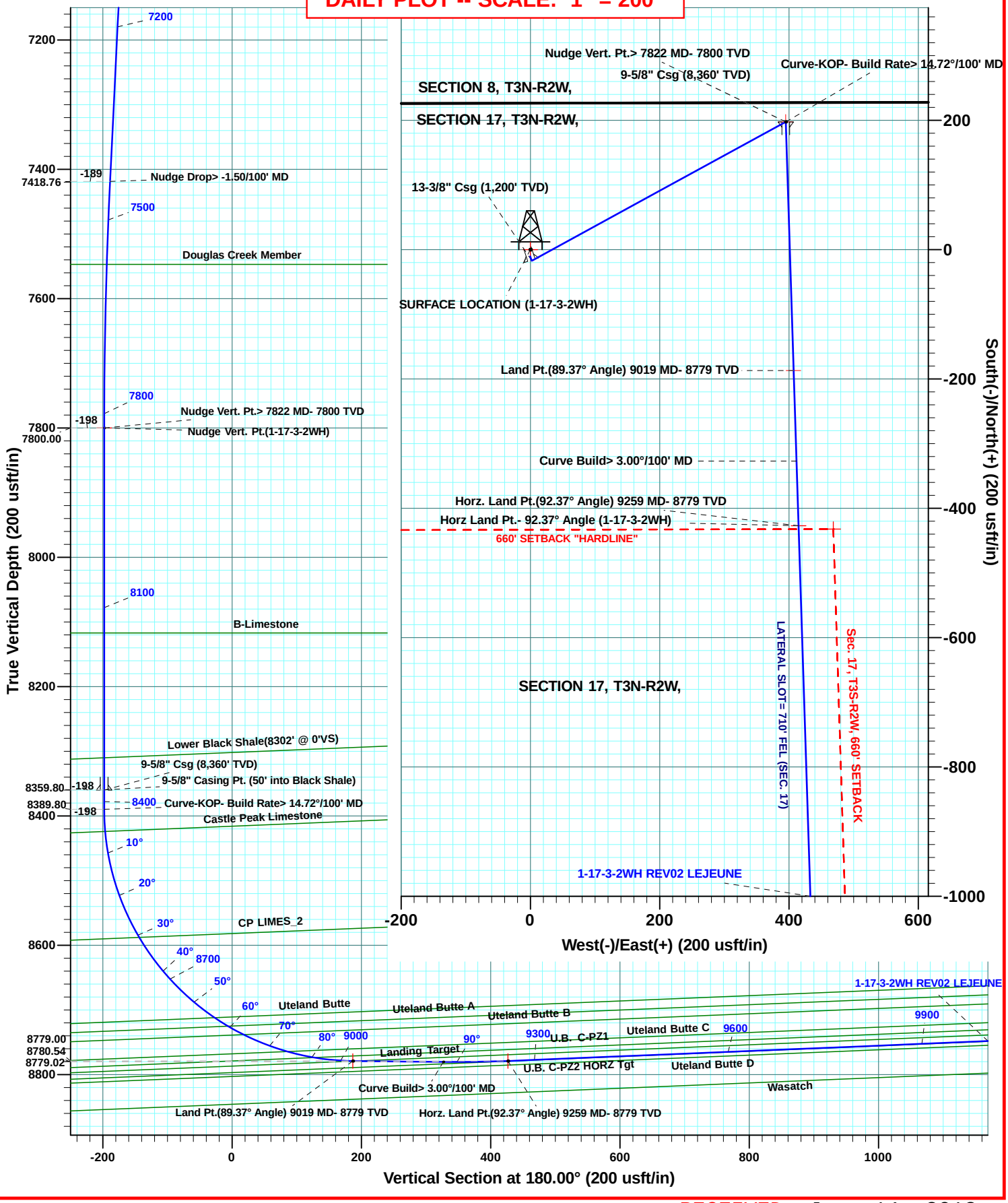
Checked: _____ Date: _____

Reviewed: _____ Date: _____

Approved: _____ Date: _____

LEAM Drilling Systems, Inc.
FOR
NEWFIELD EXPLORATION ROCKY MOUNTAINS
WELL: 1-17-3-2WH "LEJEUNE" (PLAN: REV02)
SEC. 17, T3S-R2W, DUCHESNE COUNTY, UTAH
DATE: JUNE 11, 2013 -- DAILY PLOT - 1"= 200 ft

DAILY PLOT -- SCALE: 1" = 200'



RECEIVED: Jun. 14, 2013

LEAM Drilling Systems LLC

Planning Report

LEAM Drilling Systems LLC

Database:	EDM 5000.1 Lynn Db	**Local Co-ordinate Reference:**	Well 1-17-3-2WH
Company:	NEWFIELD EXPLORATION ROCKY MOUNTAINS	**TVD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Project:	DUCHESNE COUNTY, UT (NAD 83)	**MD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Site:	CENTRAL BASIN (NAD 83)	**North Reference:**	True
Well:	1-17-3-2WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	1-17-3-2WH "LEJUENE"		
Design:	1-17-3-2WH REV02 LEJUENE		

Project DUCHESNE COUNTY, UT (NAD 83),

Map System:	US State Plane 1983	**System Datum:**	Mean Sea Level
Geo Datum:	North American Datum 1983		
Map Zone:	Utah Central Zone		

Site CENTRAL BASIN (NAD 83)

Site Position:		**Northing:**	7,254,409.48 usft	**Latitude:**	40° 13' 43.080 N
From:	Lat/Long	**Easting:**	1,986,891.62 usft	**Longitude:**	110° 15' 32.490 W
Position Uncertainty:	0.00 usft	**Slot Radius:**	13-3/16 "	**Grid Convergence:**	0.79 °

Well 1-17-3-2WH, LEJEUNE PROSPECT

Well Position	**+N/-S**	-0.64 usft	**Northing:**	7,254,915.74 usft	**Latitude:**	40° 13' 42.810 N
	+E/-W	36,536.29 usft	**Easting:**	2,023,424.40 usft	**Longitude:**	110° 7' 41.400 W
Position Uncertainty		0.00 usft	**Wellhead Elevation:**	5,242.00 usft	**Ground Level:**	5,214.00 usft

Wellbore 1-17-3-2WH "LEJUENE"

Magnetics	Model Name	Sample Date	Declination (°)	Dip Angle (°)	Field Strength (nT)
	IGRF2010	6/14/2013	11.11	65.88	52,166

Design 1-17-3-2WH REV02 LEJEUNE

Audit Notes:

Version:	REV02	**Phase:**	PLAN	**Tie On Depth:**	968.00

Vertical Section:	Depth From (TVD) (usft)	+N/-S (usft)	+E/-W (usft)	Direction (°)
	0.00	0.00	0.00	180.00

Plan Sections

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
968.00	1.54	161.71	967.89	-10.22	-0.34	0.00	0.00	0.00	0.00	
1,200.00	1.54	161.71	1,199.81	-16.15	1.62	0.00	0.00	0.00	0.00	
1,277.12	0.00	0.00	1,276.92	-17.13	1.94	2.00	-2.00	0.00	180.00	
3,000.00	0.00	0.00	2,999.80	-17.13	1.94	0.00	0.00	0.00	0.00	
3,286.41	5.73	61.33	3,285.73	-10.27	14.49	2.00	2.00	0.00	61.33	
7,440.18	5.73	61.33	7,418.76	188.60	378.26	0.00	0.00	0.00	0.00	
7,822.05	0.00	0.00	7,800.00	197.75	395.00	1.50	-1.50	0.00	180.00	
8,381.85	0.00	0.00	8,359.80	197.75	395.00	0.00	0.00	0.00	0.00	
8,411.85	0.00	0.00	8,389.80	197.75	395.00	0.00	0.00	0.00	0.00	
9,018.97	89.37	178.18	8,779.00	-187.00	407.23	14.72	14.72	0.00	178.18	
9,158.97	89.37	178.18	8,780.54	-326.92	411.67	0.00	0.00	0.00	0.00	
9,258.97	92.37	178.18	8,779.02	-426.85	414.85	3.00	3.00	0.00	0.00	
13,238.31	92.37	178.18	8,614.47	-4,400.79	541.12	0.00	0.00	0.00	0.00	TD-PBHL(1-17-3-2\

LEAM Drilling Systems LLC

Planning Report

LEAM Drilling Systems LLC

Database:	EDM 5000.1 Lynn Db	**Local Co-ordinate Reference:**	Well 1-17-3-2WH
Company:	NEWFIELD EXPLORATION ROCKY MOUNTAINS	**TVD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Project:	DUCHESNE COUNTY, UT (NAD 83)	**MD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Site:	CENTRAL BASIN (NAD 83)	**North Reference:**	True
Well:	1-17-3-2WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	1-17-3-2WH "LEJUENE"		
Design:	1-17-3-2WH REV02 LEJEUNE		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
28.00	0.00	0.00	28.00	0.00	0.00	0.00	0.00	0.00	0.00
128.00	0.12	227.50	128.00	-0.07	-0.08	0.07	0.12	0.12	0.00
228.00	0.11	195.83	228.00	-0.24	-0.19	0.24	0.07	-0.01	-31.67
328.00	0.15	216.11	328.00	-0.44	-0.29	0.44	0.06	0.04	20.28
428.00	0.46	235.40	428.00	-0.77	-0.70	0.77	0.32	0.31	19.29
528.00	0.40	212.20	528.00	-1.30	-1.21	1.30	0.18	-0.06	-23.21
628.00	0.97	188.07	627.99	-2.43	-1.52	2.43	0.63	0.57	-24.13
728.00	1.23	177.47	727.97	-4.34	-1.59	4.34	0.33	0.26	-10.60
828.00	1.47	169.65	827.94	-6.67	-1.31	6.67	0.30	0.24	-7.82
928.00	1.52	162.22	927.91	-9.20	-0.67	9.20	0.20	0.06	-7.43
968.00	1.54	161.71	967.89	-10.22	-0.34	10.22	0.06	0.05	-1.28
Gyro Survey at 968' MD- 9667.89 TVD									
1,000.00	1.54	161.71	999.88	-11.03	-0.07	11.03	0.00	0.00	0.00
1,100.00	1.54	161.71	1,099.85	-13.59	0.77	13.59	0.00	0.00	0.00
1,200.00	1.54	161.71	1,199.81	-16.15	1.62	16.15	0.00	0.00	0.00
Casing Pt.> 1200' MD Drop -2.00									
1,210.00	1.34	161.71	1,209.81	-16.38	1.70	16.38	2.00	-2.00	0.00
13-3/8" Csg (1,200' TVD)									
1,277.12	0.00	0.00	1,276.92	-17.13	1.94	17.13	2.00	-2.00	0.00
Tangent> 1723 ft. at 1277 MD									
1,300.00	0.00	0.00	1,299.80	-17.13	1.94	17.13	0.00	0.00	0.00
1,400.00	0.00	0.00	1,399.80	-17.13	1.94	17.13	0.00	0.00	0.00
1,500.00	0.00	0.00	1,499.80	-17.13	1.94	17.13	0.00	0.00	0.00
1,600.00	0.00	0.00	1,599.80	-17.13	1.94	17.13	0.00	0.00	0.00
1,700.00	0.00	0.00	1,699.80	-17.13	1.94	17.13	0.00	0.00	0.00
1,800.00	0.00	0.00	1,799.80	-17.13	1.94	17.13	0.00	0.00	0.00
1,900.00	0.00	0.00	1,899.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,000.00	0.00	0.00	1,999.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,100.00	0.00	0.00	2,099.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,200.00	0.00	0.00	2,199.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,300.00	0.00	0.00	2,299.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,400.00	0.00	0.00	2,399.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,500.00	0.00	0.00	2,499.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,600.00	0.00	0.00	2,599.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,700.00	0.00	0.00	2,699.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,800.00	0.00	0.00	2,799.80	-17.13	1.94	17.13	0.00	0.00	0.00
2,900.00	0.00	0.00	2,899.80	-17.13	1.94	17.13	0.00	0.00	0.00
3,000.00	0.00	0.00	2,999.80	-17.13	1.94	17.13	0.00	0.00	0.00
Nudge KOP- Build> 2.00/100' MD									
3,100.00	2.00	61.33	3,099.78	-16.29	3.47	16.29	2.00	2.00	0.00
3,200.00	4.00	61.33	3,199.64	-13.78	8.07	13.78	2.00	2.00	0.00
3,286.41	5.73	61.33	3,285.73	-10.27	14.49	10.27	2.00	2.00	0.00
EOB-Tangent> 4153.77 ft. at 3286 MD									
3,300.00	5.73	61.33	3,299.26	-9.62	15.68	9.62	0.00	0.00	0.00
3,400.00	5.73	61.33	3,398.76	-4.83	24.44	4.83	0.00	0.00	0.00
3,500.00	5.73	61.33	3,498.26	-0.04	33.20	0.04	0.00	0.00	0.00
3,515.82	5.73	61.33	3,514.00	0.71	34.59	-0.71	0.00	0.00	0.00
Green River									
3,600.00	5.73	61.33	3,597.76	4.74	41.96	-4.74	0.00	0.00	0.00
3,700.00	5.73	61.33	3,697.26	9.53	50.71	-9.53	0.00	0.00	0.00

RECEIVED: Jun. 14, 2013

LEAM Drilling Systems LLC

Planning Report

LEAM Drilling Systems LLC

Database:	EDM 5000.1 Lynn Db	**Local Co-ordinate Reference:**	Well 1-17-3-2WH
Company:	NEWFIELD EXPLORATION ROCKY MOUNTAINS	**TVD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Project:	DUCHESNE COUNTY, UT (NAD 83)	**MD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Site:	CENTRAL BASIN (NAD 83)	**North Reference:**	True
Well:	1-17-3-2WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	1-17-3-2WH "LEJUENE"		
Design:	1-17-3-2WH REV02 LEJEUNE		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
3,800.00	5.73	61.33	3,796.76	14.32	59.47	-14.32	0.00	0.00	0.00
3,900.00	5.73	61.33	3,896.26	19.11	68.23	-19.11	0.00	0.00	0.00
4,000.00	5.73	61.33	3,995.76	23.90	76.99	-23.90	0.00	0.00	0.00
4,100.00	5.73	61.33	4,095.26	28.68	85.75	-28.68	0.00	0.00	0.00
4,200.00	5.73	61.33	4,194.76	33.47	94.50	-33.47	0.00	0.00	0.00
4,300.00	5.73	61.33	4,294.26	38.26	103.26	-38.26	0.00	0.00	0.00
4,400.00	5.73	61.33	4,393.76	43.05	112.02	-43.05	0.00	0.00	0.00
4,500.00	5.73	61.33	4,493.26	47.83	120.78	-47.83	0.00	0.00	0.00
4,600.00	5.73	61.33	4,592.76	52.62	129.53	-52.62	0.00	0.00	0.00
4,700.00	5.73	61.33	4,692.26	57.41	138.29	-57.41	0.00	0.00	0.00
4,800.00	5.73	61.33	4,791.77	62.20	147.05	-62.20	0.00	0.00	0.00
4,900.00	5.73	61.33	4,891.27	66.98	155.81	-66.98	0.00	0.00	0.00
5,000.00	5.73	61.33	4,990.77	71.77	164.56	-71.77	0.00	0.00	0.00
5,100.00	5.73	61.33	5,090.27	76.56	173.32	-76.56	0.00	0.00	0.00
5,200.00	5.73	61.33	5,189.77	81.35	182.08	-81.35	0.00	0.00	0.00
5,300.00	5.73	61.33	5,289.27	86.14	190.84	-86.14	0.00	0.00	0.00
5,400.00	5.73	61.33	5,388.77	90.92	199.59	-90.92	0.00	0.00	0.00
5,500.00	5.73	61.33	5,488.27	95.71	208.35	-95.71	0.00	0.00	0.00
5,534.90	5.73	61.33	5,523.00	97.38	211.41	-97.38	0.00	0.00	0.00
Trona									
5,579.13	5.73	61.33	5,567.00	99.50	215.28	-99.50	0.00	0.00	0.00
Mahogany Bench									
5,600.00	5.73	61.33	5,587.77	100.50	217.11	-100.50	0.00	0.00	0.00
5,700.00	5.73	61.33	5,687.27	105.29	225.87	-105.29	0.00	0.00	0.00
5,800.00	5.73	61.33	5,786.77	110.07	234.62	-110.07	0.00	0.00	0.00
5,900.00	5.73	61.33	5,886.27	114.86	243.38	-114.86	0.00	0.00	0.00
6,000.00	5.73	61.33	5,985.77	119.65	252.14	-119.65	0.00	0.00	0.00
6,100.00	5.73	61.33	6,085.27	124.44	260.90	-124.44	0.00	0.00	0.00
6,200.00	5.73	61.33	6,184.77	129.22	269.65	-129.22	0.00	0.00	0.00
6,300.00	5.73	61.33	6,284.28	134.01	278.41	-134.01	0.00	0.00	0.00
6,400.00	5.73	61.33	6,383.78	138.80	287.17	-138.80	0.00	0.00	0.00
6,446.46	5.73	61.33	6,430.00	141.02	291.24	-141.02	0.00	0.00	0.00
Garden Gulch Member (GG)									
6,500.00	5.73	61.33	6,483.28	143.59	295.93	-143.59	0.00	0.00	0.00
6,600.00	5.73	61.33	6,582.78	148.38	304.69	-148.38	0.00	0.00	0.00
6,700.00	5.73	61.33	6,682.28	153.16	313.44	-153.16	0.00	0.00	0.00
6,708.77	5.73	61.33	6,691.00	153.58	314.21	-153.58	0.00	0.00	0.00
Garden Gulch Member-1 (GG-1)									
6,800.00	5.73	61.33	6,781.78	157.95	322.20	-157.95	0.00	0.00	0.00
6,877.61	5.73	61.33	6,859.00	161.67	329.00	-161.67	0.00	0.00	0.00
Garden Gulch Member-2 (GG-2)									
6,900.00	5.73	61.33	6,881.28	162.74	330.96	-162.74	0.00	0.00	0.00
7,000.00	5.73	61.33	6,980.78	167.53	339.72	-167.53	0.00	0.00	0.00
7,100.00	5.73	61.33	7,080.28	172.31	348.47	-172.31	0.00	0.00	0.00
7,200.00	5.73	61.33	7,179.78	177.10	357.23	-177.10	0.00	0.00	0.00
7,300.00	5.73	61.33	7,279.28	181.89	365.99	-181.89	0.00	0.00	0.00
7,400.00	5.73	61.33	7,378.78	186.68	374.75	-186.68	0.00	0.00	0.00
7,440.18	5.73	61.33	7,418.76	188.60	378.26	-188.60	0.00	0.00	0.00
Nudge Drop> -1.50/100' MD									
7,500.00	4.83	61.33	7,478.33	191.24	383.09	-191.24	1.50	-1.50	0.00
7,568.87	3.80	61.33	7,547.00	193.73	387.64	-193.73	1.50	-1.50	0.00

LEAM Drilling Systems LLC

Planning Report

LEAM Drilling Systems LLC

Database:	EDM 5000.1 Lynn Db	**Local Co-ordinate Reference:**	Well 1-17-3-2WH
Company:	NEWFIELD EXPLORATION ROCKY MOUNTAINS	**TVD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Project:	DUCHESNE COUNTY, UT (NAD 83)	**MD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Site:	CENTRAL BASIN (NAD 83)	**North Reference:**	True
Well:	1-17-3-2WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	1-17-3-2WH "LEJUENE"		
Design:	1-17-3-2WH REV02 LEJEUNE		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
Douglas Creek Member									
7,600.00	3.33	61.33	7,578.07	194.65	389.34	-194.65	1.50	-1.50	0.00
7,700.00	1.83	61.33	7,677.97	196.81	393.29	-196.81	1.50	-1.50	0.00
7,800.00	0.33	61.33	7,777.95	197.72	394.94	-197.72	1.50	-1.50	0.00
7,822.05	0.00	0.00	7,800.00	197.75	395.00	-197.75	1.50	-1.50	0.00
Nudge Vert. Pt.> 7822 MD- 7800 TVD									
7,900.00	0.00	0.00	7,877.95	197.75	395.00	-197.75	0.00	0.00	0.00
8,000.00	0.00	0.00	7,977.95	197.75	395.00	-197.75	0.00	0.00	0.00
8,100.00	0.00	0.00	8,077.95	197.75	395.00	-197.75	0.00	0.00	0.00
8,139.05	0.00	0.00	8,117.00	197.75	395.00	-197.75	0.00	0.00	0.00
B-Limestone									
8,200.00	0.00	0.00	8,177.95	197.75	395.00	-197.75	0.00	0.00	0.00
8,300.00	0.00	0.00	8,277.95	197.75	395.00	-197.75	0.00	0.00	0.00
8,332.24	0.00	0.00	8,310.18	197.75	395.00	-197.75	0.00	0.00	0.00
Lower Black Shale(8302' @ 0'VS)									
8,381.85	0.00	0.00	8,359.80	197.75	395.00	-197.75	0.00	0.00	0.00
9-5/8" Casing Pt. (50' into Black Shale)									
8,382.05	0.00	0.00	8,360.00	197.75	395.00	-197.75	0.00	0.00	0.00
9-5/8" Csg (8,360' TVD)									
8,400.00	0.00	0.00	8,377.95	197.75	395.00	-197.75	0.00	0.00	0.00
8,411.85	0.00	0.00	8,389.80	197.75	395.00	-197.75	0.00	0.00	0.00
Curve-KOP- Build Rate> 14.72°/100' MD									
8,425.00	1.94	178.18	8,402.94	197.53	395.01	-197.53	14.72	14.72	0.00
8,446.22	5.06	178.18	8,424.12	196.23	395.05	-196.23	14.72	14.72	0.00
Castle Peak Limestone									
8,450.00	5.62	178.18	8,427.89	195.88	395.06	-195.88	14.72	14.72	0.00
8,475.00	9.30	178.18	8,452.67	192.64	395.16	-192.64	14.72	14.72	0.00
8,500.00	12.98	178.18	8,477.19	187.82	395.32	-187.82	14.72	14.72	0.00
8,525.00	16.66	178.18	8,501.36	181.43	395.52	-181.43	14.72	14.72	0.00
8,550.00	20.34	178.18	8,525.06	173.50	395.77	-173.50	14.72	14.72	0.00
8,575.00	24.02	178.18	8,548.21	164.07	396.07	-164.07	14.72	14.72	0.00
8,600.00	27.70	178.18	8,570.70	153.18	396.42	-153.18	14.72	14.72	0.00
8,619.74	30.60	178.18	8,587.94	143.57	396.72	-143.57	14.72	14.72	0.00
CP LIMES_2									
8,625.00	31.38	178.18	8,592.45	140.86	396.81	-140.86	14.72	14.72	0.00
8,650.00	35.06	178.18	8,613.36	127.18	397.24	-127.18	14.72	14.72	0.00
8,675.00	38.74	178.18	8,633.35	112.18	397.72	-112.18	14.72	14.72	0.00
8,700.00	42.42	178.18	8,652.34	95.93	398.24	-95.93	14.72	14.72	0.00
8,725.00	46.10	178.18	8,670.24	78.49	398.79	-78.49	14.72	14.72	0.00
8,750.00	49.78	178.18	8,686.99	59.94	399.38	-59.94	14.72	14.72	0.00
8,775.00	53.46	178.18	8,702.51	40.36	400.00	-40.36	14.72	14.72	0.00
8,791.61	55.90	178.18	8,712.11	26.81	400.43	-26.81	14.72	14.72	0.00
Uteland Butte									
8,800.00	57.14	178.18	8,716.74	19.82	400.65	-19.82	14.72	14.72	0.00
8,816.22	59.52	178.18	8,725.25	6.03	401.09	-6.03	14.72	14.72	0.00
Uteland Butte A									
8,825.00	60.82	178.18	8,729.62	-1.59	401.33	1.59	14.72	14.72	0.00
8,843.51	63.54	178.18	8,738.26	-17.95	401.85	17.95	14.72	14.72	0.00
Uteland Butte B									
8,850.00	64.50	178.18	8,741.10	-23.78	402.04	23.78	14.72	14.72	0.00

RECEIVED: Jun. 14, 2013

LEAM Drilling Systems LLC

Planning Report

LEAM Drilling Systems LLC

Database:	EDM 5000.1 Lynn Db	**Local Co-ordinate Reference:**	Well 1-17-3-2WH
Company:	NEWFIELD EXPLORATION ROCKY MOUNTAINS	**TVD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Project:	DUCHESNE COUNTY, UT (NAD 83)	**MD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Site:	CENTRAL BASIN (NAD 83)	**North Reference:**	True
Well:	1-17-3-2WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	1-17-3-2WH "LEJUENE"		
Design:	1-17-3-2WH REV02 LEJEUNE		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
8,875.00	68.18	178.18	8,751.13	-46.66	402.77	46.66	14.72	14.72	0.00
8,900.00	71.86	178.18	8,759.67	-70.14	403.51	70.14	14.72	14.72	0.00
8,916.39	74.27	178.18	8,764.45	-85.81	404.01	85.81	14.72	14.72	0.00
Uteland Butte C									
8,925.00	75.54	178.18	8,766.69	-94.12	404.27	94.12	14.72	14.72	0.00
8,950.00	79.22	178.18	8,772.15	-118.50	405.05	118.50	14.72	14.72	0.00
8,958.98	80.54	178.18	8,773.73	-127.33	405.33	127.33	14.72	14.72	0.00
U.B. C-PZ1									
8,975.00	82.90	178.18	8,776.04	-143.18	405.83	143.18	14.72	14.72	0.00
9,000.00	86.58	178.18	8,778.33	-168.06	406.62	168.06	14.72	14.72	0.00
9,018.97	89.37	178.18	8,779.00	-187.00	407.23	187.00	14.72	14.72	0.00
Land Pt.(89.37° Angle) 9019 MD- 8779 TVD									
9,023.94	89.37	178.18	8,779.05	-191.97	407.38	191.97	0.00	0.00	0.00
Landing Target									
9,100.00	89.37	178.18	8,779.89	-267.99	409.80	267.99	0.00	0.00	0.00
9,158.97	89.37	178.18	8,780.54	-326.92	411.67	326.92	0.00	0.00	0.00
Curve Build> 3.00°/100' MD									
9,200.00	90.60	178.18	8,780.55	-367.93	412.98	367.93	3.00	3.00	0.00
9,258.97	92.37	178.18	8,779.02	-426.85	414.85	426.85	3.00	3.00	0.00
Horz. Land Pt.(92.37° Angle) 9259 MD- 8779 TVD									
9,300.00	92.37	178.18	8,777.32	-467.83	416.15	467.83	0.00	0.00	0.00
9,400.00	92.37	178.18	8,773.19	-567.69	419.32	567.69	0.00	0.00	0.00
9,500.00	92.37	178.18	8,769.05	-667.55	422.50	667.55	0.00	0.00	0.00
9,600.00	92.37	178.18	8,764.92	-767.42	425.67	767.42	0.00	0.00	0.00
9,700.00	92.37	178.18	8,760.78	-867.28	428.84	867.28	0.00	0.00	0.00
9,800.00	92.37	178.18	8,756.65	-967.15	432.02	967.15	0.00	0.00	0.00
9,900.00	92.37	178.18	8,752.51	-1,067.01	435.19	1,067.01	0.00	0.00	0.00
10,000.00	92.37	178.18	8,748.38	-1,166.87	438.36	1,166.87	0.00	0.00	0.00
10,100.00	92.37	178.18	8,744.24	-1,266.74	441.54	1,266.74	0.00	0.00	0.00
10,200.00	92.37	178.18	8,740.11	-1,366.60	444.71	1,366.60	0.00	0.00	0.00
10,300.00	92.37	178.18	8,735.97	-1,466.47	447.88	1,466.47	0.00	0.00	0.00
10,400.00	92.37	178.18	8,731.84	-1,566.33	451.05	1,566.33	0.00	0.00	0.00
10,500.00	92.37	178.18	8,727.70	-1,666.20	454.23	1,666.20	0.00	0.00	0.00
10,600.00	92.37	178.18	8,723.57	-1,766.06	457.40	1,766.06	0.00	0.00	0.00
10,700.00	92.37	178.18	8,719.43	-1,865.92	460.57	1,865.92	0.00	0.00	0.00
10,800.00	92.37	178.18	8,715.30	-1,965.79	463.75	1,965.79	0.00	0.00	0.00
10,900.00	92.37	178.18	8,711.16	-2,065.65	466.92	2,065.65	0.00	0.00	0.00
11,000.00	92.37	178.18	8,707.03	-2,165.52	470.09	2,165.52	0.00	0.00	0.00
11,100.00	92.37	178.18	8,702.89	-2,265.38	473.27	2,265.38	0.00	0.00	0.00
11,200.00	92.37	178.18	8,698.75	-2,365.24	476.44	2,365.24	0.00	0.00	0.00
11,300.00	92.37	178.18	8,694.62	-2,465.11	479.61	2,465.11	0.00	0.00	0.00
11,400.00	92.37	178.18	8,690.48	-2,564.97	482.79	2,564.97	0.00	0.00	0.00
11,500.00	92.37	178.18	8,686.35	-2,664.84	485.96	2,664.84	0.00	0.00	0.00
11,600.00	92.37	178.18	8,682.21	-2,764.70	489.13	2,764.70	0.00	0.00	0.00
11,700.00	92.37	178.18	8,678.08	-2,864.56	492.31	2,864.56	0.00	0.00	0.00
11,800.00	92.37	178.18	8,673.94	-2,964.43	495.48	2,964.43	0.00	0.00	0.00
11,900.00	92.37	178.18	8,669.81	-3,064.29	498.65	3,064.29	0.00	0.00	0.00
12,000.00	92.37	178.18	8,665.67	-3,164.16	501.83	3,164.16	0.00	0.00	0.00
12,100.00	92.37	178.18	8,661.54	-3,264.02	505.00	3,264.02	0.00	0.00	0.00
12,200.00	92.37	178.18	8,657.40	-3,363.88	508.17	3,363.88	0.00	0.00	0.00
12,300.00	92.37	178.18	8,653.27	-3,463.75	511.35	3,463.75	0.00	0.00	0.00

LEAM Drilling Systems LLC

Planning Report

LEAM Drilling Systems LLC

Database:	EDM 5000.1 Lynn Db	**Local Co-ordinate Reference:**	Well 1-17-3-2WH
Company:	NEWFIELD EXPLORATION ROCKY MOUNTAINS	**TVD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Project:	DUCHESNE COUNTY, UT (NAD 83)	**MD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Site:	CENTRAL BASIN (NAD 83)	**North Reference:**	True
Well:	1-17-3-2WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	1-17-3-2WH "LEJUENE"		
Design:	1-17-3-2WH REV02 LEJEUNE		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
12,400.00	92.37	178.18	8,649.13	-3,563.61	514.52	3,563.61	0.00	0.00	0.00
12,500.00	92.37	178.18	8,645.00	-3,663.48	517.69	3,663.48	0.00	0.00	0.00
12,600.00	92.37	178.18	8,640.86	-3,763.34	520.87	3,763.34	0.00	0.00	0.00
12,700.00	92.37	178.18	8,636.73	-3,863.20	524.04	3,863.20	0.00	0.00	0.00
12,800.00	92.37	178.18	8,632.59	-3,963.07	527.21	3,963.07	0.00	0.00	0.00
12,900.00	92.37	178.18	8,628.46	-4,062.93	530.39	4,062.93	0.00	0.00	0.00
13,000.00	92.37	178.18	8,624.32	-4,162.80	533.56	4,162.80	0.00	0.00	0.00
13,100.00	92.37	178.18	8,620.18	-4,262.66	536.73	4,262.66	0.00	0.00	0.00
13,200.00	92.37	178.18	8,616.05	-4,362.52	539.91	4,362.52	0.00	0.00	0.00
13,238.31	92.37	178.18	8,614.47	-4,400.79	541.12	4,400.79	0.00	0.00	0.00
TD-PBHL(REV02) 13238 MD- 8614 TVD									

LEAM Drilling Systems LLC

Planning Report

LEAM Drilling Systems LLC

Database:	EDM 5000.1 Lynn Db	**Local Co-ordinate Reference:**	Well 1-17-3-2WH
Company:	NEWFIELD EXPLORATION ROCKY MOUNTAINS	**TVD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Project:	DUCHESNE COUNTY, UT (NAD 83)	**MD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Site:	CENTRAL BASIN (NAD 83)	**North Reference:**	True
Well:	1-17-3-2WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	1-17-3-2WH "LEJUENE"		
Design:	1-17-3-2WH REV02 LEJEUNE		

Design Targets

Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
SURFACE LOCATIOI	0.00	0.00	0.00	0.05	0.00	7,254,915.78	2,023,424.39	40° 13' 42.810 N	110° 7' 41.400 W
- plan misses target center by 0.05usft at 0.00usft MD (0.00 TVD, 0.00 N, 0.00 E)									
- Point									
Sec. 17, T3S-R2W, 6(	0.00	0.00	28.00	-432.01	468.45	7,254,490.96	2,023,899.42	40° 13' 38.540 N	110° 7' 35.360 W
- plan misses target center by 637.24usft at 28.00usft MD (28.00 TVD, 0.00 N, 0.00 E)									
- Polygon									
Point 1			28.00	0.00	0.00	7,254,490.96	2,023,899.42		
Point 2			28.00	-2,003.50	62.87	7,252,488.66	2,023,993.01		
Point 3			28.00	-3,968.54	122.64	7,250,524.77	2,024,082.91		
Point 4			28.00	-3,975.63	-514.21	7,250,507.91	2,023,446.24		
Point 5			28.00	-3,922.77	-3,954.47	7,250,508.00	2,020,005.57		
Point 6			28.00	-1,990.10	-3,997.63	7,252,439.79	2,019,932.78		
Point 7			28.00	-664.56	-4,001.32	7,253,765.11	2,019,908.76		
Point 8			28.00	-7.85	-3,989.60	7,254,421.93	2,019,910.40		
Point 9			28.00	0.00	0.00	7,254,490.96	2,023,899.42		
Sec. 17, T3S-R2W,	0.00	0.00	28.00	228.75	1,107.50	7,255,161.45	2,024,528.26	40° 13' 45.070 N	110° 7' 27.120 W
- plan misses target center by 1130.88usft at 28.00usft MD (28.00 TVD, 0.00 N, 0.00 E)									
- Polygon									
Point 1			28.00	0.00	0.00	7,255,161.45	2,024,528.26		
Point 2			28.00	-2,644.01	83.12	7,252,519.03	2,024,651.92		
Point 3			28.00	-5,282.95	164.70	7,249,881.65	2,024,773.96		
Point 4			28.00	-5,296.13	-1,155.59	7,249,848.22	2,023,454.03		
Point 5			28.00	-5,233.06	-5,239.01	7,249,848.66	2,019,370.12		
Point 6			28.00	-2,658.86	-5,296.76	7,252,421.67	2,019,272.90		
Point 7			28.00	-1,320.16	-5,300.41	7,253,760.16	2,019,248.72		
Point 8			28.00	-9.80	-5,276.15	7,255,070.73	2,019,252.88		
Point 9			28.00	0.00	0.00	7,255,161.45	2,024,528.26		
Nudge Vert. Pt.(1-17-:	0.00	359.06	7,800.00	197.75	395.00	7,255,119.52	2,023,816.32	40° 13' 44.764 N	110° 7' 36.307 W
- plan hits target center									
- Point									
TD-PBHL(1-17-3-2WI	0.00	359.06	8,614.00	-4,400.79	540.25	7,250,523.76	2,024,032.08	40° 12' 59.318 N	110° 7' 34.435 W
- plan misses target center by 0.99usft at 13238.30usft MD (8614.47 TVD, -4400.78 N, 541.12 E)									
- Point									
Land Pt.- 89.37° Angl(	0.00	359.06	8,779.00	-187.00	407.00	7,254,735.00	2,023,834.22	40° 13' 40.961 N	110° 7' 36.152 W
- plan misses target center by 0.23usft at 9018.96usft MD (8779.00 TVD, -186.99 N, 407.23 E)									
- Point									
Horz Land Pt.- 92.37°	0.00	0.00	8,779.00	-427.00	415.00	7,254,495.15	2,023,845.90	40° 13' 38.590 N	110° 7' 36.049 W
- plan misses target center by 0.15usft at 9259.12usft MD (8779.01 TVD, -427.01 N, 414.85 E)									
- Point									

Casing Points

Measured Depth (usft)	Vertical Depth (usft)	Name	Casing Diameter (")	Hole Diameter (")
1,210.00	1,209.81	13-3/8" Csg (1,200' TVD)	13-3/8	17-1/2
8,382.05	8,360.00	9-5/8" Csg (8,360' TVD)	9-5/8	9-5/8

RECEIVED: Jun. 14, 2013

LEAM Drilling Systems LLC

Planning Report

LEAM Drilling Systems LLC

Database:	EDM 5000.1 Lynn Db	**Local Co-ordinate Reference:**	Well 1-17-3-2WH
Company:	NEWFIELD EXPLORATION ROCKY MOUNTAINS	**TVD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Project:	DUCHESNE COUNTY, UT (NAD 83)	**MD Reference:**	WELL(5214'+28'= 5,242' MSL) @ 5242.00usft (Pioneer 44 (KB= 28'))
Site:	CENTRAL BASIN (NAD 83)	**North Reference:**	True
Well:	1-17-3-2WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	1-17-3-2WH "LEJUENE"		
Design:	1-17-3-2WH REV02 LEJEUNE		

Formations

Measured Depth (usft)	Vertical Depth (usft)	Name	Lithology	Dip (°)	Dip Direction (°)
3,515.82	-1,728.00	Green River		0.00	180.00
4,243.00	0.00	U.B. C-PZ2 HORZ Tgt		-2.37	180.00
4,243.00	0.00	Uteland Butte D		-2.37	180.00
4,243.00	0.00	Wasatch		-2.37	180.00
5,534.90	281.00	Trona		0.00	180.00
5,579.13	325.00	Mahogany Bench		0.00	180.00
6,446.46	1,188.00	Garden Gulch Member (GG)		0.00	180.00
6,708.77	1,449.00	Garden Gulch Member-1 (GG-1)		0.00	180.00
6,877.61	1,617.00	Garden Gulch Member-2 (GG-2)		0.00	180.00
7,568.87	2,305.00	Douglas Creek Member		0.00	180.00
8,139.05	2,875.00	B-Limestone		0.00	180.00
8,332.24	3,068.18	Lower Black Shale(8302' @ 0'VS)		-2.37	180.00
8,446.22	3,182.12	Castle Peak Limestone		-2.37	180.00
8,619.74	3,345.94	CP LIMES_2		-2.37	180.00
8,791.61	3,470.11	Uteland Butte		-2.37	180.00
8,816.22	3,483.25	Uteland Butte A		-2.37	180.00
8,843.51	3,496.26	Uteland Butte B		-2.37	180.00
8,916.39	3,522.45	Uteland Butte C		-2.37	180.00
8,958.98	3,531.73	U.B. C-PZ1		-2.37	180.00
9,023.94	3,537.05	Landing Target		-2.37	180.00

Plan Annotations

Measured Depth (usft)	Vertical Depth (usft)	Local Coordinates +N/-S (usft)	Local Coordinates +E/-W (usft)	Comment
968.00	967.89	-10.22	-0.34	Gyro Survey at 968' MD- 9667.89 TVD
1,200.00	1,199.81	-16.15	1.62	Casing Pt.> 1200' MD Drop -2.00
1,277.12	1,276.92	-17.13	1.94	Tangent> 1723 ft. at 1277 MD
3,000.00	2,999.80	-17.13	1.94	Nudge KOP- Build> 2.00/100' MD
3,286.41	3,285.73	-10.27	14.49	EOB-Tangent> 4153.77 ft. at 3286 MD
7,440.18	7,418.76	188.60	378.26	Nudge Drop> -1.50/100' MD
7,822.05	7,800.00	197.75	395.00	Nudge Vert. Pt.> 7822 MD- 7800 TVD
8,381.85	8,359.80	197.75	395.00	9-5/8" Casing Pt. (50' into Black Shale)
8,411.85	8,389.80	197.75	395.00	Curve-KOP- Build Rate> 14.72°/100' MD
9,018.97	8,779.00	-187.00	407.23	Land Pt.(89.37° Angle) 9019 MD- 8779 TVD
9,158.97	8,780.54	-326.92	411.67	Curve Build> 3.00°/100' MD
9,258.97	8,779.02	-426.85	414.85	Horz. Land Pt.(92.37° Angle) 9259 MD- 8779 TVD
13,238.31	8,614.47	-4,400.79	541.12	TD-PBHL(REV02) 13238 MD- 8614 TVD

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS, AND MINING

FORM 9

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

5.LEASE DESIGNATION AND SERIAL NUMBER: Patented

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

7.UNIT or CA AGREEMENT NAME:

1. TYPE OF WELL Oil Well

8. WELL NAME and NUMBER: Lejeune 1-17-3-2WH

2. NAME OF OPERATOR: NEWFIELD PRODUCTION COMPANY

9. API NUMBER: 43013518530000

3. ADDRESS OF OPERATOR: Rt 3 Box 3630 , Myton, UT, 84052

PHONE NUMBER: 435 646-4825 Ext

9. FIELD and POOL or WILDCAT: WILDCAT

4. LOCATION OF WELL
FOOTAGES AT SURFACE: 0227 FNL 1115 FEL
QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: Qtr/Qtr: NENE Section: 17 Township: 03.0S Range: 02.0W Meridian: U

COUNTY: DUCHESNE

STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

TYPE OF SUBMISSION	TYPE OF ACTION		
✓ NOTICE OF INTENT Approximate date work will start: 6/15/2013	☐ ACIDIZE	☐ ALTER CASING	☐ CASING REPAIR
	✓ CHANGE TO PREVIOUS PLANS	☐ CHANGE TUBING	☐ CHANGE WELL NAME
	☐ CHANGE WELL STATUS	☐ COMMINGLE PRODUCING FORMATIONS	☐ CONVERT WELL TYPE
☐ SUBSEQUENT REPORT Date of Work Completion:	☐ DEEPEN	☐ FRACTURE TREAT	☐ NEW CONSTRUCTION
	☐ OPERATOR CHANGE	☐ PLUG AND ABANDON	☐ PLUG BACK
☐ SPUD REPORT Date of Spud:	☐ PRODUCTION START OR RESUME	☐ RECLAMATION OF WELL SITE	☐ RECOMPLETE DIFFERENT FORMATION
	☐ REPERFORATE CURRENT FORMATION	☐ SIDETRACK TO REPAIR WELL	☐ TEMPORARY ABANDON
	☐ TUBING REPAIR	☐ VENT OR FLARE	☐ WATER DISPOSAL
☐ DRILLING REPORT Report Date:	☐ WATER SHUTOFF	☐ SI TA STATUS EXTENSION	☐ APD EXTENSION
	☐ WILDCAT WELL DETERMINATION	☐ OTHER	OTHER:

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

Newfield Production Company respectfully requests to increase the depth of the 9-5/8" intermediate casing on the subject well from the previously approved depth of 6,000' to 8,382'. This places the 9-5/8" shoe 50' into the Lower Black Shale formation. Offset well data shows the integrity of this shoe provides the best integrity to withstand the expected mud weight of 14 ppg at TD. The target formation remains unchanged. Updated drilling plan and horizontal plan are attached. This well is intended to spud this weekend.

Approved by the
Utah Division of
Oil, Gas and Mining

Date: 07-09-13

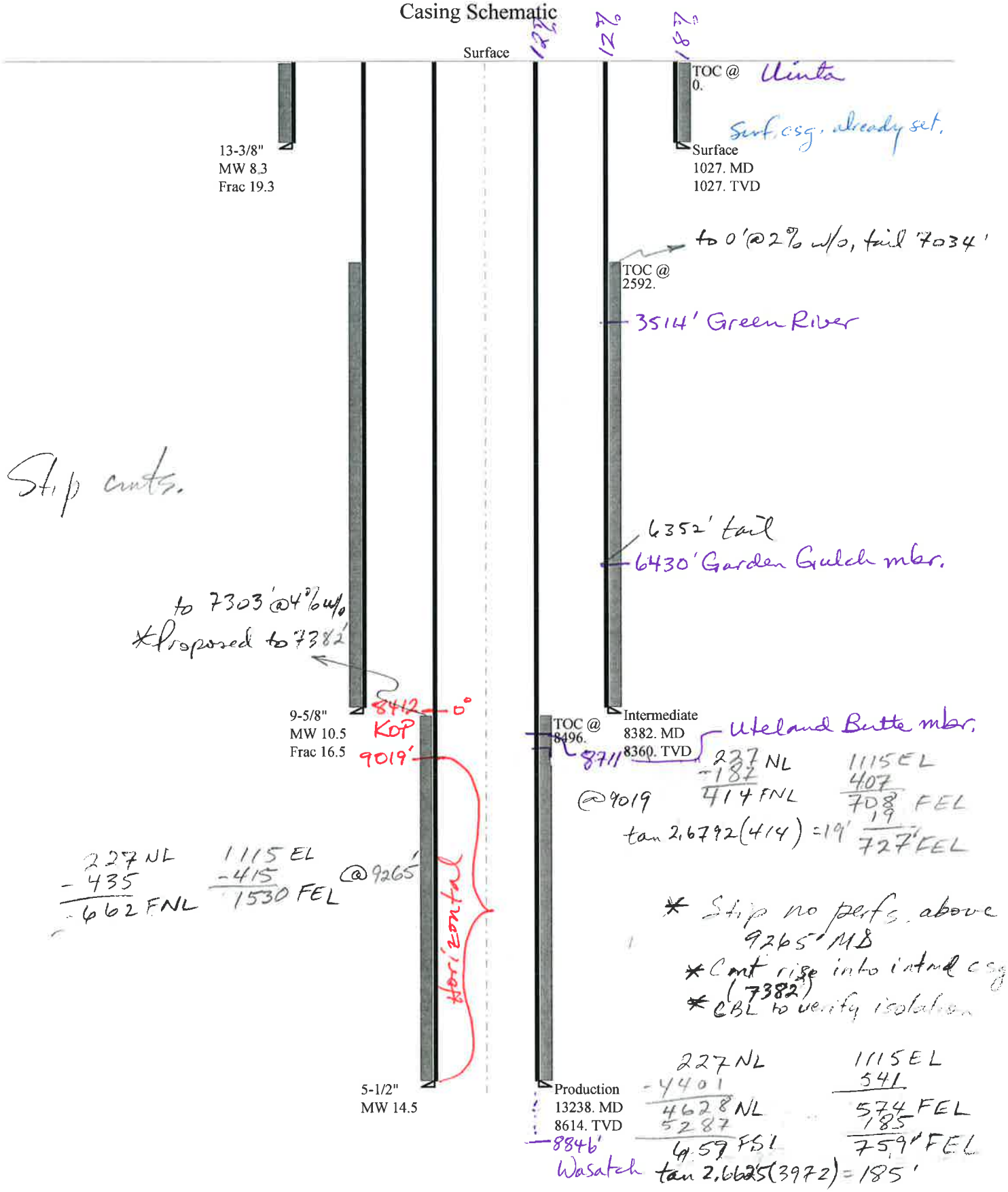
By:

NAME (PLEASE PRINT)	PHONE NUMBER	TITLE
Don Hamilton	435 719-2018	Permitting Agent
SIGNATURE		**DATE**
N/A		6/14/2013

RECEIVED: Jun. 14, 2013

43013518530000 Lejeune 1-17-3-2WHrev2

Casing Schematic



Well name:	**43013518530000 Lejeune 1-17-3-2WHrev2**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Surface
Project ID:	43-013-51853
Location:	DUCHESNE COUNTY

Design parameters:

Collapse
Mud weight: 8.330 ppg
Design is based on evacuated pipe.

Burst
Max anticipated surface pressure: 801 psi
Internal gradient: 0.220 psi/ft
Calculated BHP 1,027 psi

No backup mud specified.

Minimum design factors:

Collapse:
Design factor 1.125

Burst:
Design factor 1.00

Tension:
8 Round STC: 1.80 (J)
8 Round LTC: 1.70 (J)
Buttress: 1.60 (J)
Premium: 1.50 (J)
Body yield: 1.50 (B)

Tension is based on air weight.
Neutral point: 900 ft

Environment:
H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 88 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 100 ft

Cement top: Surface

Directional Info - Build & Build
Kick-off point 8412 ft
Departure at shoe: 15 ft
Maximum dogleg: .16 °/100ft
Inclination at shoe: 1.54 °

Re subsequent strings:
Next setting depth: 8,360 ft
Next mud weight: 10.500 ppg
Next setting BHP: 4,560 psi
Fracture mud wt: 19.250 ppg
Fracture depth: 1,027 ft
Injection pressure: 1,027 psi

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	1027	13.375	54.50	J-55	ST&C	1027	1027	12.49	12743

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	444	1130	2.543	1027	2730	2.66	56	514	9.18 J

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940
Date: June 13,2013
Salt Lake City, Utah

Remarks:
Collapse is based on a vertical depth of 1027 ft, a mud weight of 8.33 ppg The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.
Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

Well name:	**43013518530000 Lejeune 1-17-3-2WHrev2**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Intermediate
Project ID:	43-013-51853
Location:	DUCHESNE COUNTY

Design parameters:

Collapse

Mud weight:	10.500 ppg
Internal fluid density:	4.200 ppg

Burst

Max anticipated surface pressure:	4,594 psi
Internal gradient:	0.220 psi/ft
Calculated BHP	6,433 psi
Annular backup:	2.00 ppg

Minimum design factors:

Collapse:

Design factor	1.125

Burst:

Design factor	1.00

Tension:

8 Round STC:	1.80 (J)
8 Round LTC:	1.80 (J)
Buttress:	1.60 (J)
Premium:	1.50 (J)
Body yield:	1.60 (B)

Tension is based on air weight.
Neutral point: 7,074 ft

Environment:

H2S considered?	No
Surface temperature:	74 °F
Bottom hole temperature:	191 °F
Temperature gradient:	1.40 °F/100ft
Minimum section length:	1,000 ft
Cement top:	2,592 ft

Directional Info - Build & Build

Kick-off point	8412 ft
Departure at shoe:	445 ft
Maximum dogleg:	2 °/100ft
Inclination at shoe:	0 °

Re subsequent strings:

Next setting depth:	8,614 ft
Next mud weight:	14.500 ppg
Next setting BHP:	6,489 psi
Fracture mud wt:	16.500 ppg
Fracture depth:	8,360 ft
Injection pressure:	7,166 psi

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	8382	9.625	40.00	N-80	Buttress	8360	8382	8.75	114128

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	2736	3090	1.129	5564	5750	1.03	334.4	916.3	2.74 B

Prepared by: Helen Sadik-Macdonald, Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940
Date: June 13,2013
Salt Lake City, Utah

Remarks:
Collapse is based on a vertical depth of 8360 ft, a mud weight of 10.5 ppg An internal gradient of .218 psi/ft was used for collapse from TD
Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.
Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

Well name:	**43013518530000 Lejeune 1-17-3-2WHrev2**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Production
Project ID:	43-013-51853
Location:	DUCHESNE COUNTY

Design parameters:

Collapse
Mud weight: 14.500 ppg
Design is based on evacuated pipe.

Burst
Max anticipated surface pressure: 4,594 psi
Internal gradient: 0.220 psi/ft
Calculated BHP 6,489 psi

No backup mud specified.

Minimum design factors:

Collapse:
Design factor 1.125

Burst:
Design factor 1.00

Tension:
8 Round STC: 1.80 (J)
8 Round LTC: 1.80 (J)
Buttress: 1.60 (J)
Premium: 1.50 (J)
Body yield: 1.60 (B)

Tension is based on air weight.
Neutral point: 6,741 ft

Environment:
H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 195 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 1,000 ft

Cement top: 8,496 ft

Directional Info - Build & Build
Kick-off point 8412 ft
Departure at shoe: 4436 ft
Maximum dogleg: 14.72 °/100ft
Inclination at shoe: 92.37 °

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	13238	5.5	20.00	P-110	Buttress	8614	13238	4.653	109825

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	6489	11100	1.711	6525	12360	1.89	172.3	641.1	3.72 B

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940
Date: June 13,2013
Salt Lake City, Utah

Remarks:
Collapse is based on a vertical depth of 8614 ft, a mud weight of 14.5 ppg The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.
Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

Helen Sadik-Macdonald <hmacdonald@utah.gov>

RE: Lejeune 1-17-3-2WHrev2

1 message

Sean Stevens <sstevens@newfield.com> Tue, Jul 9, 2013 at 7:00 AM
To: Helen Sadik-Macdonald <hmacdonald@utah.gov>, "starpoint@etv.net" <starpoint@etv.net>
Cc: Dustin Doucet <dustindoucet@utah.gov>, Brad Hill <bradhill@utah.gov>, Kirby Carroll <kcarroll@newfield.com>

Hello Helen,

I got your voicemail yesterday. Here's a quick email addressing your concerns. I will also call you back later this morning to discuss in greater detail.

I believe I have some explanations for your concerns:

1. The well bore as planned in the directional survey becomes horizontal at 9019' , but is only 414' FNL of section 17.

    a. On wells we plan to cement the lateral, we intentionally plan to land horizontal prior to reaching the 660' setback on our directional plans to account for geologic uncertainty. If the geologists are 100% correct on where they think we will intersect our horizontal target, then yes, in fact we will land at 414' FNL. The entire lateral will be cemented and isolated and our completion team will ensure their perforations will not be outside the 660' setback. I have yet to see the geologist be 100% correct. What ends up happening is our targets shift as we see formations come in and we end up landing inside our setback and we actually lose some productive lateral length. This design limits the amount of wasted productive lateral length inside the setback. We never intend to perforate or produce outside the setback.

2. At proposed TD of 13238' , proposed bore was approx 600' FEL.

    a. I believe you may be using the footage calls to calculate this. If so, this section is not actually square. The Eastern setback line runs at an azimuth of 277.3 (or 2.7 degrees east of due south) when you convert the degrees-minutes-seconds call. If you do the trigonometry on the 2.7 degree triangle (sin 2.7*3972 = 187'), The BHL shifts 187' to the east relative to the "top of producing interval" on the plat. If you are referring to a different issue, we can discuss that over the phone.

Thanks,

Sean Stevens
Engineer.Drilling
Office: 303-382-4481 Ext 4481
Mobile: 435-823-1162

NEWFIELD

CONFIDENTIAL

BLM - Vernal Field Office - Notification Form

Operator Newfield Exploration Rig Name/# Pioneer 44 Submitted By Mike Woolsey/ Dustin Edwards Phone Number 435-632-5240
Well Name/Number Lejeune 1-17-3-2WH
Qtr/Qtr NE/NE Section 17 Township 3S Range 2W
Lease Serial Number FEE
API Number 43013518530000

Spud Notice – Spud is the initial spudding of the well, not drilling out below a casing string.

Date/Time _____ _____ AM ☐ PM ☐

Casing – Please report time casing run starts, not cementing times.

☐ Surface Casing
☐ Intermediate Casing
☐ Production Casing
☐ Liner
☐ Other

Date/Time _____ _____ AM ☐ PM ☐

BOPE

☒ Initial BOPE test at surface casing point
☐ BOPE test at intermediate casing point
☐ 30 day BOPE test
☐ Other

RECEIVED
JUN 13 2013
DIV. OF OIL, GAS & MINING

Date/Time 6/14/2013 06:00 AM ☒ PM ☐

Remarks _____

EAGER BEAVER TESTERS INC.

P.O. BOX 1616
ROCK SPRINGS, WY 82902

PHONE:
CASPER - (307) 265-8147
ROCK SPRINGS - (307) 382-3350

RECEIVED
JUN 19 2013
DIV. OF OIL, GAS & MINING

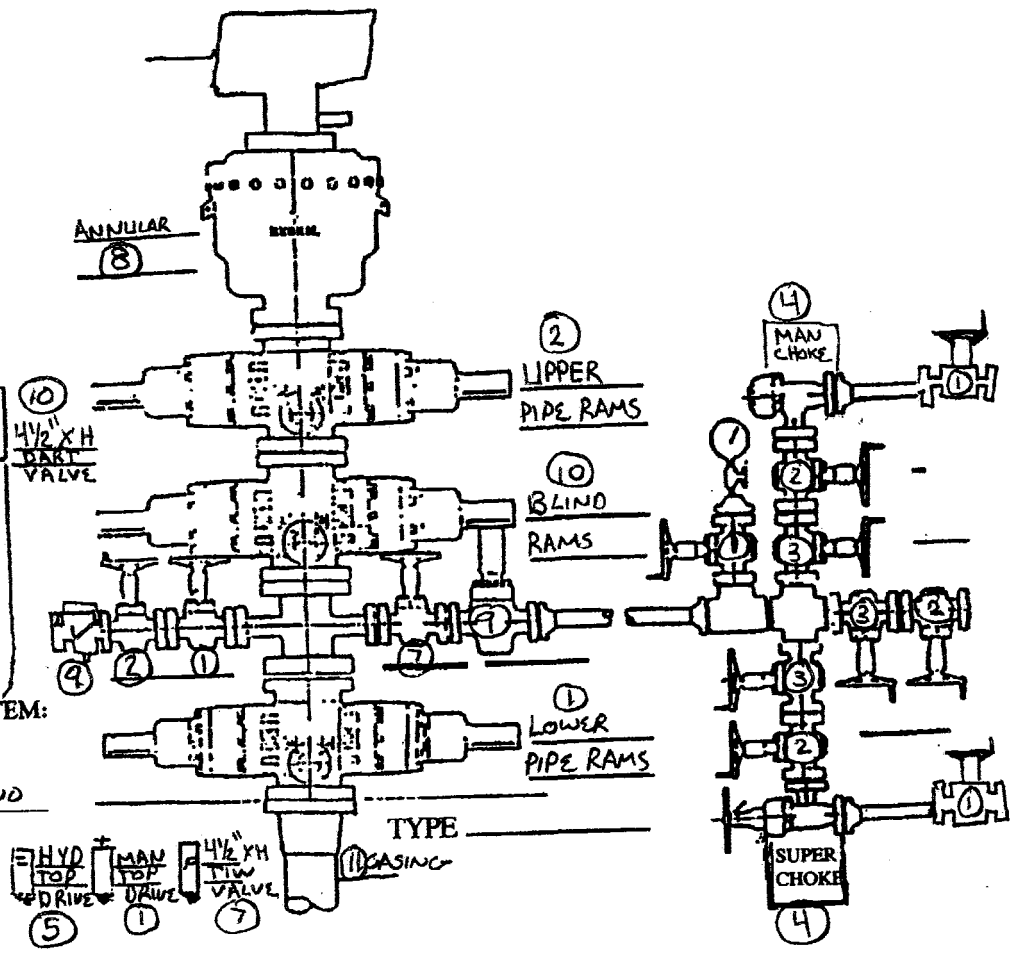
BOP TEST REPORT

DATE: 6-14-13 OPERATOR: NEWFIELD RIG OR SITE#: PIONEER 44 SEC: 17 TNSHIP: 35OUTH RANGE: 3WEST

FIELD: FEE WELL#: LEJEUNE 1-17-3-2WH TEST PRESSURE: 250PSI/5MIN & 5,000PSI/10MIN

EQUIPMENT PRESSURE TESTED:

ANNULAR ~~50%~~ 3,500	(8)
UPPER PIPE RAMS	(2)
LOWER PIPE RAMS	(1)
BLIND RAMS	(10)
KILL LINE VALVES	(1)(2)(9)
HCR VALVE	(9)
CHOKE VALVES	(7)
MANIFOLD VALVES	(1)(2)(3)
SUPER CHOKE	(4)
MANUAL CHOKE MANIFOLD	(4)
UPPER KELLY VALVE HYD	(5)
LOWER KELLY VALVE MAN	(1)
INSIDE BOP	(10)
FLOOR VALVE (TIW)	(7)
CASING PRE. 1500	(11)



ACCUMULATOR AND CLOSING SYSTEM:

NITROGEN PRECHARGE PSI 900↑
FIELD CHECK X GUAGE CHECK NO
BOTTLES X SPHERES NO

FUNCTION CHECK 1500PSI
PUMP CHECK 1MIN 21SEC.
REMOTE OPERATION CHECK NO
HYDRAULIC FLUID LEVEL ✓

OTHER TESTS: (6) MUDLINE - FAIL
(12) RETEST MUDLINE @ 250PSI/5MIN & 5,000PSI/10MIN

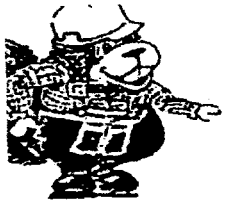
EQUIPMENT TYPE _____ PRESSURE _____

*PLEASE NOTE: CONFIGURATION OF B.O.P COMPONENTS DOES NOT MATCH THIS DRAWING DUE TO MUD CROSS ASSEMBLY BEING CONFIGURED BELOW LOWER PIPE RAMS.

REPAIRS OR POTENTIAL PROBLEMS:

REPLACED & REPAIRED ALL MUDLINE VALVES EXCEPT FOR STAND PIPE VALVE & 2" BLEED OFFS ON PUMPS, TIGHTENED FLANGES IN CHOKE HOUSE, GREASED STEMS AND CYCLED VALVES THAT HAD USABLE BODY PRESSURE SEEPAGE THROUGH STEM PACKING (MULTIBLE VALVES IN SYSTEM)

RECEIVED
JUN 19 2013
DIV. OF OIL, GAS & MINING



EAGER BEAVER TESTERS

DATE: 8-14-2015 COMPANY: NEWFIELD RIG: PIONEER 44 WELL NAME & #: LEJEUNE 1-17-3-2W H

ACCUMULATOR FUNCTION TESTS

TO CHECK THE USABLE FLUID STORED IN THE NITROGEN BOTTLES ON THE ACCUMULATOR

O.S.O. #2 SECTION iii, A.3.C.1. OR II OR III)

1. Make sure all rams and annular are open and if applicable HCR is closed
2. Ensure accumulator is pumped up to working pressure! (shut off pumps)
3. Open HCR Valve (if applicable)
4. Close annular
5. Close all pipe rams
6. Open one set of the pipe rams to simulate closing the blind ram
7. If you have a 3 ram stack open the annular to achieve the 50%+ safety factor for 5M and greater systems
8. Accumulator pressure should be 200 psi over desired precharge pressure, (accumulator working pressure (1500 psi= 750 desired psi) (2000 and 3000 psi= 100 desired psi)
9. Record the remaining pressure 1500 PSI

TO CHECK THE CAPACITY OF THE ACCUMULATOR PUMPS

(O.S.O. #2 SECTION III.A.2.F.)

. Shut the accumulator bottles or spherical, (isolate them from the pumps and manifold) Open the bleed off valve to the tank, (manifold psi should go to 0 psi) close bleed valve.

:. Open the HCR valve (if applicable)

. Close annular

. With pumps only, time how long it takes to regain manifold pressure to 200 psi over desired precharge pressure! (Accumulator working pressure {1500 psi=750 desired psi} {2000 and 3000 psi= 1000 desired psi})

. Record elapsed time 1 MIN 21 SEC. (2 minutes or less)

TO CHECK THE PRECHARGE ON BOTTLES OR SPHERICAL

(O.S.O. #2 SECTION III.A.2.D.)

. Open bottles back up to the manifold (pressure should be above the desired precharge pressure, (1500 psi=750 desired psi) (2000 and 3000 psi= 1000 desired psi) may need to use pumps to pressure back up.

. With power to pumps shut off open bleed line to the tank

. Watch and record where the pressure drops (accumulator psi)

. Record the pressure drop 900 ↑ PSI

If pressure drops below the minimum precharge, (accumulator working pressure {1500 psi=700 min}{2000 and 3000 psi= 900 psi min.}) each bottle shall be independently checked with a gauge.

EAGER BEAVER TESTERS

DATE: 6-14-2013 COMPANY: NEWFIELD RIG: PIONEER 44 WELL NAME & #: LEJEUNE 1-17-3-2WH

Time		Test No.		Results
4:11	AM □PM☒	1	MANUAL TOP DRIVE, LOWER PIPE RAMS, INSIDE KILL LINE, DOWNSTREAM CHOKE MANIFOLD, RISER	Pass ☒Fail □
4:39	AM □PM☒	2	UPPER PIPE RAMS, OUTSIDE CHOKE MANIFOLD VALVES, OUTSIDE KILL LINE VALVE	Pass ☒Fail □
5:52	AM □PM☒	3	INSIDE CHOKE MANIFOLD VALVES	Pass ☒Fail □
6:30	AM □PM☒	4	SUPER CHOKE, MANUAL CHOKE	Pass ☒Fail □
6:53	AM □PM☒	5	HYDRAULIC TOP DRIVE	Pass ☒Fail □
7:30	AM □PM☒	6	MUD LINE	Pass □Fail ☒
8:59	AM □PM☒	7	4 1/2" X-HOLE F.O.S.V. (TIW), MANUAL CHOKE LINE VALVE	Pass ☒Fail □
9:25	AM □PM☒	8	ANNULAR	Pass ☒Fail □
2:18	AM ☒PM□	9	HCR, KILL LINE CHECK VALVE	Pass ☒Fail □
2:45	AM ☒PM□	10	BLIND RAMS, 4 1/2" X-HOLE DART VALVE	Pass ☒Fail □
3:57	AM ☒PM□	11	CASING	Pass ☒Fail □
5:40	AM ☒PM□	12	MUD LINE	Pass ☒Fail □
	AM □PM□	13		Pass □Fail □
	AM □PM□	14		Pass □Fail □
	AM □PM□	Retest		Pass □Fail □
	AM □PM□	Retest		Pass □Fail □
	AM □PM□	Retest		Pass □Fail □
	AM □PM□	Retest		Pass □Fail □
	AM □PM□	Retest		Pass □Fail □
	AM □PM□	Retest		Pass □Fail □
	AM □PM□	Retest		Pass □Fail □

Acc. Tank Size (inches) (_____W_____D_____L) ÷ 231=_____gal.

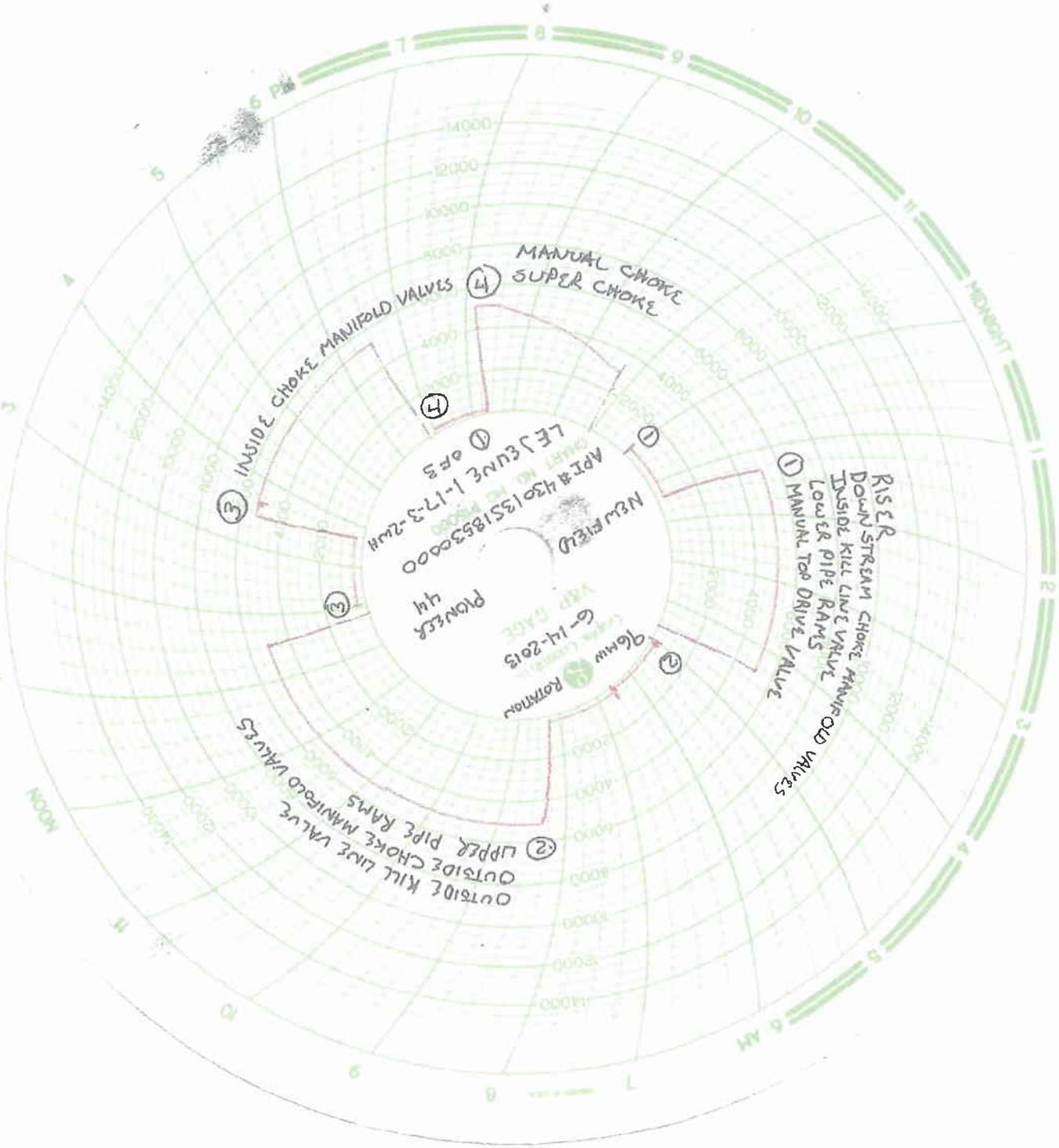
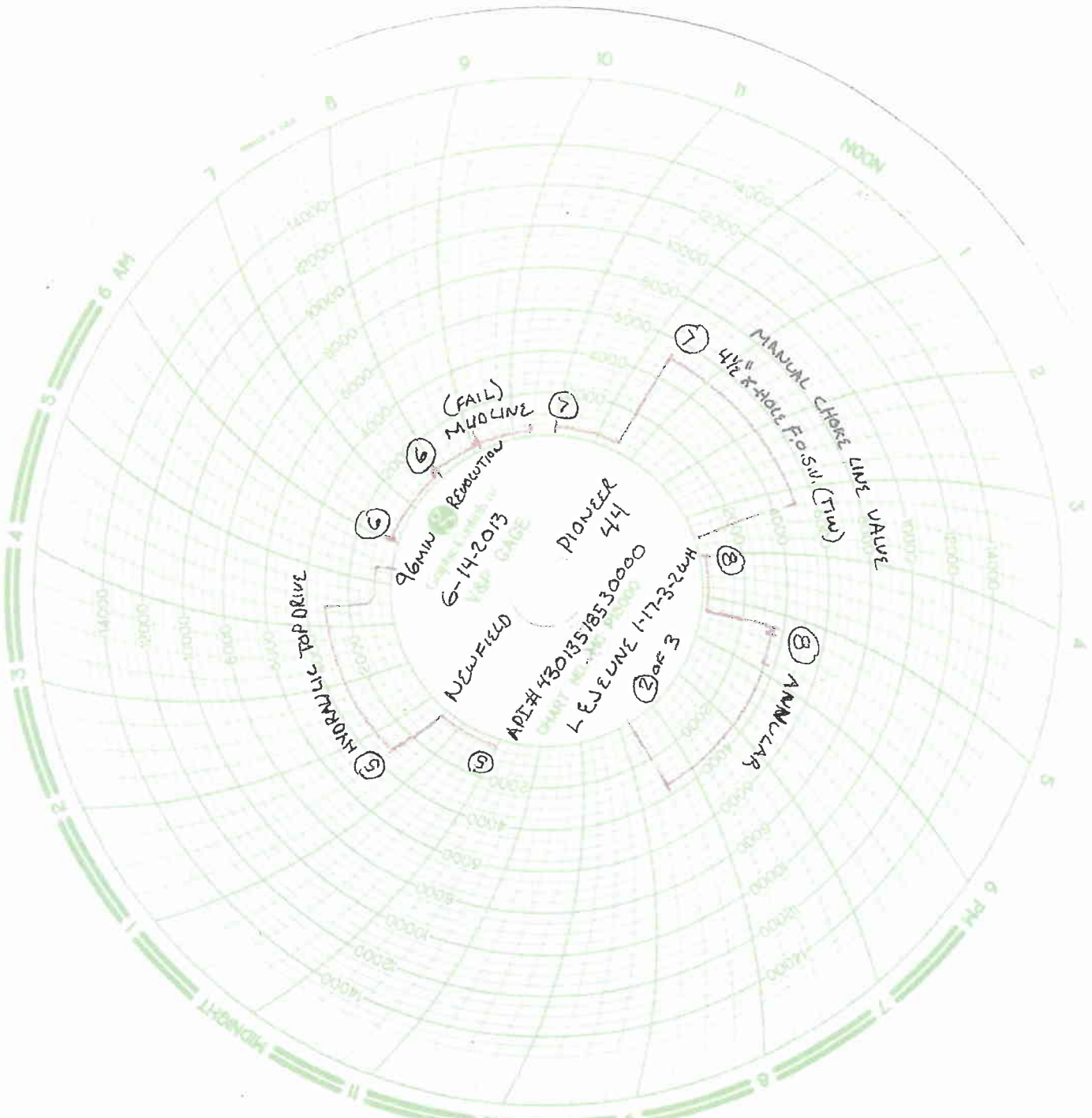
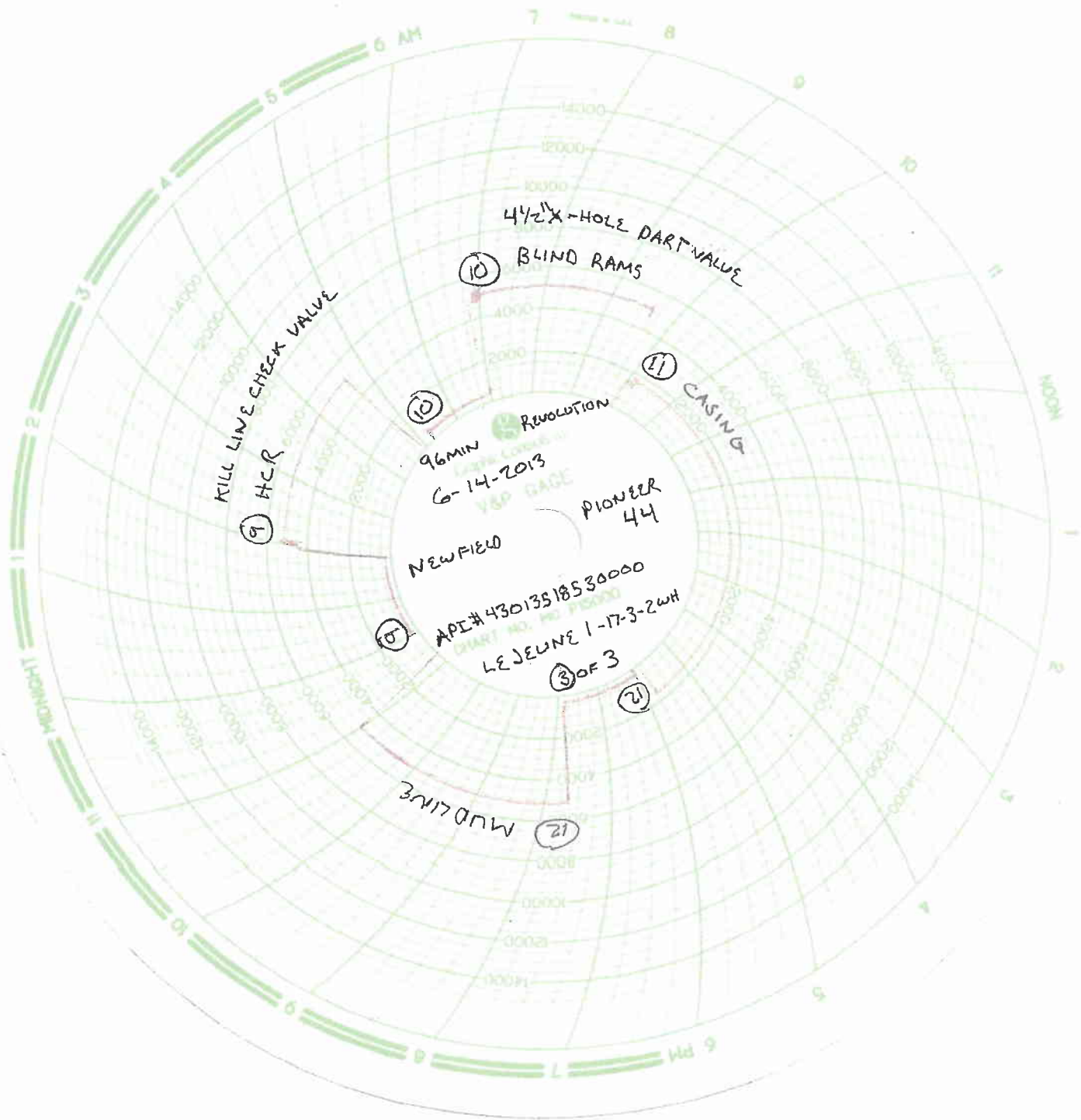


Chart # 2 on Reverse


MANUAL CHOKE LINE VALVE
4½" 8-HOLE F.O.S.V. (TIW)
(FAIL) MUD LINE
REDUCTION
96MIN
6-14-2013
PIONEER 44
API#4301351853000
LEJEUNE 1-17-3-2WH
2 OF 3
NEWFIELD
HYDRAULIC TOP DRIVE
MANUAL
NOON
MIDNIGHT


4½" X-HOLE DART VALVE
10 BLIND RAMS
KILL LINE CHECK VALVE
9 HCR
11 CASING
10
96 MIN
REVOLUTION
6-14-2013
PIONEER
44
NEWFIELD
API# 43013518530000
LEJEUNE 1-17-3-2WH
3 OF 3
21
MUD LINE
21

CONFIDENTIAL

BLM - Vernal Field Office - Notification Form

Operator Newfield Exploration Rig Name/# Pioneer 44 Submitted By Alvin nielsen/ Joe Johnson Phone Number 713-948-9196
Well Name/Number Lejeune 1-17-3-2WH
Qtr/Qtr NE/NE Section 17 Township 3S Range 2W
Lease Serial Number FEE
API Number 4301351850000

Spud Notice – Spud is the initial spudding of the well, not drilling out below a casing string.

Date/Time _____ _____ AM ☐ PM ☐

Casing – Please report time casing run starts, not cementing times.

☐ Surface Casing
☒ Intermediate Casing
☐ Production Casing
☐ Liner
☐ Other

Date/Time 7/1/2013 06:30 AM ☒ PM ☐

BOPE

☐ Initial BOPE test at surface casing point
☒ BOPE test at intermediate casing point
☐ 30 day BOPE test
☐ Other

RECEIVED
JUN 20 2013
DIV. OF OIL, GAS & MINING

Date/Time 7/2/2013 00:00 AM ☒ PM ☐

Remarks _____

EAGER BEAVER TESTERS INC.

P.O. BOX 1616
ROCK SPRINGS, WY 82902

PHONE:
CASPER - (307) 265-8147
ROCK SPRINGS - (307) 382-3350

43 013 51853

BOP TEST REPORT

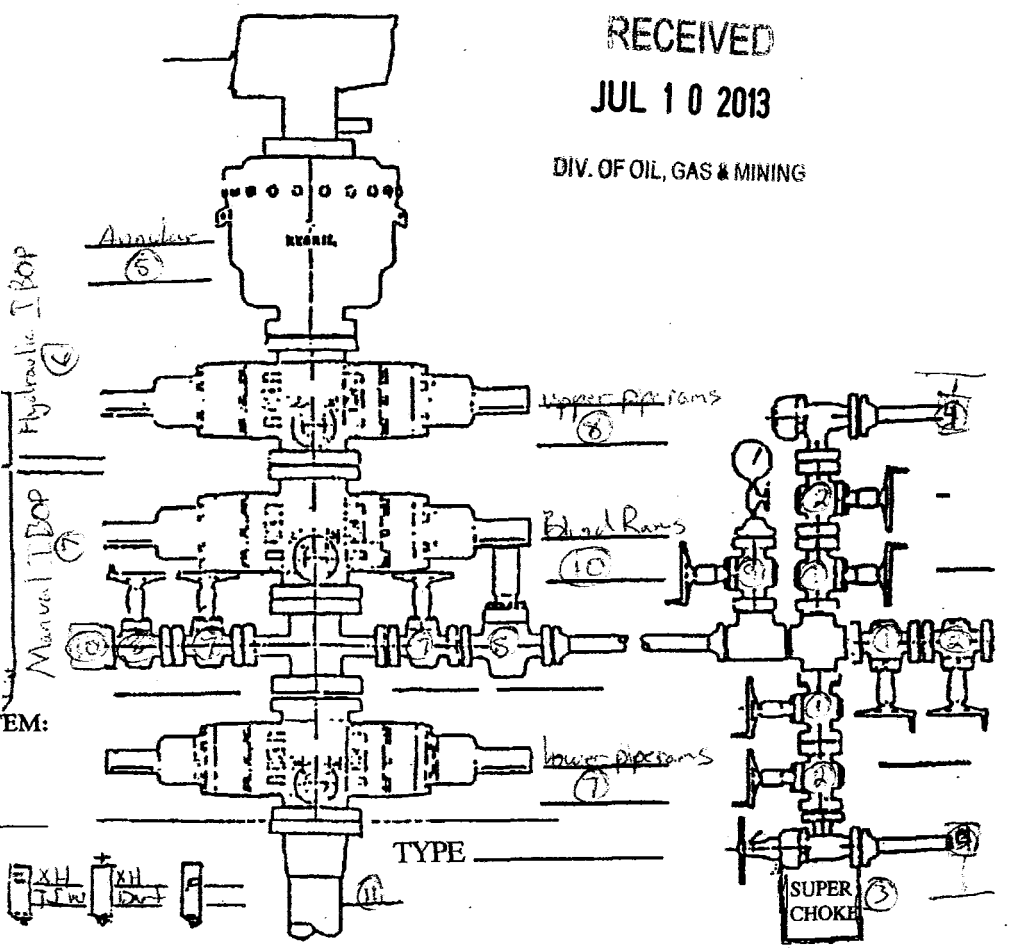
DATE: 7-3-13 OPERATOR: Newfield RIG OR SITE#: pioneer 44 SEC: 17 TNSHIP: 3S RANGE: ~~3W~~ 2W

FIELD: Lejeune WELL#: Lejeune 1-17-3-2WH TEST PRESSURE: 250/7000 psi

EQUIPMENT PRESSURE TESTED:

ANNULAR 50%	5
UPPER PIPE RAMS	8
LOWER PIPE RAMS	7
BLIND RAMS	10
KILL LINE VALVES	7,8
HCR VALVE	8
CHOKE VALVES	7
MANIFOLD VALVES	1,2
SUPER CHOKE	3
MANUAL CHOKE	N/A
UPPER KELLY VALVE	6
LOWER KELLY VALVE	7
INSIDE BOP	8
FLOOR VALVE	9
CASING PRE. 1500	11

RECEIVED
JUL 10 2013
DIV. OF OIL, GAS & MINING



ACCUMULATOR AND CLOSING SYSTEM:

NITROGEN PRECHARGE PSI 1050 psi
FIELD CHECK ✓ GUAGE CHECK ____
BOTTLES ✓ SPHERES ____

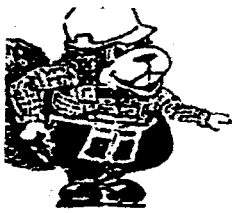
FUNCTION CHECK 51 sec
PUMP CHECK 1550 psi
REMOTE OPERATION CHECK ✓
HYDRAULIC FLUID LEVEL ✓

OTHER TESTS:

EQUIPMENT TYPE ____ PRESSURE ____

REPAIRS OR POTENTIAL PROBLEMS:

RECEIVED
JUL 10 2013
DIV. OF OIL, GAS & MINING



EAGER BEAVER TESTERS

DATE: 7-3-13 COMPANY: Newfield RIG: Pioneer 44 WELL NAME & #: Lejeune 1-17-3-2W (H)

ACCUMULATOR FUNCTION TESTS

TO CHECK THE USABLE FLUID STORED IN THE NITROGEN BOTTLES ON THE ACCUMULATOR

(O.S.O. #2 SECTION iii, A.3.C.1. OR II OR III)

1. Make sure all rams and annular are open and if applicable HCR is closed
2. Ensure accumulator is pumped up to working pressure! (shut off pumps)
3. Open HCR Valve (if applicable)
4. Close annular
5. Close all pipe rams
6. Open one set of the pipe rams to simulate closing the blind ram
7. If you have a 3 ram stack open the annular to achieve the 50%+ safety factor for 5M and greater systems
8. Accumulator pressure should be 200 psi over desired precharge pressure, (accumulator working pressure (1500 psi= 750 desired psi) (2000 and 3000 psi= 100 desired psi)
9. Record the remaining pressure 1550 PSI

TO CHECK THE CAPACITY OF THE ACCUMULATOR PUMPS

(O.S.O. #2 SECTION III.A.2.F.)

1. Shut the accumulator bottles or spherical, (isolate them from the pumps and manifold) Open the bleed off valve to the tank, (manifold psi should go to 0 psi) close bleed valve.
2. Open the HCR valve (if applicable)
3. Close annular
4. With pumps only, time how long it takes to regain manifold pressure to 200 psi over desired precharge pressure! (Accumulator working pressure {1500 psi=750 desired psi} {2000 and 3000 psi= 1000 desired psi})
5. Record elapsed time 51 SEC (2 minutes or less)

TO CHECK THE PRECHARGE ON BOTTLES OR SPHERICAL

(O.S.O. #2 SECTION III.A.2.D.)

. Open bottles back up to the manifold (pressure should be above the desired precharge pressure, (1500 psi=750 desired psi) (2000 and 3000 psi= 1000 desired psi) may need to use pumps to pressure back up.

. With power to pumps shut off open bleed line to the tank

. Watch and record where the pressure drops (accumulator psi)

. Record the pressure drop 1550 PSI

EAGER BEAVER TESTERS

DATE: 7-3-13 COMPANY: _____ RIG: Pioneer 44 WELL NAME & #: Legume 1-17-3-2WH

Time	Test No.		Result
11:10 AM ☐PM☒	1	inside manifold valves	Pass ☒Fail ☐
11:32 AM ☐PM☒	2	outside manifold valves	Pass ☒Fail ☐
11:55 AM ☐PM☒	3	Superchoke	Pass ☒Fail ☐
12:02 AM ☒PM☐	4	Downstream manifold valves	Pass ☒Fail ☐
1:49 AM ☒PM☐	5	Standpipe, Annular	Pass ☒Fail ☐
2:11 AM ☒PM☐	6	Hydraulic IBOP	Pass ☒Fail ☐
4:17 AM ☒PM☐	7	Manual IBOP, lower pipe rams, inside kill & choke valves	Pass ☒Fail ☐
4:45 AM ☒PM☐	8	upper pipe rams, outside kill valve, HCR, TIW	Pass ☒Fail ☐
5:07 AM ☒PM☐	9	Riser valve, Dart valve	Pass ☒Fail ☐
5:38 AM ☒PM☐	10	Blind Rams, check valve,	Pass ☐Fail ☐
6:49 AM ☒PM☐	11	Casing	Pass ☐Fail ☐
5:10 AM ☒PM☐	12	(Standpipe @ 4700 psi)	Pass ☐Fail ☐
AM ☐PM☐	13		Pass ☐Fail ☐
AM ☐PM☐	14		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐

Acc. Tank Size (inches) (_____W_____D_____L) ÷ 231=_____gal.

Rock Springs, WY (307) 382-3350

BOP TESTING, CASING TESTING, LEAK OFF TESTING, &

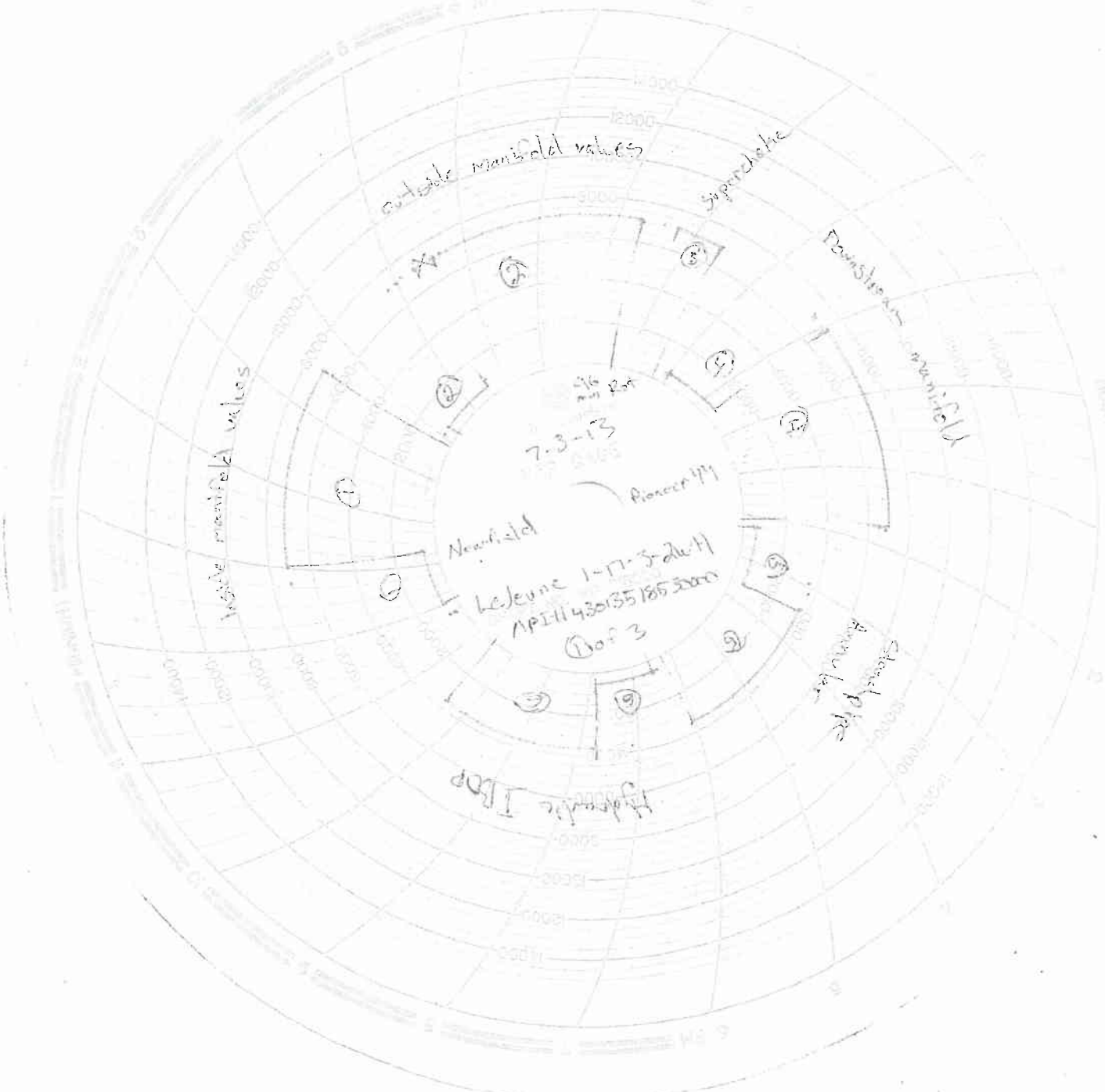
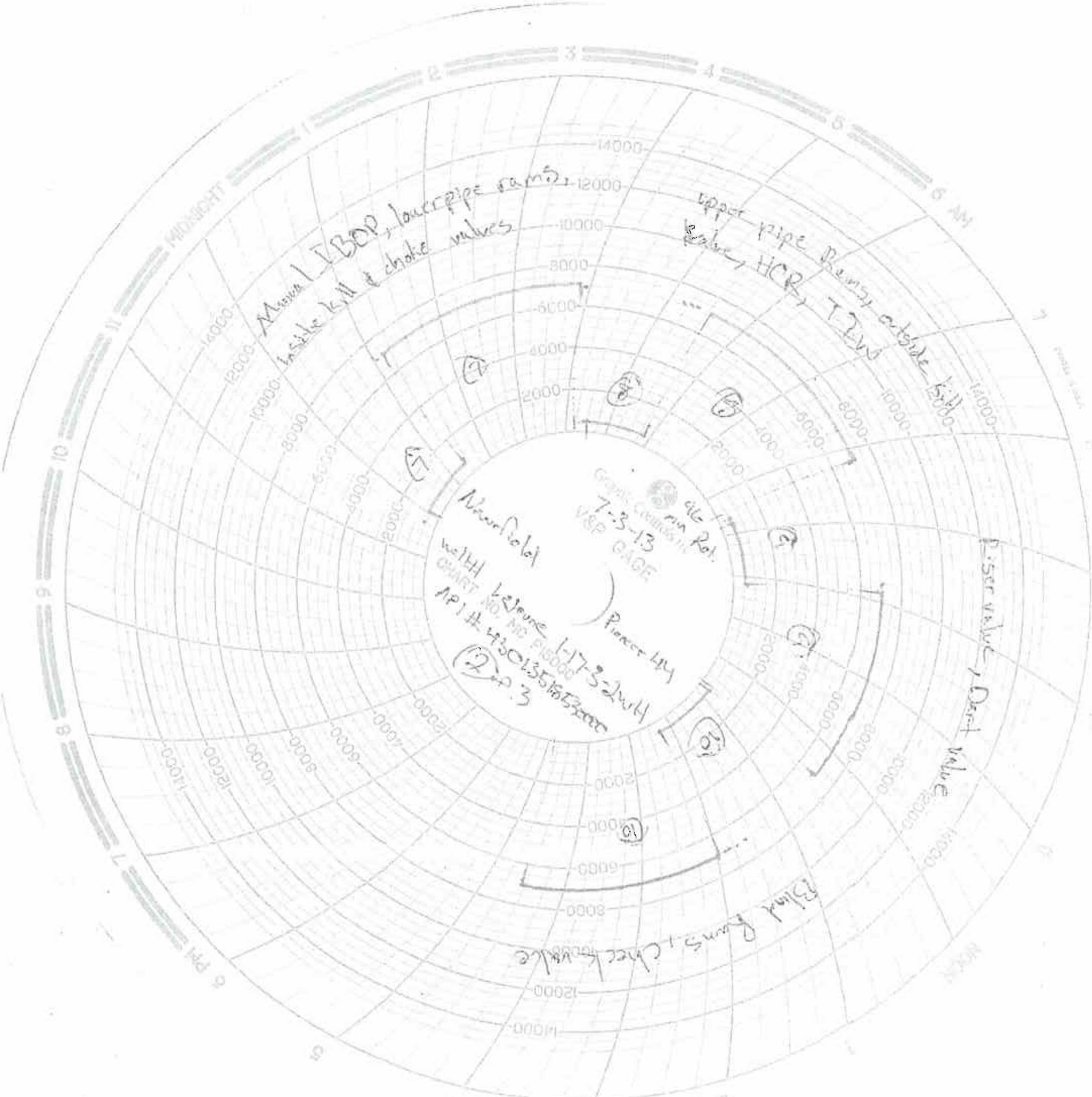
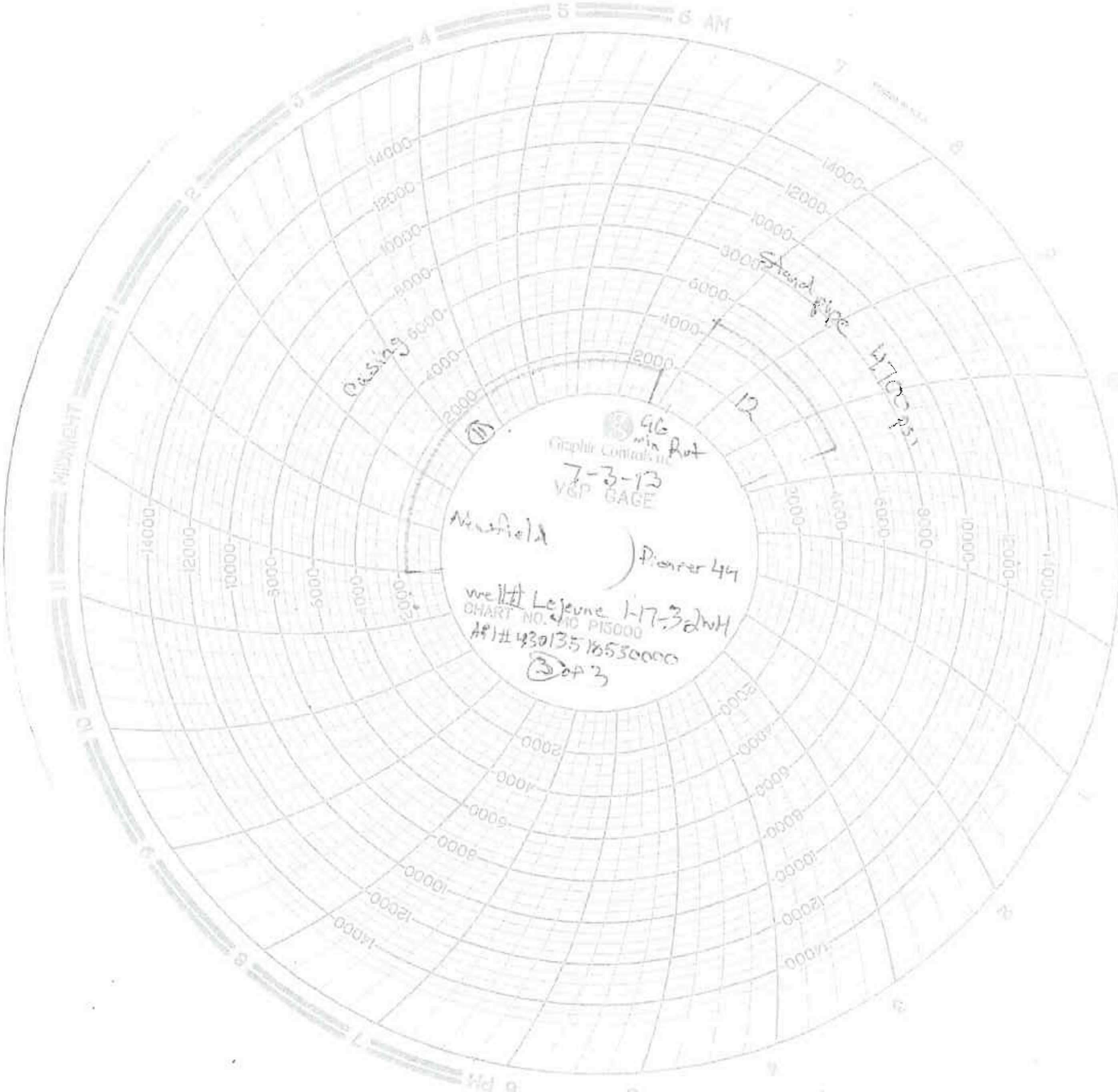


Chart #2 on Reverse


MIDNIGHT
6 AM
NOON
6 PM
V&P GAGE
Manual IBOP, lower pipe rams, inside kill & choke valves
upper pipe Rams, outside kill valve, HCR, TIW
Riser valve, Dart valve
Blind Rams, check valve
7-3-13
Newfield
Pioneer 44


Graphic Controls
VGP GAGE
CHART NO. MC P15000
7-3-13
46 min Rot
Newfield
Pioneer 44
well # Lejeune 1-17-3-2WH
API # 43013518550000
3 of 3
Casing
Stand Pipe
4700 PSI
11
12
MIDNIGHT
NOON
6 AM
6 PM

RECEIVED
JUL 10 2013
DIV. OF OIL, GAS & MINING

EAGER BEAVER TESTERS INC.

P.O. BOX 1616
ROCK SPRINGS, WY 82902

PHONE:
CASPER - (307) 265-8147
ROCK SPRINGS - (307) 382-3350

BOP TEST REPORT

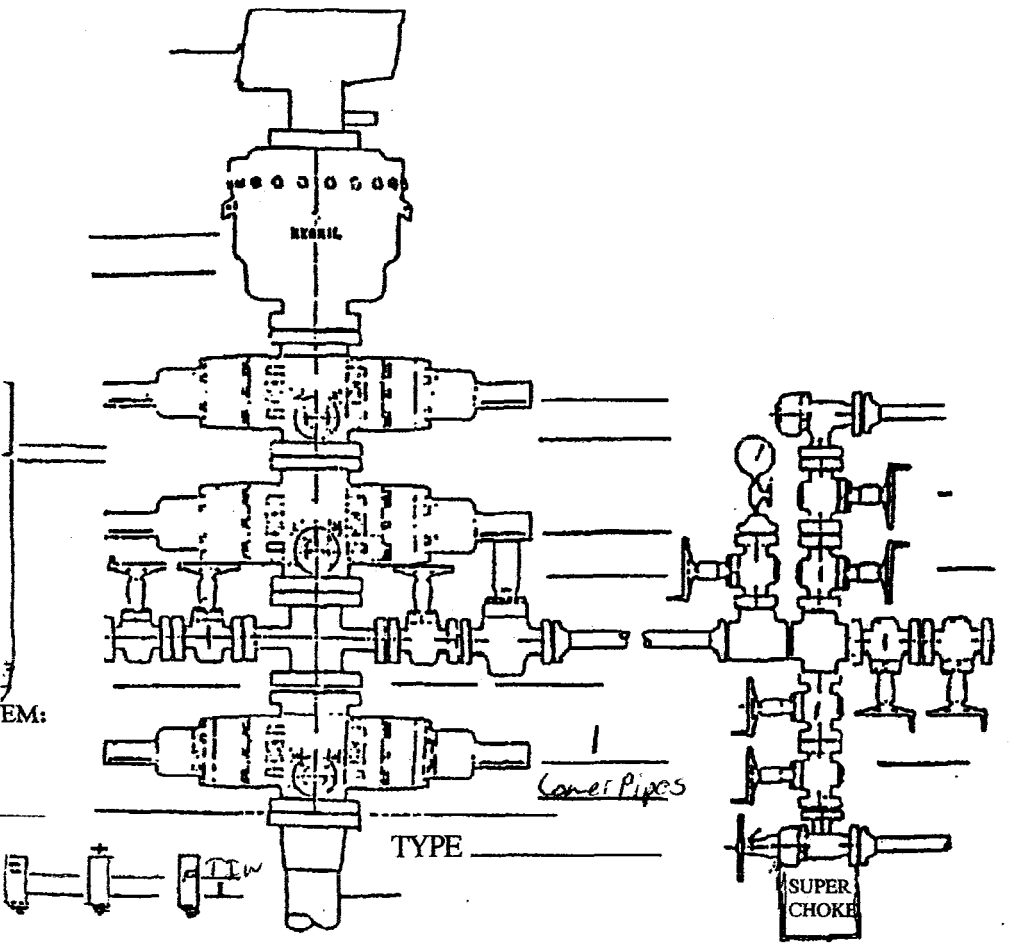
DATE: 7/5/13 OPERATOR: New field RIG OR SITE#: Pioneer 44 SEC: 17 TNSHIP: 3S RANGE: ~~3W~~ 2W

FIELD: Central basin WELL#: Lejeune 1-17-3-2WH TEST PRESSURE: 256/7000

43-013 51053 0000

EQUIPMENT PRESSURE TESTED:

ANNULAR 50%	____
UPPER PIPE RAMS	____
LOWER PIPE RAMS	1
BLIND RAMS	____
KILL LINE VALVES	1
HCR VALVE	____
CHOKE VALVES	____
MANIFOLD VALVES	1
SUPER CHOKE	____
MANUAL CHOKE	____
UPPER KELLY VALVE	____
LOWER KELLY VALVE	____
INSIDE BOP	____
FLOOR VALVE	1
CASING PRE.____	____



ACCUMULATOR AND CLOSING SYSTEM:

NITROGEN PRECHARGE PSI____
FIELD CHECK____GUAGE CHECK____
BOTTLES____SPHERES____

FUNCTION CHECK____
PUMP CHECK____
REMOTE OPERATION CHECK____
HYDRAULIC FLUID LEVEL____

TYPE ____

OTHER TESTS:

EQUIPMENT TYPE____PRESSURE____

REPAIRS OR POTENTIAL PROBLEMS:

RECEIVED
JUL 1 0 2013
DIV. OF OIL, GAS & MINING

EAGER BEAVER TESTERS

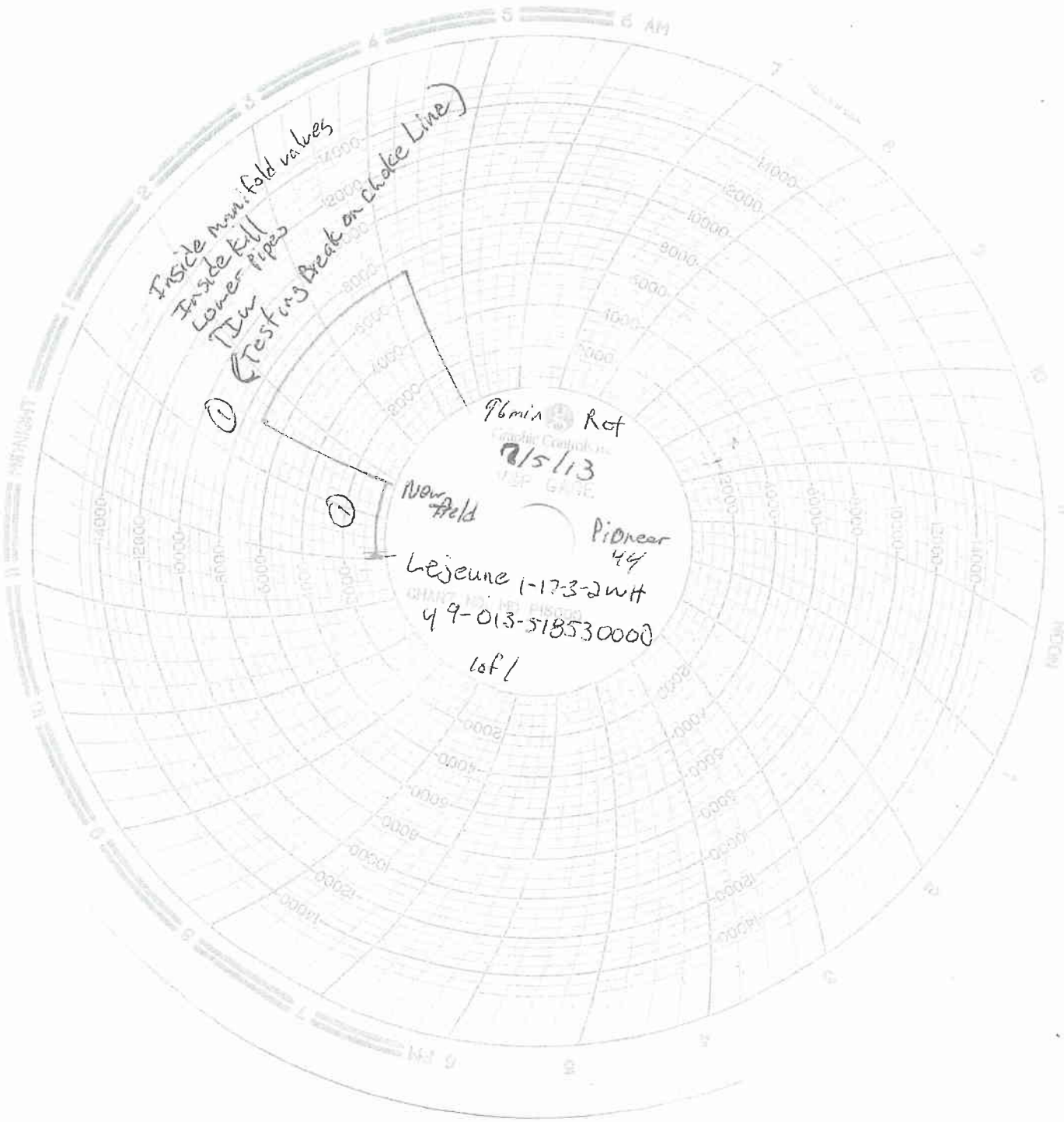
DATE: 7/5/13 COMPANY: New Field RIG: Pioneer 44 WELL NAME & #: Lejeune 1-17-3-2 wH

Time	Test No.	Results
5:35 AM □PM☒	1	Inside manifold valves, Inside kill, Lower pipes, TIW Pass ☒Fail □
AM □PM□	2	Pass □Fail □
AM □PM□	3	Pass □Fail □
AM □PM□	4	Pass □Fail □
AM □PM□	5	Pass □Fail □
AM □PM□	6	Pass □Fail □
AM □PM□	7	Pass □Fail □
AM □PM□	8	Pass □Fail □
AM □PM□	9	Pass □Fail □
AM □PM□	10	Pass □Fail □
AM □PM□	11	Pass □Fail □
AM □PM□	12	Pass □Fail □
AM □PM□	13	Pass □Fail □
AM □PM□	14	Pass □Fail □
AM □PM□	Retest	Pass □Fail □
AM □PM□	Retest	Pass □Fail □
AM □PM□	Retest	Pass □Fail □
AM □PM□	Retest	Pass □Fail □
AM □PM□	Retest	Pass □Fail □
AM □PM□	Retest	Pass □Fail □
AM □PM□	Retest	Pass □Fail □

Acc. Tank Size (inches) (_____ W _____ D _____ L) ÷ 231= _____ gal.

Rock Springs, WY (307) 382-3350

BOP TESTING, CASING TESTING, LEAK OFF TESTING, & INTEGRITY TESTING
NIPPLE UP CREWS, NITROGEN CHARGING SERVICE


Inside manifold valves
Inside Kill
Lower Pipes
TIW
(Testing Break on Choke Line)
1
96 min Rot
7/5/13
1
New Field
Pioneer
44
Lejeune 1-17-3-2WH
49-013-51853 0000
1 of 1

CONFIDENTIAL

BLM - Vernal Field Office - Notification Form

Operator Newfield Exploration Rig Name/# Pioneer 44 Submitted By Alvin Nielsen/ Dustin Edwards Phone Number 713-948-9196
Well Name/Number Lejeune 1-17-3-2WH
Qtr/Qtr NE/NE Section 17 Township 73S Range 2W
Lease Serial Number FEE
API Number 43013518530000

Spud Notice – Spud is the initial spudding of the well, not drilling out below a casing string.

Date/Time _____ _____ AM ☐ PM ☐

Casing – Please report time casing run starts, not cementing times.

- ☐ Surface Casing
- ☐ Intermediate Casing
- ☒ Production Casing
- ☐ Liner
- ☐ Other

Date/Time 8/4/2013 09:00 AM ☒ PM ☐

BOPE

- ☐ Initial BOPE test at surface casing point
- ☐ BOPE test at intermediate casing point
- ☐ 30 day BOPE test
- ☐ Other

RECEIVED
AUG 02 2013
DIV. OF OIL, GAS & MINING

Date/Time _____ _____ AM ☐ PM ☐

Remarks _____

API Well Number: 43013518530000

PBTVD 0611'

Form 3160-4
(March 2012)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB NO. 1004-0137
Expires: October 31, 2014

WELL COMPLETION OR RECOMPLETION REPORT AND LOG

5. Lease Serial No.: PATENTED

1a. Type of Well: ☑ Oil Well ☐ Gas Well ☐ Dry ☐ Other
b. Type of Completion: ☑ New Well ☐ Work Over ☐ Deepen ☐ Plug Back ☐ Diff. Resvr.,
Other: _____

6. If Indian, Allottee or Tribe Name:

7. Unit or CA Agreement Name and No.:

2. Name of Operator: NEWFIELD PRODUCTION COMPANY

8. Lease Name and Well No.: LEJUNE 1-17-3-2WH

3. Address: ROUTE #3 BOX 3630, MYTON, UT 84052

3a. Phone No. *(include area code)*: Ph:435-646-3721

9. API Well No.: 43-013-51853

4. Location of Well *(Report location clearly and in accordance with Federal requirements)**

At surface: 227' FNL 1115' FEL (NE/NE) SEC 17, T3S, R2W

At top prod. interval reported below: 800' FNL 679' FEL (NE/NE) SEC 17, T3S, R2W

At total depth: 609' FSL 662' FEL (SE/SE) SEC 17, T3S, R2W

10. Field and Pool or Exploratory: WILDCAT

11. Sec., T., R., M., on Block and Survey or Area: SEC 17, T3S, R2W

12. County or Parish: DUCHESNE

13. State: UT

14. Date Spudded: 02/14/2013

15. Date T.D. Reached: 08/07/2013

16. Date Completed: ☐ D & A ☑ Ready to Prod. 09/02/2013

17. Elevations (DF, RKB, RT, GL)*: 5214' GL 5241'KB

18. Total Depth: MD 13301' TVD 8608'

19. Plug Back T.D.: MD 13,238 TVD

20. Depth Bridge Plug Set: MD TVD

21. Type Electric & Other Mechanical Logs Run (Submit copy of each)
DUAL IND GRD, SP, COMP. NEUTRON, GR, CALIPER, CMT BOND

22. Was well cored? ☑ No ☐ Yes (Submit analysis)
Was DST run? ☑ No ☐ Yes (Submit report)
Directional Survey? ☐ No ☑ Yes (Submit copy)

23. Casing and Liner Record *(Report all strings set in well)*

Hole Size	Size/Grade	Wt. (#/ft.)	Top (MD)	Bottom (MD)	Stage Cementer Depth	No. of Sks. & Type of Cement	Slurry Vol. (BBL)	Cement Top*	Amount Pulled
17-1/2"	13-3/8" J-55	68#	0'	1027'		1280 CLASS G			
12-1/4"	9-5/8" N-80	40#	26'	8379'		660 bondcem			
						1500versacem			
						140 varicem			
8-3/4"	5-1/2" P-110	20#	26'	13297'		400 elastiseal		7671'	
						420 bondcem			

24. Tubing Record

Size	Depth Set (MD)	Packer Depth (MD)	Size	Depth Set (MD)	Packer Depth (MD)	Size	Depth Set (MD)	Packer Depth (MD)
2-7/8"	EOT@8750'	XN@8743'						

25. Producing Intervals / 26. Perforation Record

Formation	Top	Bottom	Perforated Interval	Size	No. Holes	Perf. Status
A) WASATCH	9400'	13159'	9400'-13159' MD	0.49	457	
B)						
C)						
D)						

27. Acid, Fracture, Treatment, Cement Squeeze, etc.

Depth Interval	Amount and Type of Material
9400'-13159' MD	Frac w/ 10520# of 100 mesh 2117435#s of 30/50 sand in 36923 bbls of Lightning 17 fluid, in 20 stages.

28. Production - Interval A

Date First Produced	Test Date	Hours Tested	Test Production	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
8/22/13	9/2/13	24	→	265	0	125			GAS LIFT

Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status
			→					PRODUCING

28a. Production - Interval B

Date First Produced	Test Date	Hours Tested	Test Production	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
			→						

Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status
			→					

*(See instructions and spaces for additional data on page 2)

RECEIVED: Oct. 10, 2013

28b. Production - Interval C

Date First Produced	Test Date	Hours Tested	Test Production →	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method

Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate →	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status

28c. Production - Interval D

Date First Produced	Test Date	Hours Tested	Test Production →	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method

Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate →	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status

29. Disposition of Gas *(Solid, used for fuel, vented, etc.)*

30. Summary of Porous Zones (Include Aquifers):

Show all important zones of porosity and contents thereof: Cored intervals and all drill-stem tests, including depth interval tested, cushion used, time tool open, flowing and shut-in pressures and recoveries.

31. Formation (Log) Markers
GEOLOGICAL MARKERS

Formation	Top	Bottom	Descriptions, Contents, etc.	Name	Top Meas. Depth
				GREEN RIVER FORMATION	3514'
				GARDEN GULCH	6415'
				DOUGLAS CREEK	7524'
				B LIMESTONE	8088'
				CASTLE PEAK	8415'
				UTELAND BUTTE	8711'
				UTELAND BUTTE A	8726'
				UTELAND BUTTE B	8740'
				UTELAND BUTTE C	8768'
				UTELAND BUTTE D	8803'
				WASATCH	8846'

32. Additional remarks (include plugging procedure):

33. Indicate which items have been attached by placing a check in the appropriate boxes:

☐ Electrical/Mechanical Logs (1 full set req'd.) ☐ Geologic Report ☐ DST Report ☑ Directional Survey
☐ Sundry Notice for plugging and cement verification ☐ Core Analysis ☑ Other: Drilling daily activity

34. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records (see attached instructions)*

Name *(please print)* Heather Calder Title Regulatory Technician

Signature Heather Calder Date 10/10/2013

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 3)

RECEIVED: Oct. 10, 2013

API Well Number: 43013518530000

Operator: NEWFIELD EXPLORATION COMPANY
Directional: LEAM DRILLING SYSTEMS, INC
County/State: DUCHESNE, UTAH
Well Name: LeJeune 1-17-3-2WH
Drill Rig: PIONEER 44
Geologist: ADAM SCHROEDER / ACLAM KPEKPASSE

Dates: 06/15/2013 to 08/01/2013
SPUD Date: 6/15/2013
Depth Reference: GL: 5213' / KB: 5241'
Surface Location: 227' FNL, 1115' FEL
Sec. 17 - T3S - R2W

Calculation Method

Main Lateral		BHA #	16
		GTB =	42.44'
Proposed Azi, =	180.00°	PTB =	58.85'
Target Angle =	92.37°	NB Inc =	3.98'
Target TVD =	8,805'	NB GR =	2.75'

Tool Type	BR	BRN	Survey	Incl	Azi	CL (ft)	TVD (ft)	VS (ft)	Coordinates N/S (ft)		Coordinates E/W (ft)		Closure Dist (ft)	Closure Ang (°)	DLS (°/100')	Bld Rate (°/100')	Wlk Rate (°/100')	BRN
Tie-In			968	1.54	161.71		967.89	10.22	-10.22		-0.03							
MWD	0.4	0.7	1078	2.02	161.67	110	1077.84	13.46	-13.46	S	1.04	E	13.50	175.58	0.44	0.44	-0.04	0.7
MWD	0.0	0.7	1173	2.02	169.75	95	1172.78	16.70	-16.70	S	1.86	E	16.80	173.63	0.30	0.00	8.51	0.7
MWD	-0.2	0.7	1269	1.85	174.15	96	1268.72	19.91	-19.91	S	2.32	E	20.04	173.34	0.24	-0.18	4.58	0.7
MWD	0.0	0.7	1332	1.85	178.45	63	1331.69	21.94	-21.94	S	2.45	E	22.07	173.62	0.22	0.00	6.83	0.7
MWD	0.2	0.7	1427	2.02	173.71	95	1426.64	25.13	-25.13	S	2.68	E	25.27	173.92	0.25	0.18	-4.99	0.7
MWD	0.0	0.8	1522	2.02	172.74	95	1521.58	28.46	-28.46	S	3.07	E	28.62	173.83	0.04	0.00	-1.02	0.8
MWD	0.1	0.8	1618	2.11	183.29	96	1617.51	31.90	-31.90	S	3.19	E	32.06	174.30	0.41	0.09	10.99	0.8
MWD	-0.2	0.8	1713	1.93	181.00	95	1712.46	35.25	-35.25	S	3.06	E	35.38	175.04	0.21	-0.19	-2.41	0.8
MWD	0.4	0.8	1808	2.29	182.23	95	1807.39	38.74	-38.74	S	2.96	E	38.85	175.64	0.38	0.38	1.29	0.8
MWD	0.2	0.8	1903	2.46	175.91	95	1902.31	42.67	-42.67	S	3.03	E	42.78	175.94	0.33	0.18	-6.65	0.8
MWD	0.2	0.8	1998	2.64	176.17	95	1997.22	46.89	-46.89	S	3.32	E	47.01	175.95	0.19	0.19	0.27	0.8
MWD	0.1	0.8	2093	2.73	177.14	95	2092.11	51.33	-51.33	S	3.58	E	51.46	176.01	0.11	0.09	1.02	0.8
MWD	0.2	0.8	2188	2.90	174.67	95	2187.00	55.98	-55.98	S	3.91	E	56.12	176.00	0.22	0.18	-2.60	0.8
MWD	0.3	0.8	2284	3.17	174.32	96	2282.86	61.04	-61.04	S	4.40	E	61.20	175.87	0.28	0.28	-0.36	0.8
MWD	0.1	0.8	2379	3.25	181.53	95	2377.71	66.35	-66.35	S	4.59	E	66.51	176.04	0.43	0.08	7.59	0.8
MWD	0.5	0.8	2473	3.69	174.85	94	2471.54	72.02	-72.02	S	4.79	E	72.18	176.19	0.63	0.47	-7.11	0.8
MWD	0.2	0.9	2569	3.87	175.99	96	2567.33	78.33	-78.33	S	5.30	E	78.51	176.13	0.20	0.19	1.19	0.9
MWD	0.5	0.9	2662	4.31	178.89	93	2660.09	84.96	-84.96	S	5.58	E	85.14	176.24	0.52	0.47	3.12	0.9
MWD	-1.5	0.9	2757	2.90	170.98	95	2754.90	90.90	-90.90	S	6.03	E	91.10	176.21	1.57	-1.48	-8.33	0.9
MWD	-0.2	0.9	2853	2.73	149.54	96	2850.79	95.27	-95.27	S	7.57	E	95.57	175.46	1.10	-0.18	-22.33	0.9
MWD	-0.9	0.9	2948	1.85	122.38	95	2945.72	98.04	-98.04	S	10.01	E	98.55	174.17	1.45	-0.93	-28.59	0.9
MWD	0.6	1.0	3043	2.46	83.36	95	3040.65	98.63	-98.63	S	13.33	E	99.52	172.30	1.63	0.64	-41.07	1.0
MWD	2.1	0.9	3138	4.48	61.82	95	3135.48	96.64	-96.64	S	18.63	E	98.42	169.09	2.50	2.13	-22.67	0.9
MWD	1.1	0.9	3234	5.54	55.49	96	3231.11	92.24	-92.24	S	25.75	E	95.77	164.40	1.24	1.10	-6.59	0.9
MWD	0.0	0.9	3329	5.54	56.64	95	3325.67	87.12	-87.12	S	33.36	E	93.29	159.05	0.12	0.00	1.21	0.9
MWD	0.0	1.0	3424	5.54	57.25	95	3420.22	82.12	-82.12	S	41.05	E	91.81	153.44	0.06	0.00	0.64	1.0
MWD	0.1	1.0	3519	5.63	61.12	95	3514.77	77.39	-77.39	S	48.98	E	91.59	147.67	0.41	0.09	4.07	1.0
MWD	0.6	1.0	3613	6.16	54.35	94	3608.28	72.22	-72.22	S	57.12	E	92.08	141.66	0.93	0.56	-7.20	1.0
MWD	0.1	1.0	3709	6.24	49.08	96	3703.72	65.80	-65.80	S	65.25	E	92.67	135.24	0.60	0.08	-5.49	1.0
MWD	0.7	1.0	3805	6.95	44.51	96	3799.08	58.24	-58.24	S	73.26	E	93.59	128.49	0.92	0.74	-4.76	1.0
MWD	-0.2	1.0	3900	6.77	53.56	95	3893.40	50.82	-50.82	S	81.80	E	96.30	121.85	1.15	-0.19	9.53	1.0
MWD	-0.6	1.1	3995	6.24	53.30	95	3987.79	44.41	-44.41	S	90.44	E	100.75	116.15	0.56	-0.56	-0.27	1.1
MWD	-0.2	1.1	4089	6.07	52.68	94	4081.25	38.34	-38.34	S	98.49	E	105.69	111.27	0.19	-0.18	-0.66	1.1
MWD	-0.7	1.1	4184	5.45	54.97	95	4175.77	32.71	-32.71	S	106.18	E	111.10	107.12	0.70	-0.65	2.41	1.1
MWD	-0.9	1.2	4280	4.57	56.90	96	4271.40	28.00	-28.00	S	113.11	E	116.53	103.90	0.93	-0.92	2.01	1.2
MWD	0.2	1.2	4376	4.75	55.41	96	4367.09	23.66	-23.66	S	119.59	E	121.91	101.19	0.23	0.19	-1.55	1.2
MWD	-0.6	1.2	4472	4.13	57.52	96	4462.80	19.54	-19.54	S	125.78	E	127.29	98.83	0.67	-0.65	2.20	1.2
MWD	0.6	1.2	4568	4.75	46.71	96	4558.51	14.96	-14.96	S	131.59	E	132.44	96.49	1.08	0.65	-11.26	1.2
MWD	-0.8	1.3	4663	3.96	50.22	95	4653.24	10.16	-10.16	S	136.97	E	137.35	94.24	0.88	-0.83	3.69	1.3
MWD	0.6	1.3	4759	4.57	49.87	96	4748.97	5.58	-5.58	S	142.44	E	142.55	92.24	0.64	0.64	-0.36	1.3
MWD	1.1	1.3	4855	5.63	58.75	96	4844.59	0.67	-0.67	S	149.39	E	149.40	90.26	1.37	1.10	9.25	1.3
MWD	0.4	1.3	4951	5.98	68.50	96	4940.10	-3.61	3.61	N	158.07	E	158.11	88.69	1.09	0.36	10.16	1.3
MWD	-0.8	1.4	5047	5.19	74.57	96	5035.64	-6.59	6.59	N	166.91	E	167.04	87.74	1.03	-0.82	6.32	1.4
MWD	-0.3	1.4	5142	4.92	78.17	95	5130.27	-8.57	8.57	N	175.04	E	175.25	87.20	0.44	-0.28	3.79	1.4
MWD	1.4	1.4	5237	6.24	74.48	95	5224.82	-10.79	10.79	N	184.00	E	184.32	86.64	1.44	1.39	-3.88	1.4
MWD	0.3	1.5	5332	6.51	63.05	95	5319.24	-14.61	14.61	N	193.78	E	194.33	85.69	1.36	0.28	-12.03	1.5
MWD	0.3	1.5	5428	6.77	59.27	96	5414.59	-19.97	19.97	N	203.49	E	204.47	84.40	0.53	0.27	-3.94	1.5
MWD	-0.9	1.6	5523	5.89	52.33	95	5509.02	-25.81	25.81	N	212.17	E	213.73	83.06	1.23	-0.93	-7.31	1.6
MWD	-1.1	1.6	5618	4.84	55.14	95	5603.60	-31.08	31.08	N	219.31	E	221.50	81.93	1.14	-1.11	2.96	1.6
MWD	-0.6	1.7	5714	4.31	55.23	96	5699.29	-35.45	35.45	N	225.60	E	228.37	81.07	0.55	-0.55	0.09	1.7
MWD	-0.7	1.8	5809	3.61	67.89	95	5794.07	-38.61	38.61	N	231.30	E	234.50	80.52	1.17	-0.74	13.33	1.8
MWD	0.2	1.8	5905	3.78	65.34	96	5889.87	-41.07	41.07	N	236.98	E	240.51	80.17	0.25	0.18	-2.66	1.8
MWD	0.2	1.9	6000	3.96	64.20	95	5984.65	-43.80	43.80	N	242.78	E	246.70	79.77	0.21	0.19	-1.20	1.9
MWD	0.2	1.9	6095	4.13	55.23	95	6079.41	-47.18	47.18	N	248.54	E	252.98	79.25	0.69	0.18	-9.44	1.9
MWD	-0.3	2.0	6191	3.87	60.42	96	6175.18	-50.75	50.75	N	254.20	E	259.22	78.71	0.46	-0.27	5.41	2.0
MWD	0.6	2.1	6287	4.48	58.66	96	6270.93	-54.30	54.30	N	260.22	E	265.82	78.21	0.65	0.64	-1.83	2.1
MWD	0.8	2.1	6383	5.28	58.66	96	6366.58	-58.55	58.55	N	267.19	E	273.53	77.64	0.83	0.83	0.00	2.1
MWD	-0.3	2.2	6478	5.01	59.27	95	6461.19	-62.94	62.94	N	274.49	E	281.62	77.08	0.29	-0.28	0.64	2.2
MWD	0.5	2.3	6574	5.45	55.67	96	6556.79	-67.66	67.66	N	281.86	E	289.87	76.50	0.57	0.46	-3.75	2.3
MWD	-0.3	2.4	6669	5.19	58.04	95	6651.39	-72.48	72.48	N	289.23	E	298.17	75.93	0.36	-0.27	2.49	2.4
MWD	0.3	2.5	6765	5.45	56.37	96	6746.97	-77.30	77.30	N	296.71	E	306.61	75.40	0.32	0.27	-1.74	2.5
MWD	-0.2	2.6	6861	5.28	60.68	96	6842.55	-81.99	81.99	N	304.36	E	315.21	74.92	0.46	-0.18	4.49	2.6
MWD	-0.3	2.8	6956	5.01	61.74	95	6937.17	-86.09	86.09	N	311.82	E	323.49	74.57	0.30	-0.28	1.12	2.8
MWD	-0.2	3.0	7052	4.84	65.25	96	7032.81	-89.77	89.77	N	319.19	E	331.58	74.29	0.36	-0.18	3.66	3.0
MWD	-0.2	3.1	7148	4.66	72.28	96	7128.49	-92.65	92.65	N	326.59	E	339.47	74.16	0.63	-0.19	7.32	3.1
MWD	0.0	3.3	7244	4.66	79.00	96	7224.17	-94.58	94.58	N	334.13	E	347.26	74.19	0.57	0.00	7.00	3.3

RECEIVED: Oct. 10, 2013

API Well Number: 43013518530000

Operator: NEWFIELD EXPLORATION COMPANY
Directional: LEAM DRILLING SYSTEMS, INC
County/State: DUCHESNE, UTAH
Well Name: LeJeune 1-17-3-2WH
Drill Rig: PIONEER 44
Geologist: ADAM SCHROEDER / ACLAM KPEKPASSE

Dates: 06/15/2013 to 08/01/2013
SPUD Date: 6/15/2013
Depth Reference: GL: 5213' / KB: 5241'
Surface Location: 227' FNL, 1115' FEL
Sec. 17 - T3S - R2W

Calculation Method

Main Lateral	
Proposed Azi. =	180.00°
Target Angle =	92.37°
Target TVD =	8,805'

BHA #	16
GTB =	42.44'
PTB =	58.85'
NB Inc =	3.98'
NB GR =	2.75'

Tool Type	BR	BRN	Survey	Incl	Azi	CL (ft)	TVD (ft)	VS (ft)	Coordinates N/S (ft)		E/W (ft)		Closure Dist (ft)	Ang (°)	DLS (°/100')	Bld Rate (°/100')	Wlk Rate (°/100')	BRN
MWD	-0.4	3.6	7339	4.31	84.32	95	7318.88	-95.67	95.67	N	341.47	E	354.62	74.35	0.57	-0.37	5.60	3.6
MWD	0.4	3.8	7435	4.66	86.70	96	7414.58	-96.26	96.26	N	348.95	E	361.98	74.58	0.41	0.36	2.48	3.8
MWD	0.7	4.0	7530	5.36	88.19	95	7509.22	-96.62	96.62	N	357.24	E	370.07	74.87	0.75	0.74	1.57	4.0
MWD	-0.1	4.3	7626	5.28	87.66	96	7604.81	-96.94	96.94	N	366.13	E	378.75	75.17	0.10	-0.08	-0.55	4.3
MWD	-0.3	4.7	7722	5.01	83.53	96	7700.42	-97.59	97.59	N	374.71	E	387.21	75.40	0.48	-0.28	-4.30	4.7
MWD	0.3	5.1	7817	5.28	87.22	95	7795.04	-98.27	98.27	N	383.20	E	395.60	75.62	0.45	0.28	3.88	5.1
MWD	0.6	5.6	7912	5.89	86.61	95	7889.59	-98.77	98.77	N	392.43	E	404.67	75.87	0.65	0.64	-0.64	5.6
MWD	0.2	6.2	8008	6.07	83.36	96	7985.06	-99.65	99.65	N	402.39	E	414.55	76.09	0.40	0.19	-3.39	6.2
MWD	0.7	7.0	8103	6.77	68.24	95	8079.48	-102.31	102.31	N	412.58	E	425.08	76.07	1.92	0.74	-15.92	7.0
MWD	-0.6	8.1	8199	6.16	62.35	96	8174.87	-106.80	106.80	N	422.40	E	435.69	75.81	0.94	-0.64	-6.14	8.1
MWD	-0.4	9.6	8293	5.80	63.93	94	8268.35	-111.22	111.22	N	431.13	E	445.25	75.53	0.42	-0.38	1.68	9.6
MWD	-0.8	10.2	8325	5.54	65.51	32	8300.20	-112.57	112.57	N	433.99	E	448.35	75.46	0.95	-0.81	4.94	10.2
MWD	9.3	10.5	8421	14.42	80.95	96	8394.66	-116.38	116.38	N	450.05	E	464.85	75.50	9.58	9.25	16.08	10.5
MWD	13.8	10.2	8453	18.82	82.36	32	8425.32	-117.70	117.70	N	459.10	E	473.95	75.62	13.81	13.75	4.41	10.2
MWD	11.0	10.1	8485	22.34	85.28	32	8455.27	-118.88	118.88	N	470.28	E	485.08	75.81	11.45	11.00	9.13	10.1
MWD	9.1	10.2	8517	25.24	94.61	32	8484.56	-118.84	118.84	N	483.15	E	497.55	76.18	14.82	9.06	29.16	10.2
MWD	5.9	10.7	8548	27.08	104.33	31	8512.40	-116.56	116.56	N	496.58	E	510.08	76.79	15.02	5.94	31.35	10.7
MWD	0.3	11.8	8580	27.17	115.64	32	8540.90	-111.59	111.59	N	510.24	E	522.30	77.66	16.10	0.28	35.34	11.8
MWD	1.9	13.0	8612	27.79	131.06	32	8569.32	-103.52	103.52	N	522.46	E	532.62	78.79	22.27	1.94	48.19	13.0
MWD	2.5	14.4	8644	28.58	144.48	32	8597.56	-92.38	92.38	N	532.55	E	540.50	80.16	19.92	2.47	41.94	14.4
MWD	6.0	15.7	8676	30.51	154.44	32	8625.41	-78.81	78.81	N	540.50	E	546.22	81.70	16.47	6.03	31.13	15.7
MWD	14.6	15.9	8708	35.17	163.80	32	8652.31	-62.61	62.61	N	546.59	E	550.16	83.47	21.50	14.56	29.25	15.9
MWD	17.3	15.6	8740	40.71	167.71	32	8677.54	-43.55	43.55	N	551.38	E	553.10	85.48	18.86	17.31	12.22	15.6
MWD	17.1	15.3	8772	46.17	171.02	32	8700.77	-21.93	21.93	N	555.41	E	555.84	87.74	18.48	17.06	10.34	15.3
MWD	16.2	15.0	8804	51.35	174.58	32	8721.86	1.93	-1.93	S	558.39	E	558.40	90.20	18.22	16.19	11.13	15.0
MWD	17.1	14.4	8836	56.81	178.07	32	8740.63	27.78	-27.78	S	560.03	E	560.72	92.84	19.21	17.06	10.91	14.4
MWD	15.9	14.0	8867	61.73	180.93	31	8756.47	54.41	-54.41	S	560.24	E	562.88	95.55	17.74	15.87	9.23	14.0
MWD	22.0	10.9	8899	68.76	183.71	32	8769.86	83.42	-83.42	S	559.05	E	565.24	98.49	23.34	21.97	8.69	10.9
MWD	16.5	8.6	8932	74.22	186.99	33	8780.34	114.56	-114.56	S	556.12	E	567.79	101.64	19.04	16.55	9.94	8.6
MWD	15.0	5.9	8963	78.88	190.54	31	8787.55	144.34	-144.34	S	551.52	E	570.09	104.67	18.71	15.03	11.45	5.9
MWD	4.3	6.7	8994	80.20	191.91	31	8793.18	174.24	-174.24	S	545.58	E	572.73	107.71	6.08	4.26	4.42	6.7
MWD	5.8	7.3	9027	82.13	193.78	33	8798.24	206.03	-206.03	S	538.33	E	576.41	110.94	8.10	5.85	5.67	7.3
MWD	11.3	3.2	9059	85.74	195.40	32	8801.62	236.82	-236.82	S	530.32	E	580.79	114.06	12.35	11.28	5.06	3.2
MWD	13.4	-2.2	9091	90.04	196.10	32	8802.80	267.59	-267.59	S	521.64	E	586.27	117.16	13.61	13.44	2.19	-2.2
MWD	0.0	-2.2	9155	90.04	195.91	64	8802.76	329.11	-329.11	S	503.99	E	601.93	123.14	0.30	0.00	-0.30	-2.2
MWD	0.7	-1.9	9218	90.48	195.77	63	8802.47	389.72	-389.72	S	486.80	E	623.58	128.68	0.73	0.70	-0.22	-1.9
MWD	6.0	0.0	9249	92.33	196.37	31	8801.71	419.50	-419.50	S	478.22	E	636.14	131.26	6.27	5.97	1.94	0.0
MWD	3.7	2.0	9313	94.70	196.22	64	8797.79	480.81	-480.81	S	460.30	E	665.62	136.25	3.71	3.70	-0.23	2.0
MWD	6.6	3.4	9345	96.81	196.06	32	8794.58	511.39	-511.39	S	451.45	E	682.14	138.56	6.61	6.59	-0.50	3.4
MWD	0.4	2.1	9409	97.08	191.54	64	8786.84	573.07	-573.07	S	436.29	E	720.25	142.72	7.02	0.42	-7.06	2.1
MWD	0.0	1.8	9441	97.08	189.01	32	8782.89	604.31	-604.31	S	430.63	E	742.05	144.53	7.85	0.00	-7.91	1.8
MWD	-2.8	0.6	9507	95.23	185.35	66	8775.81	669.40	-669.40	S	422.43	E	791.55	147.75	6.18	-2.80	-5.55	0.6
MWD	-4.7	-0.1	9601	90.84	183.63	94	8770.84	762.96	-762.96	S	415.09	E	868.56	151.45	5.01	-4.67	-1.83	-0.1
MWD	-0.9	-0.1	9696	89.96	183.28	95	8770.17	857.78	-857.78	S	409.37	E	950.46	154.49	1.00	-0.93	-0.37	-0.1
MWD	0.9	-0.1	9792	90.84	182.97	96	8769.50	953.63	-953.63	S	404.13	E	1035.73	157.03	0.97	0.92	-0.32	-0.1
MWD	2.4	0.1	9888	93.12	181.26	96	8766.19	1049.50	-1049.50	S	400.59	E	1123.36	159.11	2.97	2.38	-1.78	0.1
MWD	-0.7	0.0	9983	92.42	180.00	95	8761.60	1144.38	-1144.38	S	399.55	E	1212.13	160.75	1.52	-0.74	-1.33	0.0
MWD	-1.6	-0.1	10079	90.84	181.36	96	8758.87	1240.33	-1240.33	S	398.41	E	1302.75	162.19	2.17	-1.65	1.42	-0.1
MWD	0.7	-0.1	10175	91.54	180.25	96	8756.87	1336.30	-1336.30	S	397.06	E	1394.04	163.45	1.37	0.73	-1.16	-0.1
MWD	-1.0	-0.1	10270	90.57	179.56	95	8755.12	1431.28	-1431.28	S	397.22	E	1485.38	164.49	1.25	-1.02	-0.73	-0.1
MWD	0.6	-0.1	10366	91.19	178.46	96	8753.65	1527.25	-1527.25	S	398.88	E	1578.48	165.36	1.32	0.65	-1.15	-0.1
MWD	1.1	0.0	10462	92.24	178.63	96	8750.77	1623.18	-1623.18	S	401.31	E	1672.05	166.11	1.11	1.09	0.18	0.0
MWD	0.8	0.1	10558	93.03	178.16	96	8746.36	1719.04	-1719.04	S	404.00	E	1765.87	166.77	0.96	0.82	-0.49	0.1
MWD	1.0	0.1	10653	94.00	176.86	95	8740.54	1813.77	-1813.77	S	408.12	E	1859.12	167.32	1.71	1.02	-1.37	0.1
MWD	-1.3	0.0	10749	92.77	175.63	96	8734.87	1909.39	-1909.39	S	414.39	E	1953.84	167.76	1.81	-1.28	-1.28	0.0
MWD	-0.1	0.0	10845	92.68	175.71	96	8730.30	2005.01	-2005.01	S	421.63	E	2048.86	168.12	0.13	-0.09	0.08	0.0
MWD	-1.4	0.0	10941	91.36	175.10	96	8726.92	2100.64	-2100.64	S	429.32	E	2144.06	168.45	1.51	-1.38	-0.64	0.0
MWD	1.5	0.0	11033	92.77	174.65	92	8723.61	2192.21	-2192.21	S	437.53	E	2235.44	168.71	1.61	1.53	-0.49	0.0
MWD	2.2	0.1	11098	94.18	175.88	65	8719.67	2256.86	-2256.86	S	442.89	E	2299.91	168.90	2.88	2.17	1.89	0.1
MWD	0.3	0.1	11194	94.44	175.28	96	8712.45	2352.31	-2352.31	S	450.27	E	2395.01	169.16	0.68	0.27	-0.62	0.1
MWD	0.7	0.2	11289	95.06	175.84	95	8704.58	2446.70	-2446.70	S	457.59	E	2489.12	169.41	0.88	0.65	0.59	0.2
MWD	-0.1	0.2	11385	94.97	176.09	96	8696.19	2542.09	-2542.09	S	464.32	E	2584.15	169.65	0.28	-0.09	0.26	0.2
MWD	-0.6	0.1	11481	94.35	176.21	96	8688.39	2637.56	-2637.56	S	470.75	E	2679.24	169.88	0.66	-0.65	0.13	0.1
MWD	-2.1	0.0	11577	92.33	176.25	96	8682.80	2733.18	-2733.18	S	477.05	E	2774.50	170.10	2.10	-2.10	0.04	0.0
MWD	-0.7	0.0	11673	91.63	177.01	96	8679.48	2828.96	-2828.96	S	482.69	E	2869.84	170.32	1.08	-0.73	0.79	0.0
MWD	2.6	0.1	11768	94.09	177.71	95	8674.74	2923.73	-2923.73	S	487.06	E	2964.02	170.54	2.69	2.59	0.74	0.1
MWD	-0.2	0.1	11865	93.91	176.28	97	8667.98	3020.36	-3020.36	S	492.13	E	3060.19	170.75	1.48	-0.19	-1.47	0.1

RECEIVED: Oct. 10, 2013

API Well Number: 43013518530000

Operator: NEWFIELD EXPLORATION COMPANY
Directional: LEAM DRILLING SYSTEMS, INC
County/State: DUCHESNE, UTAH
Well Name: LeJeune 1-17-3-2WH
Drill Rig: PIONEER 44
Geologist: ADAM SCHROEDER / ACLAM KPEKPASSE

Dates: 06/15/2013 to 08/01/2013
SPUD Date: 6/15/2013
Depth Reference: GL: 5213' / KB: 5241'
Surface Location: 227' FNL, 1115' FEL
Sec. 17 - T3S - R2W

Calculation Method

Main Lateral	
Proposed Azi. =	180.00°
Target Angle =	92.37°
Target TVD =	8,805'

BHA #	16
GTB =	42.44'
PTB =	58.85'
NB Inc =	3.98'
NB GR =	2.75'

Tool Type	BR	BRN	Survey	Incl	Azi	CL (ft)	TVD (ft)	VS (ft)	Coordinates N/S (ft)		E/W (ft)		Closure Dist (ft)	Closure Ang (°)	DLS (°/100')	Bld Rate (°/100')	Wlk Rate (°/100')	BRN
MWD	-0.3	0.0	11960	93.65	176.45	95	8661.71	3114.96	-3114.96	S	498.14	E	3154.54	170.91	0.33	-0.27	0.18	0.0
MWD	-1.3	0.0	12056	92.42	175.51	96	8656.63	3210.59	-3210.59	S	504.86	E	3250.04	171.06	1.61	-1.28	-0.98	0.0
MWD	-0.1	0.0	12152	92.33	175.87	96	8652.65	3306.23	-3306.23	S	512.07	E	3345.65	171.20	0.39	-0.09	0.38	0.0
MWD	-1.3	0.0	12247	91.10	175.68	95	8649.81	3400.93	-3400.93	S	519.07	E	3440.31	171.32	1.31	-1.29	-0.20	0.0
MWD	2.1	0.0	12343	93.12	179.29	96	8646.27	3496.75	-3496.75	S	523.28	E	3535.69	171.49	4.31	2.10	3.76	0.0
MWD	-2.1	0.0	12438	91.10	180.29	95	8642.78	3591.68	-3591.68	S	523.63	E	3629.65	171.71	2.37	-2.13	1.05	0.0
MWD	1.6	0.0	12533	92.59	181.78	95	8639.72	3686.61	-3686.61	S	521.91	E	3723.37	171.94	2.22	1.57	1.57	0.0
MWD	0.2	0.0	12629	92.77	183.79	96	8635.23	3782.39	-3782.39	S	517.25	E	3817.59	172.21	2.10	0.19	2.09	0.0
MWD	-0.7	0.0	12724	92.07	183.01	95	8631.22	3877.14	-3877.14	S	511.62	E	3910.75	172.48	1.10	-0.74	-0.82	0.0
MWD	-0.2	0.0	12820	91.89	185.34	96	8627.90	3972.82	-3972.82	S	504.64	E	4004.74	172.76	2.43	-0.19	2.43	0.0
MWD	-0.1	0.0	12915	91.80	186.83	95	8624.84	4067.23	-4067.23	S	494.57	E	4097.19	173.07	1.57	-0.09	1.57	0.0
MWD	1.6	0.0	13010	93.30	186.31	95	8620.61	4161.51	-4161.51	S	483.72	E	4189.53	173.37	1.67	1.58	-0.55	0.0
MWD	-1.4	0.0	13106	91.98	185.38	96	8616.19	4256.91	-4256.91	S	473.95	E	4283.21	173.65	1.68	-1.37	-0.97	0.0
MWD	0.7	0.0	13200	92.68	186.47	94	8612.37	4350.32	-4350.32	S	464.26	E	4375.03	173.91	1.38	0.74	1.16	0.0
Proj	-0.7	0.0	13301	92.00	186.50	101	8608.25	4450.59	-4450.59	S	452.86	E	4473.57	174.19	0.67	-0.67	0.03	0.0

RECEIVED: Oct. 10, 2013

Daily Activity Report

Format For Sundry

LEJEUNE 1-17-3-2WH

6/1/2013 To 12/30/2013

8/13/2013 Day: 1 **Completion**

Rigless on 8/13/2013 - Prepped well for completions. Moved in all frac tanks. NU & test Frac Tree. Haul in water for pump down. Co man trailer, start RU flowback. - NU Frac Tree as per program. 10K 7-1/16? Lower HCV, 10K 7-1/16? Spool, 10K 7 1/16? Upper MCV, 10K 7-1/16? flowcross with dual, double 2-1/16? outlets, 10K 7-1/16? Crown MCV, 10K 7-1/16? Goats Head. Test Frac Tree as per Newfield guidelines. AOI representative Mark Thies on location to verify testing procedures. Rigged in Rock Water flow back iron from flowback tanks to the plug catcher. The sand trap and remainder of the iron will be rigged in tomorrow. Meanwhile 2 flowback tanks with diffusers and 3 flowback tanks without diffusers (5 total flowback frac tanks) were spotted along with 2 swab frac tanks, 20 fresh water frac tanks, Consultants office, light plants, and guard shack. Man lift and front end loader were hauled in. Swab tanks are being filled with 1,000 bbls fresh water, biocide and a clay stabilizer were added to both tanks for the injection and pump down tomorrow. We have started loading fresh water into Nabors frac tanks. Note: Goats Head is not pressure tested. We will pressure test it with Halliburton tomorrow. Also, Tubing hanger has been removed from well head. SDFN. - Drilling department turned well over to Completions today. Finished grading location today with blade. Washed out drilling mud from cellar. Cut down and filled rat hole in cellar with gravel. Installed a 2? line with ball a valve above ground level from both the 9 5/8? and the 7? casings. Held PJSM with Cameron pressure tester, B & G Crane operator, FMC Frac Tree crew, and Western Well Service Hot Shot Driver on ND Flange, installing a TWCV and NU Frac Tree. ND Night flange from tubing head. Verified that there was no pressure under tubing hanger. Remove BPV and install TWCV.
Daily Cost: $0
Cumulative Cost: $19,558

8/14/2013 Day: 2 **Completion**

Rigless on 8/14/2013 - Rig Up Halliburton pump open toe sleeve - rig up JW WL pump Tools to 13,100 feet - Start to log out of hole - ISIP's were, 5 min = 4,104 psi, 10 min = 4,041 psi, 15 min = 4,022 psi. Connect logging tools and lubricator to well head. Pressure tested lubricator to 9,600 psi, test good. Having trouble with grease unit. LD tools to work on grease unit. Re-connect to well head and pressure test to 9,500 psi. Test good. - 17:25 - RIH with WL tools to 7,500?. 19:00 - Correlate depth with casing tally. 200 ft/min LT 270 WH 3785 Psi ? Start to pump (8200 feet 3 to 10 BPM 8245 psi 87 ft/min LT 620 -14 .7 BPM)-(9200 feet 14.7 BPM 7404 psi 100 ft/min LT 880) - (10,000 feet 14.7 BPM 7531 psi 142 ft/min LT 806) - (13,000 feet 14.7 BPM 7856 psi 88 ft/min LT 800) 20:11 At depth 13,100 feet Total volume pumped 653 bbls - 20:30 ? Start to log out of Hole with JW WL tools current depth 13,100 feet at 60 ft/min. 00:00 ? Current depth 2,000 feet ? Coming out of hole 52 ft/min with WL Tools logging well . RNI water haulers filling Frac Water tanks 6,000 bbls remaining to have both locations full Willie O?Neill 505-860-3326 - Installed cap onto WL BOP and pressure tested WL BOP to 9,500 psi, test good. Pumped 407 bbls treated fresh water into well bore (102 bbls overflushed) at rates ranging from 1.8 bpm to 14 bpm. Max pressure kicked out pumps @ 8,420 psi while pumping at a rate of 1.8 bpm. Pressure dropped to 5,960 psi we then brought the rate back up to 4.7 bpm with a pressure of 6,800 to 7,000 psi. Increased rate up to 14 bpm and reduced back to 12 bpm once 8,200 psi was reached. PSI leveled out at 7,894 psi at 12 bpm. Shut down pumps and we are obtaining 5, 10, & 15 min shut in pressures. - No activity. - RU Halliburton and JW wireline. PJSM. Pressure test goats head and Halliburton iron to 500 psi for5 min and 10,000 psi for 10 min. Test good. Opened well and pumped 7 bbls into well @3bpm, pressured up to 8,440 psi. kicked out pumps and toe shifted open after pumps were kicked out. Pressure dropped to 4,400 psi. Walked back into it at 3 bpm then up to 8bpm pressure spiked @ 5,204 psi and leveled out to 5,084 psi. Pumped 24 bbls into it at 8bpm (total fluid pumped was 49 bbls). Shut down and shut in well. - ND 10K-7 1/16" flange from goats head and NU WL flange. RU wireline BOPE and Lubricator. MU logging tools which include Radial CBL with Gamma and CCL. OD's and lengths recorded before picking up tools. WL BHA = Cable head 7/16 Cable Head OD?1.44 X 1.0-Probe OD?2.75 X 2.88 ? RBT OD?2.75X8.92 ? Probe OD?2.75 X 2.88 ?GR

RECEIVED: Oct. 10, 2013

probe OD? 2.75 X 6.42 ? Weight Bar OD? 2.75 X 3.0 ? Quick Change OD ` 3.13 x 1.50 ? Baker #20 OD?3.38 X 6.0 ? Halliburton dummy plug OD?4.4 X 2.0 ? Total weight = 267 lbs. - PJSM. We spent 30 min trying to get WL tools to go through lubricator. RIH with WL to 1,895? and WL stopped. Picked up and pulled up to 740# to pull through sticky spot and back to line weight of 480#. Attempted to work through 3 times, no good. POOH. To check tools. Tools came out of hole covered with a substance that appeared to be oil based mud filled with grainy solids. At depth where tools stopped was a volume of 42 bbls (We pumped 49 bbls into well bore to open sleeve and establish injection rate). Decision made to flush well bore with 305 bbls fresh water treated with biocide and clay stabilizer (hole volume plus 10 bbls).
Daily Cost: $0
Cumulative Cost: $96,063

8/15/2013 Day: 3 **Completion**

Rigless on 8/15/2013 - Continue to log well to surface - Rig up halliburton frac crew spot and Filling Mountain movers - Filling water tanks and test flow back equipment- RU Water transfer line. Pressure test frac lines and bucket tested. - 00:00 ? Current depth 2,000 feet ? Coming out of hole 52 ft/min with WL Tools logging well - Out Of Hole with all WL tools. - Out Of Hole with all WL tools. Close in Lower Master Valve bleed down pressure off well and Close in top Master valve, Well is Secured with 2 barriers ,Bleed down WL Lubricator Break off Lubricator and rig WL off well head install Night Cap ? Laydown Lubricator and rig down Wire line crane , Water haulers Continue to fill frac tanks with water for the frac . - Continue hauling 30/50 white sand and continue filling tanks with fresh water. - PJSM. Onsite training on pressure testing flowback equipment. We are stopping to repair leaks as needed (6 so far). We have released several of the vendors after the 5th test. Plan forward: Continue with testing and rigging up Halliburton frac. We still lack 5000+/- bbls of water. Water hauling has stopped on location until Rock Water has their water line rigged up and tested, this was done to make room for Halliburton. Note: Rock Water did not have enough replacement valves on location to replace leaky one?s. We will not be delayed due to this because we still have several tests to go. Finished testing @ 1830 hrs. Total time to test flowback for the training was 9.5 hrs. Released Cameron Pressure Tester and Rock Water Flowback crew. Meanwhile we moved in mountain movers, blender, hydration unit, 3 more pump trucks for a total of 7. Halliburton finished rigging up their hard line and missle. Rock Water is still rigging up their water transfer hose and pump. We still lack +/- 4,300 bbls of water. We began loading 30/50 White Sand. Halliburton is rigged up and pressure tested at well head 1,500 psi for 5 min and 9,500 psi for 10 min, also bucket tested. Chemicals are here except for the X-Link, it is scheduled to arrive before midnight. Hammer delivered bleach and added it to all the frac tanks today. - Water haulers continuing to fill frac tanks. Hammer will be adding bleach to the water today. Halliburton continuing to spot in frac equipment. On site job training to be conducted today on the rigging up and pressure testing procedures for flow back equipment. - Flow Back crew finish rigging up iron to well. RNI Trucking continue to Haul in fresh water filling frac tanks
Daily Cost: $0
Cumulative Cost: $114,908

8/16/2013 Day: 4 **Completion**

Rigless on 8/16/2013 - Frac stage 1-3 - Hauled sand and chemicals throughout the night. - Reposition frac van for WL crane. - Global Kick Outs set at 9000 psi. Pressure tested to 9500 psi. Treated real tight early. Worked up rate as pressure allowed and displaced acid. Good relief once acid hit. Worked up to rate. - Plug 1##Make up WL tools (guns Tools are as follows. Cable head 2? x 10?, sinker bar 5? x 2.75?, CCL 1.25? x 3.12?, perforating gun 3? x 2.75?, perforating gun 3? x 2.75?, quick change 1.5? x 3.13?, Baker 20 ? 6? x 3.38?, Halliburton Obsidian Plug 2? x 3.62?. RU JW WL. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. # RIH with plug and perf guns at 250 ? 280 fpm to 7,450? and correlated depth with casing tally due to not having the previous logs available yet. Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 14 bpm slowed speed down to 150 fpm with line tension averaging 820#. Pump down to target depth past casing collar @ 13,111?. We slowed pumps down to 1 bpm and picked up and set plug @ 13,090?. Waited 2 minutes and we dropped 76# of line tension, but we never felt the charge either at the well head or the e-line. Pulled up hole to target depth and perforated 2? with 6spf from 13,038 ? 13,040?. Pulled

up and perforated again 2? with 6spf from 12,944? ? 12,946?. Currently logging out of hole. - Stage #2'. PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage #2 as follows: Wellhead 3,804 psi, BD Fluid 435 bbls Fresh water/15% acid, Fractured well 1,814 bbls of 20# Delta 200/Slickwater, Max Treating 6,925 psi, Minimun Treating 5,488 psi, Ave treating 6,060 psi, ISDP 4,992 psi, Ave Rate 34 bpm, Flushed Over 292 bbls, Ave HHP 5,109 HHP, Max Rate 35 bpm, Pumped 3,522 LBS 100 Mesh, 96,108 LBS 30/50 White Sand, Total Fluid Recover 2,540, Ball seat stage pressures and rate; 6,007 psi @ 12.3 bpm, 5,395 psi. Pressure before seating, 5,961 psi. Pressure after seating. WG-36-21.1% (265.8) CL-31-7.9% (2.5) Optiflo 11-5.7% (3.8), CLA-Web-5.5% (2.9) Comments Global Kick Outs set @ 9000 psi. Pressure tested to 9,550' psi. Stage went well. - Plug 2#. Make up WL tools (guns and plug). Tools are as follows. Cable head 2? x 10?, sinker bar 5? x 2.75?, CCL 1.25? x 3.12?, perforating gun 3? x 2.75?, perforating gun 3? x 2.75?, quick change 1.5? x 3.13?, Baker 20 ? 6? x 3.38?, Halliburton Obsidian Plug 2? x 3.62?. RU JW WL. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. RIH with plug and perf guns at 250 ? 280 fpm to 7,450? and correlated depth with casing tally due to not having the previous logs available yet. Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 14 bpm slowed speed down to 150 fpm with line tension averaging 820#. Pump down to target depth past casing collar @ 12934'. We slowed pumps down to 1 bpm and picked up and set plug @ 12908. Waited 2 minutes and we dropped 76# of line tension, but we never felt the charge either at the well head or the e-line. Pulled up hole to target depth and perforated 2? with 6spf from 12,820'- 12,822' Pulled up and perforated again 2? with 6spf from 12,750'- 12,752'. Currently logging out of hole.POOH. Bump up into lube and closed well in. Dropped Frac ball and installed cap. - Stage #3'. PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage #3 as follows: Wellhead 3,879 psi, BD 5,679' psi, BD Fluid 376 bbls Fresh water/15% acid, Fractured well 2,119'bbls of 20# Delta 200/Slickwater, Max Treating 6,993' psi, Minimun Treating 5,676' psi, Ave treating 6,102' psi, ISDP 4,960' psi, Ave Rate 35' bpm, Flushed Over 288' bbls, Ave HHP 5,250' HHP, Max Rate 36' bpm, Pumped 3,440' LBS 100 Mesh, 90,125' LBS 30/50 White Sand, Total Fluid Recover 2,783', Ball seat stage pressures and rate; 5,676'psi @ 12.1 bpm, 5,673 psi. Pressure before seating, 5,450' psi. Pressure after seating. WG-36-11.9% (175.9)BC-200-14.1% (20.9), FR-66-19.8% (1.5), CL-31-8.1% (3), Scalesorb 7-12.9% (53.7), Losurf 300D-20.5% (23.7), SP Breaker-31.4% (5), Optiflo H T E-40.8% (13.1), CLA -Web-20.5% (11.9), MCB 8630-37.8% (10.9). - Plug 3#. Make up WL tools (guns and plug). Tools are as follows. Cable head 2? x 10?, sinker bar 5? x 2.75?, CCL 1.25? x 3.12?, perforating gun 3? x 2.75?, perforating gun 3? x 2.75?, quick change 1.5? x 3.13?, Baker 20 ? 6? x 3.38?, Halliburton Obsidian Plug 2? x 3.62?. RU JW WL. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. RIH with plug and perf guns at 250 ? 280 fpm to 7,450? and correlated depth with casing tally due to not having the previous logs available yet. Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 14 bpm slowed speed down to 150 fpm with line tension averaging 820#. Pump down to target depth past casing collar @ 12,703 We slowed pumps down to 1 bpm and picked up and set plug @ 12,681' Waited 2 minutes and we dropped 76# of line tension, but we never felt the charge either at the well head or the e-line. Pulled up hole to target depth and perforated 2? with 6spf from 12,590'-12,592'. Pulled up and perforated again 2? with 6spf from 12,530'-12,532'. Currently logging out of hole. POOH. Bump up into lube and closed well in. Dropped ball and installed cap. - Stage #4'. PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage #4 as follows: Wellhead 3,897' psi, BD Fluid 642 bbls Fresh water/15% acid, Fractured well 1,507' bbls of 17# Delta 200/Slickwater, Max Treating 7,820' psi, Minimun Treating 5,145' psi, Ave treating 5,787' psi, ISDP 5,023' psi, Ave Rate 35' bpm, Flushed Over 283'' bbls, Ave HHP 5,021'' HHP, Max Rate 36' bpm, Pumped 110,819 LBS 30/50 White Sand, Total Fluid Recover 2,432', Ball seated 30 bbls early, BC-200-2.4% (2.8), Scalesorb 7-2% (7), MX 2-2738-8-6% (2.6), Optiflo !!-35% (2.4), MCB 8630-9.9% (2.5). - Tested chemicals and held PJSM with all personnel on location. Rigging up WL and prepping to begin pumping.

Daily Cost: $0

Cumulative Cost: $323,418

8/17/2013 Day: 5 **Completion**

Rigless on 8/17/2013 - RU Halliburton started pump flushed 12 bpm pump 205 bbls 8781 psi, Open well flow back. - Flowed well back 515 bbls on a 31/64?s choke. We attempted to get back into stage

5 with 254 bbls fresh water and well stabilized at 8800 psi @ 3bpm with no success. Flowed well back again 270 bbls at 9 bpm on a 36/64?s choke, well quit flowing and flowback manifold pressure was @ 0 psi and well head pressure was @ 3881 psi. Attempted to pump back into it with 176 bbls and pressure stabilized at 8821 psi @ 3bpm while we waited for FMC Well head technician to bring out ring gaskets for flanges on flowcross. FMC on location. PJSM. We closed well with 2 barriers, upper MCV and inside 2 1/16? wing valve. BWO and break out flowback iron from frac tree, we did not find the ball or any other restriction. Closed HCV for 2nd barrier and opened inside 2 1/16? valve then verified that there was no restriction through the flow cross. Nothing found. We used Halliburton and pumped through bleeder line and down through flowback and verified that the flowback iron was clear, iron clear. Re-installed flowback iron to well head and pressure tested all broken connection to 300 psi for 5 min and 10,000 psi fir 10 min, tests good. Plan forward: Attempt to flow well back again to see if plug ball re-seats itself in frac tree. - We were able to re-seat ball in flow cross. Closed middle MCV. Held PJSM for flowing well through frac and flow back in an attempt to catch 2 3/8" plug ball in frac iron at their manifold. Opened up well through frac and flow well through riser. Flowed approx 30 bbls. Closed well in and broke frac surface lines apart at bottom of well head, no ball. Hook up frac lines and pressure test to 9,500 psi. Test good. Flow well back through flowback in an attempt to either re-seat ball in flow cross or recover 407 bbls from well bore. - No ball to surface. Fired up Halliburton pumps and pump away 274 bbls at 10 bpm @ +/-6,700 psi and ball seated into plug and pressure spiked to 8,900 psi and kicked out pumps. Decision made to change out flowback wing on flowback side of flow cross from 2 1/16" to 4 1/16" so that the larger ID could capture the 2 3/8" ball. Changed out wing on flowcross and pressure testing replacement at time of co man change out. - Cameron test cross flow. Test good Rockwater NU from 2 1/16" to 4 1/16" so that the larger ID could capture the 2 3/8" ball. Open well 3600 psi flow 10 bpm 10 mins 400 psi flow @ 8 bpm waiting for 2-3/8 ball capture in 4-1/16 flange - Plug 4#. Make up WL tools (guns and plug). Tools are as follows. Cable head 2? x 10?, sinker bar 5? x 2.75?, CCL 1.25? x 3.12?, perforating gun 3? x 2.75?, perforating gun 3? x 2.75?, quick change 1.5? x 3.13?, Baker 20 ? 6? x 3.38?, Halliburton Obsidian Plug 2? x 3.62?. RU JW WL. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. RIH with plug and perf guns at 250 ? 280 fpm to 7,450? and correlated depth with casing tally due to not having the previous logs available yet. Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 14 bpm slowed speed down to 150 fpm with line tension averaging 820#. Pump down to target depth past casing collar @ 12,477 We slowed pumps down to 1 bpm and picked up and set plug @ 12,498'' Waited 2 minutes and we dropped 76# of line tension, but we never felt the charge either at the well head or the e-line. Pulled up hole to target depth and perforated 2? with 6spf 12 Holes, 60% from 12,440-12,442'. Pulled up and perforated again 2? with 6spf 12 Holes 60% from 12,370-12,372'. Currently logging out of hole. POOH. Bump up into lube and closed well in. All guns fired, Dropped ball and installed cap. Going Fracing stage #5 - Stage #5'. PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage #5 as follows: Wellhead 3,873' psi, BD 5,616 psi, BD Fluid 520 bbls Fresh water/15% acid, Fractured well 996'' bbls of 17# Delta 200/Slickwater, Max Treating 9,760' psi, Minimun Treating 5,462' psi, Ave treating 6,029' psi, ISDP 9,433' psi, Ave Rate 36' bpm, Flushed Over 49' bbls, Ave HHP 5,261' HHP, Max Rate 36' bpm, Pumped 108,413' LBS 30/50 White Sand, Total Fluid Recover 1,565',Global Kick Outs set @ 8800 psi. Psi tested to 9500 psi. Seated ball @ 274 bbls and 12 bpm. Broke over @ 5616 psi. Job went smoothy unitl screening out 50 blls into flush. Psi turned @ 5 ppg bh prop conc. Ball set stage psi and rate 5616 psi @ 11.7 bpm, 5217 psi pressurn before seating 5554 psi, pressure after seating. WG-36-2.2% (15.9), BC-200-3.8% (3.1), Optiflo 11-4-4% (1.7), Losurf 300D-3.55 (2.3), CLA-web-9.6% (3.1).

Daily Cost: $0

Cumulative Cost: $453,647

8/18/2013 Day: 6 **Completion**

Rigless on 8/18/2013 - MIRU Cudd CTU - Open well 3000 psi on well -flow back 6 bpm @ 1000 psi, after 1 hr 104 bbls flow 3.5 bpm @ 300 psi. - Cudd CTU arrived on location at 1330 hrs. PJSM. Assess location for CTU rig up. Rigging up Cudd CTU. - NU Cudd 2" coil tubing BOP stack of: 7-1/16" 10k x 4-1/16" 15K spool, 4-1/16" 15K Blind shear rams, 4-1/16" 15 manual gate valve, 4-1/16' 15K pipe rams, flow cross w/2 inside manual gate valves, 2 outside HCR valves, Quad BOP stack (bottom to top): pipe rams, slips, shear & Blinds. - - Open well 4000 psi flow 10 bpm 10 mins 400 psi flow @ 8 bpm waiting for 2-3/8 ball capture in 4-1/16 flange. Shut well in, Total 596 bbls flow back no ball.

RECEIVED: Oct. 10, 2013

Fired up Halliburton started pump flushed 12 bpm pump way 205 bbls went from +/- 6,890 8,900 psi kicked out pump. Open well flow back 10 bpm @ 4000 psi 15 mins, psi @ 150 flow 3.5 bpm Total 587 bbls no sand no ball. - Fired up Halliburton pumps away 306 bbls at 3.5 bpm @ +/-8,700 psi @ 8,900 psi and kicked out pumps. @ 7,600 psi fired up pump, an pump 3.5 bpm pump way 4 bbls psi up 8,900, kicked out pump. - Flowing well back. Well is @ 0 psi flowing @ a rate of 1.3 bpm. - @ 09125 hrs we shut the well in to allow it to build up pressure. Pressure increased from 0 ? 2,100 psi. Surged well through gut line 5 times and pressure went down to 900 psi. Turned well over to Halliburton and we walked the pumps up to 16.8 bpm as per Stimtech Engineer and were to get 87 bbls fresh water in hole until the pumps kicked out at 9,191 psi. Surged well again down to 3,400 psi and turned well over to Halliburton. Halliburton ramped up rate to 20 bpm as per Stimtech Engineer and pumped 8 bbls into well before pumps kicker out at 9,000 - Decision made to go with Cudd CTU to wash out sand and abrasive perforate wellbore.
Daily Cost: $0
Cumulative Cost: $500,880

8/19/2013 Day: 7 **Completion**

Rigless on 8/19/2013 - RDMO CTU - TTS Slip Type Coil Connector was installed and pressure tested to 250 psi for 5 min and 9,000 psi for 10 min. When Coil Connector was installed it was pull tested to 25,000#. MU TTS BHA. 2.88" OD X 1.64' Coil Connector with dual BPV, 2.88" X 5.97' Hydra Set Jar, 2.88" x 2.24' Hydraulic Disconnect, 3.7" x 3.16' Bypassing Abrasive Perforator, 2.88" x 12.34' Titan Supermax Motor, 4.625" x 1' Flat Bottom Junk Mill. Re-install CT BOP onto frac tree and shell test 250 psi for 5 min and 9,000 psi for 10 min. PJSM. - POOH to depth 12,195'. Started sand perf 1,200' LB .7 ppg 100 mesh pump 2.5' bpm tubing @ 5,400' psi 3.5' bpm returns @ 900 psi, pump 47'bbls and perforated tub psi 5,300' 3.5' bpm returns @ 800' psi 1? with 6spf 12 Holes 60%. Pull up to 12,193. sand perf 1,200 LB .7 ppg 100 mesh pump 2.5 bpm tubing @ 5,300' psi 3.5' bpm returns, @ 800 psi, pump 47 bbls and perforated tub psi @ 5,200' psi 3.5' bpm returns @ 800' psi. 1? with 6spf 12 Holes 60%. Pump 127 bbls fresh water flush w/10' bbl gel sweep. - POOH to 8,000' pump 2.5' bpm WH @ 1,000' psi 3.5' bpm @ 1,000' psi on returns. No sand on returns Drop 5/8' ball shift tool - Testing lubricator & injector Head - depth 12,290. Started sand perf 1,200 LB .7 ppg 100 mesh pump 2.5' bpm tubing @ 5,800' psi 3.5' bpm returns @ 1,000' psi, pump 47 bbls and perforated tub psi 5,400' 1? with 6spf 12 Holes 60%. Pull up to 12,288. sand perf 1,200 LB .7 ppg 100' mesh pump 2.5' bpm tubing @ 5,400' psi 3.5' bpm returns, pump 47 bbls and perforated tub psi @ 5,200' psi 3.5' bpm returns 800'psi. 1? with 6spf 12 Holes 60%. Pump 127'bbls fresh water flush w/10' bbl gel sweep. - Circulated out both sweeps and prepped sand hopper for perforating. Dropped small ball and pumped it through coil. - Equalize pressure and RIH with TTS clean out assembly. RIH with CT @ 80? ? 90? fpm to KOP. Stopped and got up weight of +/- 22K. Increased pump rate to 2.5 bpm and adjusted flowback choke to achieve the same returns. Continued in hole @ 40 fpm and tagged sand @ 9,040?. Currently @ 10,090? washing in hole. Target depth of 12,330? reached. Pulled up 30? and pumped a 2 stage sweep 10 bbls sweep, 10 bbls fresh water, 10 bbls sweep at 3 bpm.
Daily Cost: $0
Cumulative Cost: $572,537

8/20/2013 Day: 8 **Completion**

Rigless on 8/20/2013 - .Frac - POOH to 8,000? pump 2.5' bpm @ 1,000? psi on WH, shut HCR valve on CT 2" line going to flowback. Opened 4 1/16" wing on FMC frac tree to establish injection rate. Started injection pumping 10 bbls @ 2.5 bpm 4,000 psi, 3.0 bpm 10 bbls 5,000 psi, 3.0 bpm, 10 bbls 6,000 psi, 3.0 bpm 50' bbls max psi 6,500? good injection. Total 80' bbls max psi 6,500 psi. 6,500 PSI was coil pressure through tools. Casing pressure leveled out at +/- 2,500 PSI @ 3 bpm during injection test. - POOH w/BHA at 100 fpm while pumping @ 2.5' bpm. Coil is out of the hole and well is closed in. PJSM on rigging down Cudd CTU. - Finish rigging up JW & Halliburton. PJSM for Frac.Open well. Global kick outs set to 9,500 psi. Pressure tested to 9,000 psi. Pump Stage 6, a modified 4# max design with 20# gel. Placed 100% without issue. RIH and set Halliburton Obsidian plug @ 12,119?. Pulled up hole and perforated @ 12,047? ? 12,049? and 12,000? ? 12,002?. RD WL and drop ball. Pressure test to 9,500 psi. - Frac Stage 7# PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage #7 as follows: Wellhead 3,869 psi, BD Fluid 642 bbls Fractured well 1255 bbls of 20# Delta 200/Slickwater, Max Treating 6322 psi, Minimum Treating 5395 psi, Ave treating 5811 psi, ISDP

4897 psi, Ave Rate 35 bpm, Flushed Over 271 bbls, Ave HHP 4956 HHP, Max Rate 35 bpm, Pumped 115177 LBS 30/50 White Sand, Total Fluid Recover 2168 Stage went well. Ball seat stage pressure & rate 5438 psi @ 14.3 bpm, 4947 psi pressure before seating 5423 psi pressure after seating - Shift tool RIH w/BHA pump 2.5 bpm fresh water pump 10 bbl gel sweep tag @ 12,278' wash 20' ft pump 10' bbl gel sweep P/U 50' ft wash down to 12,298'. P/U 50' ft wash down to 12,330'. Circulate parafin & sand back. Pump 2' 10' bbl gel sweep. Circulate clean no sand or paraffin. - Plug 10#. Make up WL tools (guns and plug). Tools are as follows. Cable head 2? x 10?, sinker bar 5? x 2.75?, CCL 1.25? x 3.12?, perforating gun 3? x 2.75?, perforating gun 3? x 2.75?, quick change 1.5? x 3.13?, Baker 20 ? 6? x 3.38?, Halliburton Obsidian Plug 2? x 3.62?. RU JW WL. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. RIH with plug Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 14 bpm slowed speed down to 150 fpm with line tension averaging 948 Pump down to target depth past casing collar @ 11505 pumps down to 1 bpm and picked up and set plug @ 11526 Waited 1 minutes and we dropped 100 of line tension, Pulled up hole to target depth and perforated 2? with 6spf 12 Holes, 60% from 11470-11472 Pulled up and perforated again 2? with 6spf 12 Holes 60% from 11340-11342- Currently logging out of hole POOH Bump up into lube and closed well in. All guns fired, Dropped ball and installed cap - Frac Stage 9# PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage #9 as follows: Wellhead 3802 psi, BD Fluid 474 bbls Fractured well 1056 bbls of 20# Delta 200/Slickwater, Max Treating 7107 psi, Minimum Treating 4991 psi, Ave treating 5652 psi, ISDP 5981 psi, Ave Rate 35 bpm, Flushed Over 261 bbls, Ave HHP 4779 HHP, Max Rate 36 bpm, Pumped 105600 LBS 30/50 White Sand, Total Fluid Recover 1791 Stage went well. Observed a weak indication of the ball seating @ 260 bbls, Pumped a 20 Ib gell system Held 5 ppg due to pressure rise when 4 ppg hit formation cut prop 5000 Ibs early due to turn up in psi - Plug 9#. Make up WL tools (guns and plug). Tools are as follows. Cable head 2? x 10?, sinker bar 5? x 2.75?, CCL 1.25? x 3.12?, perforating gun 3? x 2.75?, perforating gun 3? x 2.75?, quick change 1.5? x 3.13?, Baker 20 ? 6? x 3.38?, Halliburton Obsidian Plug 2? x 3.62?. RU JW WL. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. RIH with plug Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 14 bpm slowed speed down to 150 fpm with line tension averaging 1153#. Pump down to target depth past casing collar @ 12,477 We slowed pumps down to 1 bpm and picked up and set plug @ 11710' Waited 1 minutes and we dropped 228# of line tension, Pulled up hole to target depth and perforated 2? with 6spf 12 Holes, 60% from 11639-11641 Pulled up and perforated again 2? with 6spf 12 Holes 60% from 11553-11555 Currently logging out of hole POOH Bump up into lube and closed well in. All guns fired, Dropped ball and installed cap - ND Cudd CTU from well and set aside with only breaking down lubricator. RD Cudd crane and set it out of the way. RD Cudd pump and sent it in for either repairs or to be swapped out. Move in JW WL crane and BOP/Lube trailer. RU Halliburton. Install and torque WL 7 1/16? flange. H.O.T. is on location to heat paraffin in flowback tanks for transfer. Hot work permit filled out and SMS Safety hand Wade Parsons is on location for PJSM. - RIH with WL and set plug 8 @ 11,941. Pull up and perforate as per program at 11,840-11,842 and 11,790-11,792?. POOH, Drop ball Frac Stage 8# PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage #8 as follows: Wellhead 3,957 psi, BD Fluid 544 bbls Fractured well 874 bbls of 20# Delta 200/Slickwater, Max Treating 8,278 psi, Minimum Treating 5,065 psi, Ave treating 6,712 psi, ISDP 4,773 psi, Ave Rate 35 bpm, Flushed Over 266 bbls, Ave HHP 5,807?HHP, Max Rate 41bpm, Pumped 114315 LBS 30/50 White Sand, Total Fluid Recover 1,684? Stage went well. Ball seat stage pressure & rate 4,991 psi @ 11.5 bpm, 4,750 psi pressure before seating 5,041 psi pressure after seating

Daily Cost: $0

Cumulative Cost: $917,840

8/21/2013 Day: 9 **Completion**

Rigless on 8/21/2013 - Frac - RU JW WL. Plug #18. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. RIH with plug 18 Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 14 bpm slowed speed down to 150 fpm with line tension averaging 1011 Pump down to target depth past casing collar @ 9,896 pumps down to 1 bpm and picked up and set plug @ 9,911 Waited 1 minutes dropped 150 of line tension Total 79 bbls pump POOH depth and perforated 2? with 6spf 12 Holes, 60% from 9870-9872 Pulled up and perforated 2? with 6spf 12

Holes 60% from 9790-9792 POOH Bump up into lube and closed well in. All guns fired, Dropped ball and installed cap - Frac Stage 17 PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage 17 as follows: Wellhead 3811 psi, BD Fluid 320 bbls Fractured well 987 bbls of 20# Delta 200/Slickwater, Max Treating 7085 psi, Minimum Treating 5091 psi, Ave treating 5704 psi, ISDP 5756 psi, Ave Rate 36 bpm, Flushed Over 226 bbls, Ave HHP 4777 HHP, Max Rate 36 bpm, Pumped 110400 LBS 30/50 White Sand, Total Fluid Recover 1533 Stage went well.Comments: 1. Global Kick Outs set at 9000 psi. Pressure tested to 9570 psi. 2. Job went well, placed all sand.Optiflo II-2.6% (1.2), Losurf 300D-5.3% (3.4) WG-36-2.9% (23.9),Optiflo II-2.6% (1.2), Losurf 300D-5.3% (3.4) - Pressure test lubricator to 9,500 psi. RIH with wireline and set plug for stage 17 @ 10,101. Pulled up and perforated from 10,050-10052 and 9,970-9,972 Max rate was at 14.0 bpm and max pressure was at 4,552 psi, 47 bbls used for pump down. POOH with WL. - Frac Stage 16 PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage 16 as follows: Wellhead 3840 psi, BD Fluid 379 bbls Fractured well 929 bbls of 20# Delta 200/Slickwater, Max Treating 6910 psi, Minimum Treating 4865 psi, Ave treating 5417 psi, ISDP 5492 psi, Ave Rate 36 bpm, Flushed Over 231 bbls, Ave HHP 4793 HHP, Max Rate 37 bpm, Pumped 110200 LBS 30/50 White Sand, Total Fluid Recover 1539 Stage went well.Comments: 1. Global Kick Outs set at 9000 psi. Pressure tested to 9500 psi. 2. Placed all sand, job went smooth.WG-36-4.5% (35.5), Optiflo II-16.6% (8.6), Losurf 300D-4.1% (2.6) Optiflo H T E-15.9% (2.7), CLA-Web-10.3% (3.3), MCB 8630-16% (2.1) - Stage 15 - Stage went well. 1. Global Kick Outs set at 9000 psi. Pressure tested to 9500 psi. 2. Slight indication of ball seating. Went 10 bbls over wellbore volume and proceeded with job. Ball Seat Stage Pressures and Rate: 4861 psi @ 14.4 bpm , 4854 psi Pressure before Seating , 4863 psi Pressure after Seating WG-36-13.1% (102.9), BC-200-2.8% (2.2), Optiflo II-3.7% (1.2), Losurf 300D-6.2% (4.2) CLA-Web-3.3% (1.1), Pressure test lubricator to 9,500 psi. RIH with wireline and set plug for stage 16 @ 10,329?. Pulled up and perforated from 10,257? ? 10,259? and 10,172? ? 10,174?. Max rate was at 15.7 bpm and max pressure was at 5,429psi, 124 bbls used for pump down. POOH with WL. - Stage 14 - Went back to 17# gel. Pressure slope changed on flush with 5# on formation. Increased rate 4 bpm (35 - 38). Able to place job completely. 1. Global Kick Outs set at 9000 psi. Pressure tested to 9500 psi. Very slight indication of ball seating. Pumped 10 bbls over wellbore volume then proceeded with job. First crosslink sample came in looking real weak. Held off on starting sand until a good sample was obtained. Pressure slope changed on flush with 5# on perfs. Had pump operator increase rate 4 bpm. Able to finish out flush and place job completely. Ball Seat Stage Pressures and Rate: 4725 psi @ 14.5 bpm , 4722 psi Pressure before Seating , 4731 psi Pressure after Seating WG-36-23% (164.3), MX 2-2738 -5.3% (1.1) Losurf 300D-11% (7.6) CLA-Web-11% (3.8), Pressure test lubricator to 9,500 psi. RIH with wireline and set plug for stage 15 @ 10,?515. Pulled up and perforated from 10,480? ? 10,482? and 10,415? ? 10,417?. Max rate was at 15.0 bpm and max pressure was at 7,109psi, 194 bbls used for pump down. POOH with WL. - Global Kick Outs set at 9000 psi. Pressure tested to 9500 psi. Stage went well. Had issues with fracpro during stage. Had to rerun data from Halliburton acquisition files. Ball Seat Stage Pressures and Rate: 4745 psi @ 14.4 bpm , 4738 psi Pressure before Seating , 4745 psi Pressure after Seating WG-36-6.8% (54.1), MX 2-2738 -9.5% (1.9) Got ISIP, 5, 10, and 15 for this stage. 5 ? 5,138psi, 10 ? 4,685psi, 15 ? 4,366psi. RIH with wireline and set plug for stage 14 @ 10,?699. Pulled up and perforated from 10,627? ? 10,629? and 10,541? ? 10,543?. Max rate was at 15.4 bpm and max pressure was at 5,689psi, 148 bbls used for pump down. POOH with WL. - Set Global kick outs at 9,500 psi. Pressure tested to 9,468 psi. Pumped stage 12 as per program. Stage went well. Got ISIP, 5, 10, and 15 for this stage. 5 ? 4,523psi, 10 ? 4,171psi, 15 ? 4,096psi. RIH with wireline and set plug for stage 13 @ 10,927?. Pulled up and perforated from 10,880? ? 10,882? and 10,760? ? 10,762?. Max rate was at 14 bpm and max pressure was at 5,856psi, 199 bbls used for pump down. POOH with WL. WL pump down parameters have stayed the same throughout the job. - Plug 12. Make up WL tools (guns and plug). Tools are as follows. Cable head 2? x 10?, sinker bar 5? x 2.75?, CCL 1.25? x 3.12?, perforating gun 3? x 2.75?, perforating gun 3? x 2.75?, quick change 1.5? x 3.13?, Baker 20 ? 6? x 3.38?, Halliburton Obsidian Plug 2? x 3.62?. RU JW WL. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. RIH with plug Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 14 bpm slowed speed down to 150 fpm with line tension averaging 917 Pump down to target depth past casing collar @ 11083 pumps down to 1 bpm and picked up and set plug @ 11104 Waited 1 minutes dropped 162 of line tension Total 152 bbls pump POOH depth and perforated 2? with 6spf 12 Holes, 60% from 11060-11062 Pulled up and perforated 2? with 6spf 12 Holes 60% from 10990-10992 Currently logging out of hole POOH Bump up into lube and closed well in. All guns fired, Dropped ball and installed cap - Frac Stage 11 PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage

RECEIVED: Oct. 10, 2013

11 as follows: Wellhead 6677 psi, BD Fluid 447 bbls Fractured well 1034 bbls of 20# Delta 200/Slickwater, Max Treating 7473 psi, Minimum Treating 5178 psi, Ave treating 5752 psi, ISDP 5890 psi, Ave Rate 36 bpm, Flushed Over 252 bbls, Ave HHP 5061 HHP, Max Rate 36 bpm, Pumped 110300 LBS 30/50 White Sand, Total Fluid Recover 1733 Stage went well. - Plug 11. Make up WL tools (guns and plug). Tools are as follows. Cable head 2? x 10?, sinker bar 5? x 2.75?, CCL 1.25? x 3.12?, perforating gun 3? x 2.75?, perforating gun 3? x 2.75?, quick change 1.5? x 3.13?, Baker 20 ? 6? x 3.38?, Halliburton Obsidian Plug 2? x 3.62?. RU JW WL. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. RIH with plug Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 13 bpm slowed speed down to 150 fpm with line tension averaging 1143 Pump down to target depth past casing collar @ 11276 pumps down to 1 bpm and picked up and set plug @ 11297 Waited 1 minutes and we dropped 252 of line tension Total 170 bbls pump Pulled up hole to target depth and perforated 2? with 6spf 12 Holes, 60% from 11240-11242 Pulled up and perforated 2? with 6spf 12 Holes 60% from 11130-11132 Currently logging out of hole POOH Bump up into lube and closed well in. All guns fired, Dropped ball and installed cap - Frac Stage 10 PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage 10 as follows: Wellhead 3879 psi, BD Fluid 454 bbls Fractured well 1075 bbls of 20# Delta 200/Slickwater, Max Treating 7372 psi, Minimum Treating 5149 psi, Ave treating 5956 psi, ISDP 5565 psi, Ave Rate 35 bpm, Flushed Over 256 bbls, Ave HHP 5109 HHP, Max Rate 36 bpm, Pumped 110800 LBS 30/50 White Sand, Total Fluid Recover 1785 Stage went well. Did not observe any indication of the ball seating at or around WBV Job was pumped smoothly to completion with all proppant placed

Daily Cost: $0

Cumulative Cost: $1,668,119

8/22/2013 Day: 10 **Completion**

Rigless on 8/22/2013 - Flowing well to production - Frac Stage 18 PJSM Prime pumps and test lines to 9,500 psi. Hydraulic Fracture Stage 18 as follows: Wellhead 3845 psi, BD Fluid 304 bbls Fractured well 984 bbls of 20# Delta 200/Slickwater, Max Treating 7903 psi, Minimum Treating 5195 psi, Ave treating 5824 psi, ISDP 6418 psi, Ave Rate 36 bpm, Flushed Over 222 bbls, Ave HHP 5082 HHP, Max Rate 37 bpm, Pumped 105770 LBS 30/50 White Sand, Total Fluid Recover 1510 Stage went well.Comments: 1. Global Kick Outs set at 9000 psi. Pressure tested to 9487 psi. 2. Lost rate during flush due to catching air at the blender. WG-36-5.2% (43.2), BC-200-7.7% (6.4), Optiflo II-4.7% (1.6), Losurf 300D-6.9% (4.4) CLA-Web-8.5% (2.7), - Plug #19. Function test WL BOP?s, test good. Pressure test lube to 9,500 PSI, held for 5 min, test good. RIH with plug 19 Continue in hole to KOP and slow down to 200 ? 220 fpm ramped up pump 3, 6, 8, 10, 12, 14 bpm to get WL tools around curve. Continue pumping tools down hole at 14 bpm slowed speed down to 150 fpm with line tension averaging 1066 Pump down to target depth past casing collar @ 9,714 pumps down to 1 bpm and picked up and set plug @ 9733 Waited 1 minutes dropped 192 of line tension Total 102 bbls pump POOH depth and perforated 2? with 6spf 12 Holes, 60% from 9700-9702 Pulled up and perforated 2? with 6spf 12 Holes 60% from 9626-9628 POOH Bump up into lube and closed well in. All guns fired, Dropped ball and installed cap. - Frac Stage 19. We 142 bbls in to are flush screen out, flow back @ 4,500? psi on 21/64 choke 6 bpm FB 245 bbls ball came up catch in 4-1/16 X 2-1/16 flange. Broke out flange recover ball. NU 4-1/16 X 2-1/16 flange test to 9,500? psi test good. Flow back @ 3,800 psi 6 bpm get back sand. FB 213 bbls no sand - Install lubricator with plug and guns for stage #20. Pressure test to 9,500 psi. Ran in hole with wireline to 500? and found CCL not working. POOH with wireline and re-headed e-line, still not functioning. E-line back up and running, Install and test lubricator to 9,500 psi. RIH, correlate and set Halliburton Obsidian plug for stage #20 @ 9,504?. Pull up and perforate as per program from9.450? ? 9,452? and 9,400? ? 9,402?. POOH with WL. We were down with WL failures for 3 hrs. - 1. Global Kick Outs set at 9000 psi. Pressure tested to 9500 psi. 2. Had roughly 15,000 lbs of proppant extra due to stg 19 screening out. Distributed amongst 4, 5 and 6 ppa sand stages. 3. Lost a pump near the end of the stage. Worked up rate with others. Sand and chemicals came out pretty good. A couple of small issues accounting for some of the chemicals found at the end of the well, but were discussed with the engineer and should be resolved for the next well. Fresh water volume at end of frac is 2,160 bbls to be used for drilling out plugs after flowback - RDMO Halliburton, JW wireline, Pro Technics. All equipment is off of location. Rock Water flowback is RU iron to production flowline. Cameron tester is flanging up and testing 7 1/16" x 10k flange onto goats head and then he will pressure test flowback iron. - Flowback iron is rigged up to the production flow line

and Cameron pressure tester is pressure testing it. - 19:30 -Temp 75*, FCP 3,600? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 00.0 bbls water gas-000 mcf. Sand-None 20:30 -Temp 77*, FCP 3,000? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 16.0 bbls water gas-000 mcf. Sand-Med 21:30 -Temp 78*, FCP 2,750? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 32.0 bbls water gas-000 mcf. Sand-Med 22:00 -Temp 80*, FCP 3,300? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 33.0 bbls water gas-000 mcf. Sand-Med 23:00 -Temp 87*, FCP 3,300? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 60.0 bbls water gas-000 mcf. Sand-Med 00:00 -Temp 98*, FCP 3,450? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 61.0 bbls water gas-000 mcf. Sand-Light Total BBLs flow back-202, bbls
Daily Cost: $0
Cumulative Cost: $2,108,977

8/23/2013 Day: 11 **Completion**

Rigless on 8/23/2013 - Flowback - 21:00-Temp 118*, FCP 3,157 psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 60.0 bbls water gas-048 mcf. Sand-Light 22:00 -Temp 118*, FCP 3,137? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 53.0 bbls water gas-044 mcf. Sand-Light 23:00 -Temp 121*, FCP 3,133? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 55.0 bbls water gas-056 mcf. Sand-Light 00:00 -Temp 120*, FCP 3,119 psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 53.0 bbls water gas-049 mcf. Sand-Light Total bbls water - 1,653 bbls Flowing for 28 HRS Total bbls oil ? 32 bbls - 01:00 -Temp 95*, FCP 3,450? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 69.0 bbls water gas-000 mcf. Sand-Light 02:00 -Temp 98*, FCP 3,400? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 58.0 bbls water gas-000 mcf. Sand-Light 03:00 -Temp 101*, FCP 3,400? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 65.0 bbls water gas-000 mcf. Sand-Light Total BBLs flow back-394, bbls Flowing for 9 HRS - 04:00 -Temp 105*, FCP 3,400? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 60.0 bbls water gas-000 mcf. Sand-Light 05:00 -Temp 106*, FCP 3,400? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 58.0 bbls water gas-000 mcf. Sand-Light 06:00 -Temp 108*, FCP 3,350? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 55.0 bbls water gas-000 mcf. Sand-Light Total BBLs flowed back-567, bbls Flowing for 12 HRS - 07:00 -Temp 113*, FCP 3,350? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 50.0 bbls water gas-000 mcf. Sand-Light 08:00 -Temp 112*, FCP 3,350? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 66.0 bbls water gas-046 mcf. Sand-Light 09:00 -Temp 113*, FCP 3,325? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 84.0 bbls water gas-034 mcf. Sand-Light Total BBLs flowed back-767 bbls Flowing for 14 HRS - 10:00 -Temp 114*, FCP 3,325? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 58.0 bbls water gas-033 mcf. Sand-Light 11:00 -Temp 116*, FCP 3,300? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 60.0 bbls water gas-037 mcf. Sand-Light 12:00 -Temp 117*, FCP 3,300? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 50.0 bbls water gas-033 mcf. Sand-Light Total BBLs flowed back - 935 bbls Flowing for 17 HRS - 13:00 -Temp 122*, FCP 3,300? psi on 6/64" choke. 1hrs flowing. 005 BBls oil, 58.0 bbls water gas-035 mcf. Sand-Light 14:00 -Temp 124*, FCP 3,275? psi on 6/64" choke. 1hrs flowing. 005 BBls oil, 64.0 bbls water gas-095 mcf. Sand-Light 15:00 -Temp 118*, FCP 3,250? psi on 6/64" choke. 1hrs flowing. 004 BBls oil, 70.0 bbls water gas-098 mcf. Sand-Light Total bbls water - 1127 bbls Flowing for 20 HRS Total bbls oil ? 14 bbls - 16:00-Temp 127*, FCP 3,250 psi on 6/64" choke. 1hrs flowing. 001 BBls oil, 65.0 bbls water gas-042 mcf. Sand-Light 17:00 -Temp 124*, FCP 3,209? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 93.0 bbls water gas-036 mcf. Sand-Light 18:00 -Temp 124*, FCP 3,200? psi on 6/64" choke. 1hrs flowing. 002 BBls oil, 55.0 bbls water gas-038 mcf. Sand-Light 19:00 -Temp 118*, FCP 3,177 psi on 6/64" choke. 1hrs flowing. 15.0 BBls oil, 38.0 bbls water gas-034 mcf. Sand-Light 20;00-Temp 118*, FCP 3,173? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 54.0 bbls water gas-044 mcf. Sand-Light Total bbls water - 1432 bbls Flowing for 24 HRS Total bbls oil ? 32 bbls
Daily Cost: $0
Cumulative Cost: $1,960,549

8/24/2013 Day: 12 **Completion**

Rigless on 8/24/2013 - Flowing well back - 16:00 -Temp 127*, FCP 3,005? psi on 6/64" choke. 1hrs flowing. 15.0 BBls oil, 51.0 bbls water gas-132 mcf. Sand-Light 17:00 -Temp 131*, FCP 3,002? psi on 6/64" choke. 1hrs flowing. 05.0 BBls oil, 53.0 bbls water gas-115 mcf. Sand-Light 18:00 -Temp 129*, FCP 2,992? psi on 6/64" choke. 1hrs flowing. 02.0 BBls oil, 52.0 bbls water gas-141 mcf. Sand-Light Total bbls water ? 2,615 bbls Flowing for 43 HRS Total bbls oil ? 101 bbls - 13:00 -Temp 132*, FCP 3,032? psi on 6/64" choke. 1hrs flowing. 003 BBls oil, 50.0 bbls water gas-091 mcf. Sand-Light 14:00

-Temp 135*, FCP 3,021? psi on 6/64" choke. 1hrs flowing. 002 BBls oil, 60.0 bbls water gas-073 mcf. Sand-Light 15:00 -Temp 131*, FCP 3,038? psi on 6/64" choke. 1hrs flowing. 003 BBls oil, 42.0 bbls water gas-147 mcf. Sand-Light Total bbls water ? 2,459 bbls Flowing for 43 HRS Total bbls oil ? 79 bbls - Cudd came in and blew down their coil then RDMO all equipment and took it over to the Cesspooch 15-21-3-3W. 10:00 -Temp 132*, FCP 3,054? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 64.0 bbls water gas-102 mcf. Sand-Light 11:00 -Temp 131*, FCP 3,055? psi on 6/64" choke. 1hrs flowing. 007 BBls oil, 28.0 bbls water gas-110 mcf. Sand-Light 12:00 -Temp 131*, FCP 3,050? psi on 6/64" choke. 1hrs flowing. 003 BBls oil, 70.0 bbls water gas-111 mcf. Sand-Light Total bbls water ? 2,306 bbls Flowing for 40 HRS Total bbls oil ? 67 bbls - 06:00 -Temp 121*, FCP 3,059? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 53.0 bbls water gas-040 mcf. Sand-Light 07:00 -Temp 133*, FCP 3,053? psi on 6/64" choke. 1hrs flowing. 010 BBls oil, 50.0 bbls water gas-072 mcf. Sand-Light 08:00 -Temp 131*, FCP 3,040? psi on 6/64" choke. 1hrs flowing. 008 BBls oil, 55.0 bbls water gas-069 mcf. Sand-Light 09:00 -Temp 131*, FCP 3,050? psi on 6/64" choke. 1hrs flowing. 007 BBls oil, 53.0 bbls water gas-032 mcf. Sand-Light Total bbls water ? 2,144 bbls Flowing for 37 HRS Total bbls oil ? 57 bbls - 04:00 -Temp 121*, FCP 3,076? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 58.0 bbls water gas-050 mcf. Sand-Light 05:00 -Temp 123*, FCP 3,051? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 50.0 bbls water gas-041 mcf. Sand-Light Total bbls water - 1933 bbls Flowing for 33 HRS Total bbls oil ? 32 bbls - 01:00 -Temp 121*, FCP 3,108? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 55.0 bbls water gas-043 mcf. Sand-Light 02:00 -Temp 119*, FCP 3,098? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 57.0 bbls water gas-050 mcf. Sand-Light 03:00 -Temp 122*, FCP 3,090? psi on 6/64" choke. 1hrs flowing. 000 BBls oil, 60.0 bbls water gas-041 mcf. Sand-Light Total bbls water - 1825 bbls Flowing for 31 HRS Total bbls oil ? 32 bbls - 19:00 -Temp 130*, FCP 2,999? psi on 6/64" choke. 1hrs flowing. 05.0 BBls oil, 40.0 bbls water gas-146 mcf. Sand-Light 20:00 -Temp 123*, FCP 2,998? psi on 6/64" choke. 1hrs flowing. 04.0 BBls oil, 57.0 bbls water gas-137 mcf. Sand-Light 21:00 -Temp 122*, FCP 2,982? psi on 6/64" choke. 1hrs flowing. 06.0 BBls oil, 43.0 bbls water gas-213 mcf. Sand-Light Total bbls water ? 2,755 bbls Flowing for 46 HRS Total bbls oil ? 116 bbls - 22:00 -Temp 121*, FCP 2,999? psi on 6/64" choke. 1hrs flowing. 09.0 BBls oil, 57.0 bbls water gas-164 mcf. Sand-Light 23:00 -Temp 121*, FCP 2,991 psi on 6/64" choke. 1hrs flowing. 08.0 BBls oil, 43.0 bbls water gas-156 mcf. Sand-Light 00:00 -Temp 122*, FCP 2,983? psi on 6/64" choke. 1hrs flowing. 15.00 BBls oil, 43.0 bbls water gas-166 mcf. Sand-Light Total bbls water ? 2,898 bbls Flowing for 49 HRS Total bbls oil ? 148 bbls

Daily Cost: $0

Cumulative Cost: $1,996,394

8/25/2013 Day: 13 **Completion**

Rigless on 8/25/2013 - Flow well back - 04:00 -Temp 118*, FCP 3,001 psi on 6/64" choke. 1hrs flowing. 13.0 BBls oil, 40.0 bbls water gas-211 mcf. Sand-Light 05:00 -Temp 118*, FCP 3,000 psi on 6/64" choke. 1hrs flowing. 19.0 BBls oil, 33.0 bbls water gas-253 mcf. Sand-Light 06:00 -Temp 119*, FCP 3,013 psi on 6/64" choke. 1hrs flowing. 07.0 BBls oil, 37.0 bbls water gas-205 mcf. Sand-Light Total bbls water ? 3,025 bbls Flowing for 53 HRS Total bbls oil ? 163 bbls - 01:00 -Temp 124*, FCP 2,992 psi on 6/64" choke. 1hrs flowing. 02.0 BBls oil, 47.0 bbls water gas-163 mcf. Sand-Light 02:00 -Temp 122*, FCP 2,999 psi on 6/64" choke. 1hrs flowing. 06.0 BBls oil, 43.0 bbls water gas-193 mcf. Sand-Light 03:00 -Temp 119*, FCP 3,013 psi on 6/64" choke. 1hrs flowing. 07.0 BBls oil, 37.0 bbls water gas-205 mcf. Sand-Light Total bbls water ? 3,025 bbls Flowing for 52 HRS Total bbls oil ? 163 bbls - 22:00 -Temp 113*, FCP 3,034? psi on 8/64" choke. 1hrs flowing. 000 BBls oil, 35.0 bbls water gas-183 mcf. Sand-Trace 23:00 -Temp 117*, FCP 3,021? psi on 8/64" choke. 1hrs flowing. 021 BBls oil, 15.0 bbls water gas-168 mcf. Sand-Trace 00:00 -Temp 115*, FCP 3,025? psi on 8/64" choke. 1hrs flowing. 009 BBls oil, 21.0 bbls water gas-189 mcf. Sand-Trace . Total bbls water ? 3,563 bbls Total bbls oil ? 379 bbls Flowing for 77 HRS - 19:00 -Temp 113*, FCP 3,034? psi on 8/64" choke. 1hrs flowing. 000 BBls oil, 35.0 bbls water gas-183 mcf. Sand-Trace 20:00 -Temp 117*, FCP 3,021? psi on 8/64" choke. 1hrs flowing. 021 BBls oil, 15.0 bbls water gas-168 mcf. Sand-Trace 21:00 -Temp 115*, FCP 3,025? psi on 8/64" choke. 1hrs flowing. 009 BBls oil, 21.0 bbls water gas-189 mcf. Sand-Trace . Total bbls water ? 3,563 bbls Total bbls oil ? 379 bbls Flowing for 74 HRS - 16:00 -Temp 122*, FCP 3,010? psi on 8/64" choke. 1hrs flowing. 015 BBls oil, 25.0 bbls water gas-193 mcf. Sand-Trace 17:00 -Temp 121*, FCP 3,032? psi on 8/64" choke. 1hrs flowing. 027 BBls oil, 26.0 bbls water gas-184 mcf. Sand-Trace 18:00 -Temp 113*, FCP 3,030? psi on 8/64" choke. 1hrs flowing. 007 BBls oil, 29.0 bbls water gas-160 mcf. Sand-Trace . Total bbls water ? 3,492 bbls Total bbls oil ? 349 bbls Flowing for 71

HRS - 13:00 -Temp 122*, FCP 3,010? psi on 8/64" choke. 1hrs flowing. 012 BBls oil, 28.0 bbls water gas-091 mcf. Sand-Trace 14:00 -Temp 123*, FCP 3,040? psi on 8/64" choke. 1hrs flowing. 003 BBls oil, 34.0 bbls water gas-127 mcf. Sand-Trace 15:00 -Temp 121*, FCP 3,041? psi on 8/64" choke. 1hrs flowing. 022 BBls oil, 25.0 bbls water gas-212 mcf. Sand-Trace . Total bbls water ? 3,412 bbls Total bbls oil ? 300 bbls Flowing for 68 HRS - 10:00 -Temp 123*, FCP 2,995? psi on 6/64" choke. 1hrs flowing. 008 BBls oil, 17.0 bbls water gas-145 mcf. Sand-Trace 11:00 -Temp 122*, FCP 3,005? psi on 8/64" choke. 1hrs flowing. 006 BBls oil, 22.0 bbls water gas-173 mcf. Sand-Trace 12:00 -Temp 122*, FCP 3,000? psi on 8/64" choke. 1hrs flowing. 006 BBls oil, 33.0 bbls water gas-159 mcf. Sand-Trace Choke size was increased to a Positive 8 at 11am as per Energy Operators . Total bbls water ? 3,325 bbls Total bbls oil ? 263 bbls Flowing for 65 HRS - 07:00 -Temp 130*, FCP 3,006? psi on 6/64" choke. 1hrs flowing. 013 BBls oil, 52.0 bbls water gas-242 mcf. Sand-Trace 08:00 -Temp 130*, FCP 3,006? psi on 6/64" choke. 1hrs flowing. 017 BBls oil, 37.0 bbls water gas-237 mcf. Sand-Trace 09:00 -Temp 123*, FCP 3,030? psi on 6/64" choke. 1hrs flowing. 005 BBls oil, 21.0 bbls water gas-133 mcf. Sand-Trace Total bbls water ? 3,253 bbls Total bbls oil ? 243 bbls Flowing for 62 HRS

Daily Cost: $0

Cumulative Cost: $2,010,259

8/26/2013 Day: 14 **Completion**

Rigless on 8/26/2013 - Flow well - 01:00 -Temp 114*, FCP 3,008? psi on 8/64" choke. 1hrs flowing. 014 BBls oil, 13.0 bbls water gas-191 mcf. Sand-Trace 02:00 -Temp 116*, FCP 3,011? psi on 8/64" choke. 1hrs flowing. 016 BBls oil, 15.0 bbls water gas-255 mcf. Sand-Trace 03:00 -Temp 114*, FCP 3,014? psi on 8/64" choke. 1hrs flowing. 007 BBls oil, 27.0 bbls water gas-261 mcf. Sand-Trace 04:00 -Temp 115*, FCP 3,012? psi on 8/64" choke. 1hrs flowing. 008 BBls oil, 20.0 bbls water gas-243 mcf. Sand-Trace 05:00 -Temp 114*, FCP 3,015' psi on 8/64" choke. 1hrs flowing. 012 BBls oil, 23.0 bbls water gas-193 mcf. Sand-Trace Total bbls water ? 3,661 bbls Total bbls oil ? 436 bbls Flowing for 82 HRS - 21:00 -Temp 117*, FCP 3,052? psi on 10/64" choke. 1hrs flowing. 017 BBls oil, 24.0 bbls water gas-548 mcf. Sand-Trace 22:00 -Temp 118*, FCP 3,009 psi on 10/64" choke. 1hrs flowing. 025 BBls oil, 26.0 bbls water gas-425 mcf. Sand-Trace 23:00 -Temp 119*, FCP 2,993? psi on 10/64" choke. 1hrs flowing. 027 BBls oil, 25.0 bbls water gas-478 mcf. Sand-Trace 00:00 -Temp 122*, FCP 3,006' psi on 10/64" choke. 1hrs flowing. 020 BBls oil, 34.0 bbls water gas-328 mcf. Sand-TraceTraceTraceTraceTotal bbls water ? 4,228 bbls Total bbls oil ? 751 bbls Flowing for 101 HRS - 16:00 -Temp 112*, FCP 3,020? psi on 10/64" choke. 1hrs flowing. 010 BBls oil, 15.0 bbls water gas-58.0 mcf. Sand-Trace 17:00 -Temp 112*, FCP 3,030 psi on 10/64" choke. 1hrs flowing. 013 BBls oil, 65.0 bbls water gas-349 mcf. Sand-Trace 18:00 -Temp 114*, FCP 3,032 psi on 10/64" choke. 1hrs flowing. 028 BBls oil, 38.0 bbls water gas-309 mcf. Sand-Trace 19:00 -Temp 118*, FCP 3,036? psi on 10/64" choke. 1hrs flowing. 021 BBls oil, 17.0 bbls water gas-384 mcf. Sand-Trace 20:00 -Temp 118*, FCP 3,050' psi on 10/64" choke. 1hrs flowing. 011 BBls oil, 41.0 bbls water gas-331 mcf. Sand-TraceTraceTraceTotal bbls water ? 4,025 bbls Total bbls oil ? 618 bbls Flowing for 97 HRS - 11:00 -Temp 113*, FCP 3,040 psi on 10/64" choke. 1hrs flowing. 005 BBls oil, 16.0 bbls water gas-89.0 mcf. Sand-Trace 12:00 -Temp 107*, FCP 3,049? psi on 10/64" choke. 1hrs flowing. 000 BBls oil, 10.0 bbls water gas-98.0 mcf. Sand-Trace 13:00 -Temp 110*, FCP 3,008? psi on 10/64" choke. 1hrs flowing. 012 BBls oil, 14.0 bbls water gas-200 mcf. Sand-Trace 14:00 -Temp 111*, FCP 2,988? psi on 10/64" choke. 1hrs flowing. 014 BBls oil, 26.0 bbls water gas-394 mcf. Sand-Trace 15:00 -Temp 112*, FCP 3,020' psi on 10/64" choke. 1hrs flowing. 015 BBls oil, 19.0 bbls water gas-240 mcf. Sand-TraceTraceTotal bbls water ? 3,849 bbls Total bbls oil ? 545 bbls Flowing for 92 HRS - 06:00 -Temp 114*, FCP 3,014? psi on 8/64" choke. 1hrs flowing. 014 BBls oil, 25.0 bbls water gas-291 mcf. Sand-Trace 07:00 -Temp 120*, FCP 3,010? psi on 8/64" choke. 1hrs flowing. 013 BBls oil, 20.0 bbls water gas-211 mcf. Sand-Trace 08:00 -Temp 113*, FCP 2,990? psi on 8/64" choke. 1hrs flowing. 010 BBls oil, 22.0 bbls water gas-272 mcf. Sand-Trace 09:00 -Temp 109*, FCP 3,010 psi on 8/64" choke. 1hrs flowing. 010 BBls oil, 23.0 bbls water gas-197 mcf. Sand-Trace 10:00 -Temp 113*, FCP 2,990' psi on 8/64" choke. 1hrs flowing. 016 BBls oil, 13.0 bbls water gas-239 mcf. Sand-TraceTotal bbls water ? 3,764 bbls Total bbls oil ? 499 bbls Flowing for 87 HRS

Daily Cost: $0

Cumulative Cost: $2,024,124

8/27/2013 Day: 15 **Completion**

RECEIVED: Oct. 10, 2013

Rigless on 8/27/2013 - DO Plug - Update for Lejeune 1-17-3-2WH 8-27-13 10:00 -Temp 120*, FCP 2,955 psi on 10/64" choke. 1hrs flowing. 025 BBls oil, 30 bbls water gas- 468 mcf. Sand-Light 11:00 - Temp 115*, FCP 2,949 psi on 10/64" choke. 1hrs flowing. 029 BBls oil, 34 bbls water gas- 500 mcf. Sand-Light 12:00 -Temp 115*, FCP 2,944 psi on 10/64" choke. 1hrs flowing. 023 BBls oil, 25 bbls water gas- 493 mcf. Sand-Light Total bbls water ? 4,507 bbls Total bbls oil ? 1070 bbls Flowing for 113 HRS (Made mistake on last report for Hours Flowing) 11:00 CT has BOP stack ready to be torqued up. Hold Safety & JSA meeting for Torqueing Up BOP Stack. 12:00 Closed well in so we could nipple up CT BOPs and Test Blind Shear & Cudd?s Manuel Gatevalve. - 06:00 -Temp 115*, FCP 2,975 psi on 10/64" choke. 1hrs flowing. 012 BBls oil, 25 bbls water gas- 323 mcf. Sand-Light 07:00 -Temp 120*, FCP 2,975 psi on 10/64" choke. 1hrs flowing. 040 BBls oil, 23 bbls water gas- 426 mcf. Sand-Light 08:00 -Temp 119*, FCP 2,970 psi on 10/64" choke. 1hrs flowing. 030 BBls oil, 29 bbls water gas- 455 mcf. Sand-Light 09:00 -Temp 120*, FCP 2,975 psi on 10/64" choke. 1hrs flowing. 038 BBls oil, 16 bbls water gas- 472 mcf. Sand-Trace Total bbls water ? 4,418 bbls Total bbls oil ? 993 bbls Flowing for 110 HRS 08:00; CT Arrive on location. Hold Safety meeting & JSA for Rigging Up. - 01:00 -Temp 119*, FCP 3,001 psi on 10/64" choke. 1hrs flowing. 022 BBls oil, 33 bbls water gas-473 mcf. Sand-Light 02:00 -Temp 118*, FCP 2,991 psi on 10/64" choke. 1hrs flowing. 023 BBls oil, 24 bbls water gas-410 mcf. Sand-Light 03:00 -Temp 118*, FCP 2,987 psi on 10/64" choke. 1hrs flowing. 030 BBls oil, 24 bbls water gas- 420mcf. Sand-Light 04:00 -Temp 120*, FCP 2,979? psi on 10/64" choke. 1hrs flowing. 037BBls oil, 21 bbls water gas- 427mcf. Sand-Trace 05:00 -Temp 119*, FCP 2,982 psi on 10/64" choke. 1hrs flowing. 020 BBls oil, 22 bbls water gas-402 mcf. Sand-Trace Total bbls water ? 4,036 bbls Total bbls oil ? 705 bbls Flowing for 106 HRS - Total bbls water ? 4,507 bbls Total bbls oil ? 1070 bbls Flowing for 113 HRS (Made mistake on last report for Hours Flowing) 12:00 Closed well in so we could nipple up CT BOPs and Test Blind Shear & Cudd?s Manuel Gate valve. 16:00 Finished Testing Gate valve & Blind Shear Rams. 17:00 Stabbing Injector on BOP to finish testing BOPs - 18:00 Pull tested CT Con to 25k (Good) & Tested to 9500psi as well.. 19:00 Function tested Motor (Good) and Stab on Wellhead. - 21:00 -Temp 117*, FCP 3,052? psi on 10/64" choke. 1hrs flowing. 017 BBls oil, 24.0 bbls water gas-548 mcf. Sand-Trace 22:00 -Temp 118*, FCP 3,009 psi on 10/64" choke. 1hrs flowing. 025 BBls oil, 26.0 bbls water gas-425 mcf. Sand-Trace 23:00 -Temp 119*, FCP 2,993? psi on 10/64" choke. 1hrs flowing. 027 BBls oil, 25.0 bbls water gas-478 mcf. Sand-Trace 00:00 -Temp 122*, FCP 3,006' psi on 10/64" choke. 1hrs flowing. 020 BBls oil, 34.0 bbls water gas-328 mcf. Sand-TraceTraceTraceTraceTotal bbls water ? 4,228 bbls Total bbls oil ? 751 bbls Flowing for 101 HRS - PJSM. Coil Connector was installed and pressure tested to 250 psi for 5 min and 9,000 psi for 10 min. When Coil Connector was installed it was pull tested to 25,000#. MU Weatherford BHA Convex Mill OD- 4.625? ID-1.250? L-1.56?, Force Flex Motor OD-2.875? L-10.53?, H.D Disconnect .625? Ball Drop OD-2.875? ID 0.500? L-2.27?, Dual Acting Jar OD-2.875? ID-1.000? L-4.81?, Stablizer Sub OD-3.500? ID-1.250? L-1.03?, 2-7/8? MHA With Flappers .875 Disconnect Ball OD-2.875? L-3.55?. 2.0? Tree and shell test 250 psi for 5 min and 9,000 psi for 10 min. Test good, RIH with CT @ 80? ? 90? fpm. Pump rate to 2.5 bpm 3.5 return - RIH with CT @ 80? ? 90? fpm. Pump rate to 2.5 bpm 3.5 return 9,300'
Daily Cost: $0
Cumulative Cost: $2,042,489

8/28/2013 Day: 16 **Completion**

Rigless on 8/28/2013 - CT DO Plugs - We Retagged Plug #7 @ 10,710?' @ 10:40 & DO 110 mins. Pump 10 bbl gel sweep. Wash to Plug #8 @ 10,964? @ 13:29 (WHP @ 2,792 psi pumping 2-1/4 bpm & returns 4 bpm). - Plug #5 @ 9,900' & DO 60 min. Pump 10 bbl gel sweep. Wash to Plug #6 @ 10531? (WHP @ 2,792' psi pumping 2-1/4 bpm & returns 4 bpm). Plug #6 @ 10531? & DO 83 min. Pump 10 bbl gel sweep. Wash to Plug #7 @ 10,710? pump 10 bbl gel sweep (WHP @ 2800 psi pumping @ 2.25 bpm & returns @ 4bpm). Waiting for 10bbl gel sweep to clear the end of the CT and then we will short trip to KOP @ 8359?. - Wash to Plug #4 (WHP @ 2,700' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). Tag #4 Making short tip to KOP @ 8,359? Tag plug #4 @ 10,117?' & DO 30 min. Pump 10 bbl gel sweep. Wash to Plug #5 (WHP @ 2,700' psi pumping 2-1/4 bpm & returns 4 bpm). RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #5 @ 10,335 Drilling on plug #5 (WHP @ 2,700' psi pumping 2-1/4 bpm & returns 4 bpm). - RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #3 @ 9,900' & DO 28 min. Pump 10 bbl gel sweep. Wash to Plug #4 (WHP @ 2,700' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). - RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #2 @ 9,714' & DO 28 min. Pump 10 bbl gel sweep. Wash to Plug #3 (WHP @ 2,700' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). - RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #1 @ 9,520' & DO 28 min. Pump 10 bbl

gel sweep. Wash to Plug #2 (WHP @ 2,700' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). - P/U New BHA- Convex Mill OD-4-1/2 ID-1.250 L-1.70, Force Flex Motor OD-2.875 L-10.53, CTT Aggittor OD-2.875 L-5.53, HD Disconnect .625 Ball Drop OD-2.8875 ID-.500 L-2.27, Dual Acting Jar OD-2.875 ID-1.000 L-4.81, Stablizer Sub OD-3.500 ID-1.250 L-1.03, .875 Disconnect Ball OD-2.875 L-3.55. Total Length of BHA-29.42. Shell test 250? psi for 5 min and 9,000?psi for 10 min, test good. Started RIH w/BHA - We have been milling on plug #8 for 2.5hrs with no luck. We are pumping a Sweep and once it comes around the end of CT we will POOH and check and or change BHA. - POOH LD & BHA
Daily Cost: $0
Cumulative Cost: $2,108,373

8/29/2013 Day: 17 **Completion**

Rigless on 8/29/2013 - CTU DO Plugs - RIH w/BHA Wash to 10,855? tag (WHP @ 2,792 psi pumping 2-1/4 bpm & returns 4 bpm). - RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #8 @ 10,964' & DO 45 min. Pump 10 bbl gel sweep. Wash to Plug #9 (WHP @ 2,700' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #9 @ 11,132 & DO 40 min. Pump 10 bbl gel sweep. Wash to Plug #10 (WHP @ 2,700' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #10 @ 11,300' & DO 67 min. Pump 10 bbl gel sweep. Wash to Plug #11 (WHP @ 2,700' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). - 06:00 Update: Made ST to KOP at 8,359?. RIH to Plug #12. Circulating 2.25 bpm with 3.5 bpm returns. WHP @ 2,400 psi. 07:00 We have Paraffin in our return tanks and cannot transfer our fluid so we are pulling up to the Vertical and will shut down CT Ops until Hot Oilers heat fluid and we get it sucked out of the tanks. 09:00 Hot oiler has arrived. We are holding a Safety Meeting & Review JSA?s along with Fire Assessment. We will have a Fire Watch in place as well. - 13:00 We are still heating up the Gas Buster Tanks with Hot Oilers. 15:30 We are still heating up the Gas Buster Tanks with Hot Oilers and transferring oil to production tanks. - 17:00 All oil and parrifin has been moved to production tanks. 17:10 CT RIH to Plug # 12, Circulating 2.25 bpm with 3.5 bpm returns. WHP @ 2,400 psi.434 bbls oil moved to production tank - RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #12 @ 11,708' & DO 67 min. Pump 10 bbl gel sweep. Wash to Plug #13 (WHP @ 2,500' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #13 @ 11,908' & DO 63 min. Pump 10 bbl gel sweep. Wash to Plug #14 (WHP @ 2,550' psi pumping 2-1/4 bpm & returns 3-1/2 bpm - RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #14 @ 12,108' & DO 128 min. Pump 10 bbl gel sweep. Wash to Plug #15 (WHP @ 2,500' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). RIH w/BHA pump 2-1/4 bpm fresh water. plug #15 no plug & sand ' & Pump 10 bbl gel sweep. Wash to Plug #16 (WHP @ 2,550' psi pumping 2-1/4 bpm & returns 3-1/2 bpm - RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #11 @ 11,508' & DO 101 min. Pump 10 bbl gel sweep. Wash to Plug #12 (WHP @ 2,400' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). Making short trip to KOP @ 8359?. Made ST to KOP at 8,359?. RIH to Plug #12. Circulating 2.25 bpm with 3.5 bpm returns. WHP @ 2,400 psi.
Daily Cost: $0
Cumulative Cost: $2,202,511

8/30/2013 Day: 18 **Completion**

Rigless on 8/30/2013 - Pro-Technics Logging - RIH to Plug #18 06:15 We tagged Plug # 18 @ 12918?, Circ @ 4630 psi. WH @ 2614 psi, Pump rate @ 2.25bpm / Return @ 2.25 bpm 07:36 Drill out plug # 18 in 81mins. Wash to Plug # 19 - RIH 100 fpm pumping 1 bpm every 1,000? Ft to 8,450 WH psi 2,790' - LD Weatherford DO BHA, Pull test connector 20,000 test good. RIH w/MU Weatherford BHA on CT Rod Box 5/8 OD-1.000 L-0.34, Crossover Sub OD-2.875 ID-1.125 L-0.28 2-7/8 M.H.A OD-2.875 ID-0.625 L-3.55 MU Pro-Technics Bottom-Up Spinner fixed cage continuous OD-1.7 Weight-2.5 L-16.47, Centralizer OD-1.688 Weight-10.0 L-29.19, Fluid Density OD-1.688 Weight-7.0 L-28.02, Centralizer OD-1.688 Weight-10.0 L-29.19, ICL collar locator OD-1.688 Weight-6.5 L-24.00, Centralizer OD-1.688 Weight-10.0 L-29.19, CPT psi temperature CPT-Temperature CPT-Pressure OD-1.688 Weight-9.0 L-28.39, Spectral Gamma Ray OD-1.688 Weight-10.5 L-39.5, CCL mechanical)D-1.688 Weight-1.5 L-18.88, Battery (1) OD-1.688 Weight-17.5 L-74.33, Cable Head 5/8? SR OD-1.688 Weight-2.0 L-2.75, (1) Knuckle JT OD-1.688 Weight-4.0 L-9.0, (2) Knuckle JT OD-1.688 Weight-4.0 L-9.0, Top Connection-5/8 sucker rod pin. RIH 100 fpm pumping 1 bpm every 1,000? Ft to 8,450 - Added ground rods & daisy chains to fresh water tanks due to the presence of hydrocarbons in the tanks. Filled 2 tanks with fresh water and heated one of them to 175 degrees. Pulled CT to kick off

point and circulated there until water was hot enough to pump and melt paraffin. POOH at 80-100 fpm while pumping 3/4 bpm. Pulled to 200? and pumped 200 bbls of 175 degree water to finish melting paraffin in frac tree and in surface lines. Plan forward: POOH and LD mill and motor assembly. MU Pro-Technics production logging tools and log well as per program. - 07:40 Tagged Plug #19 @ 13094?, Drill Up in 150 mins, WH @ 2700 psi, Circ @ 4690 psi @ 2.25 bpm & Return @ 2.25 bpm. 10:20 Wash down to 13170? CTM (Never Tagged), Slow pump rate to .75 bpm and Lightly Tagged @ 13177? CTM. Pick up 5ft and start pumping 20bbl Sweep. Once Sweep clears EOT we will start picking up at 30ft/min then 40ft/min. - RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #16 @ 12,499' & DO 120 min. Pump 10 bbl gel sweep. Wash to Plug #17 (WHP @ 2,500' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). RIH w/BHA pump 2-1/4 bpm fresh water. Tag plug #17 @ 12,678' & DO 120 min. Pump 10 bbl gel sweep. Wash to Plug #18 (WHP @ 2,500' psi pumping 2-1/4 bpm & returns 3-1/2 bpm). Pump 10 bbl gel sweep, Making short trip to KOP @ 8,359?
Daily Cost: $0
Cumulative Cost: $2,306,474

8/31/2013 Day: 19 **Completion**

Rigless on 8/31/2013 - NU B.O.P Stack - MIRU Nabors WOR. RU B&G Crane ND Frac stack - MU PU weatherford 5-1/2' X 2-7/8' AS1-X PKR 10K Wireline set, RIH w2-/78' N-80 Re-entry guide OD-3.625 ID-3.000 L-0.41, 2-7/8' Burst Dise Sub 10K OD-3.689 ID-2.560 L-0.77, 2-7/8' N-80 pup sub OD 2.875 ID 2.441 L-4.23, 2-7/8' X 2.205' XN Nipple OD-2.785 ID-2.205 L-1.28, 2-7/8' N-80 pup sub OD-2.875 ID-2.441 L-4.00, 5-1/2' X 2-7/8" AS1-X PKR 10K Wireline set OD-4.500 ID-2.438 L-6.93, 2-7/8' X 2.31' X Seal Nipple OD-3.250 ID- 2.312 L-1.30. RIH 70 fpm Set PKE @ 8,732' POOH shut well in RDMO J-W open well 2,600' psi bleed pressure to 0 psi monitoring for 30 mins after pressure reaches 0 psi, PKR good. - 13:00 Cudd is rigged down and moving equipment off location. We are rigging up JW wireline at moment to RIH to set 5.5? Arrow-Set packer as per NFEX program. Hot Oilers are heating up Paraffin & Oil in tanks so we can transfer to Production Tanks. 15:00 Tested WL Lube to NFX policy. JW wireline is RIH to make 4.5? Gauge Ring Run. (Tool String; Cable Head 1ft long x 1.44?OD, Tungsten Wt Bar 2.75? OD x 5ft long, Steel Wt Bar 3.13?OD x 7ft long, CCL 3.12?OD x 1.25ft, Quick Change 3.14?OD x 1.5ft long, Junk Basket 3.14?OD x 6.08ft long, Gauge Ring 4.5?OD x .25ft long). Hot Oilers are heating up Paraffin & Oil in tanks so we can transfer to Production Tanks. - Information verified by Pro-Technics. We are currently blowing down coil and preparing to rig them down. Plan forward: RD Cudd. RU JW wireline and set 5.5? ArrowSet packer as per program. ND frac tree. NU Knight BOPE. RU Nabors Rig 1460. - POOH w/Pro-Technics Log tool. Pro-Technics tools are out of the hole. The depths have been verified and the deepest that the tools were to get to. Tools were unable to go deeper due to friction in well. Centralizer came out of hole with one of the arms bent. Picture attached. Currently: Pro-Technics rep is verifying log before we blow down release CTU. 1st run ? 12,510? Deepest perforations logged were stage 5. 12,370?-12,372? & 12,440?-12,442?. 2nd run ? 11,680? Deepest perforations logged were stage 9. 11,553?-11,555? & 11,639?-11,641?. - RIH to 8,450 Make a 10:00 min stationary stop, (1) Started down pass 8,450' @ 40 fpm WH psi 2,793' 3-1/2 bbls returns take water & oil samples for flow profiler oil evaluation to 12,510'. CTU lock up do to friction @ 12,510. Start up pass @ 40 fpm WH psi 2,690' 3-1/2 bbls returns take water & oil samples for flow profiler oil evaluation to 8,450' - RIH to 8,450 Make a 10:00 min stationary stop, (2) Started down pass 8,450' @ 80 fpm WH psi 2,600 3-1/2 bbls returns take water & oil samples for flow profiler oil evaluation to 11,683. CTU lock up do to friction @ 11,683. Start up pass @ 80 fpm WH psi 2,600' 3-1/2 bbls returns take water & oil samples for flow profiler oil evaluation to 8,450'
Daily Cost: $0
Cumulative Cost: $2,395,161

9/1/2013 Day: 20 **Completion**

Rigless on 9/1/2013 - NU 10K production tree and test as per Newfield?s procedures - ND BOP?s Sack - Cameron test unit. Perform dead head test to 10,000 psi. Test good. BO pressure. Accumulator: Perform hydraulic test to 1,500 psi on all component consisting of: Blind shear rams, bottom 2-7/8 pipe rams. RU test hose to choke kill valve on double BOP. Closed Blind shear rams. Function & pressure test blind shear rams to 250 psi for low, for 5 min w/HCR valve closed. Test good. BO pressure. Test same to 10,000 psi for high, for 10 min. Test good. BO pressure. PU a 2-7/8 mandrel ran down though BOP stack to the lower 2-7/8 BOP pipe rams and closed same. Function & pressure

test lower 2-7/8 BOP pipe rams against HCR valve to 250 for low, for 5 min. Test good. BO pressure. Test same to 10,000 psi for high, for 10 min. Test good. BO pressure. Open lower BOP pipe rams. Pull out and LD 2-7/8 mandrel. Lower 2-7/8? BOP pipe ram Test 250? Low good, not test for high, Change out 2-7/8? pipe ram rubber. 10K Annular B & G Crane released. - . Lower 2-7/8? BOP pipe ram Test 250? Low good, not test for high, Change out 2-7/8? pipe ram rubber and continue with testing procedure. All valves and components to the BOPE has been tested and charted as per Newfield guidelines. - All valves and components to the BOPE has been tested and charted as per Newfield guidelines. Jessen electric is on location to ground rig, catwalk and load lines on production load line area. Bled well down and opened HCR. We had a near miss when opening well. Near miss: Due to paraffin in flowback iron we had a false sense of well being bled down and when the HCR was actuated trapped pressure caused the tubing spider to blow off of BOP. The tubing spider door was ejected causing it to fall to the ground. No injuries or equipment damage. Post incident safety meeting with all personnel on location. Rigged up Hot Oil Truck and pumped 200 degree water though all flowback equipment and across well head to assure that all paraffin on surface has been melted and cleared. - Make up o/o tool, 1 jt 2 7/8" L-80 tbg and "X" profile Nipple. Currently: 195 jts in the hole. We are measuring the last row. Plan forward: MIH with o/o tool and tbg. Tag, space out tbg and change well over with 95 degree packer fluid. ND BOPE. Install production tree and put well on production. Tagged packer with jt #271 @ 8,728?. Engaged packer and pulled 15K over and set 10K in compression. Spaced out packer 10K in compression. Added an 8? pup jt and landing jt.Circulating packer fluid at Co Rep change out time. - NU Knight B.O.P Stack. 10K 7-1/16" pipe BOP w/Blind shear rams and double valve choke/kill outlets, 10K 7-1/16" pipe BOP w/2-7/8" pipe rams on top of FMC 10K 7-1/16? "Master" HCR valve, 10K 7-1/16" flow cross w/dual, double valved 2-1/16" outlets & 10K x 5K 7-1/16" spool. 10K Annula - Circulating 230 bbls packer fluid. Laid over WOR derrick, Testing hanger and packer, 250 Psi low, 5,000 Psi high. Tested good,
Daily Cost: $0
Cumulative Cost: $2,506,895

9/2/2013 Day: 21 **Completion**

Rigless on 9/2/2013 - NU 10K production tree test -Pump off Disk with hot oiler and - Rig Up to production facility and Pop well at 08:40 am on 9/2/13 2500 psi on Tubing 6/64 choke casing pressure 0 - NU 10k production tree and test as per Newfield?s procedures.Test Good - PJSM, MIRU Preferred Hot Truck to Burst Disc in Tubing and Flow Well to Production. - 06:30 Started pumping got 3bbls pumped and well pressured up to 4500psi, shut down bleeds off psi and checked well head valves all open. Started pumping again got 4bbls away and disc blew. We pumped 100bbls behind @ 2600psi injection. Took 5000psi to rupture the disc. WH@2600psi 08:10 Rigging down Hot Oiler and turning well over to production to Open. 08:40 Open Well to production. On a 6/64 choke Well Head Psi @ 2500psi flowing tubing pressure. - 09:00 Releasing all Equipment and cleaning up location etc.
Daily Cost: $0
Cumulative Cost: $2,581,434

9/17/2013 Day: 22 **Completion**

Rigless on 9/17/2013 - Capture Costs n DCR - Capture Costs n DCR
Daily Cost: $0
Cumulative Cost: $2,634,327

RECEIVED: Oct. 10, 2013